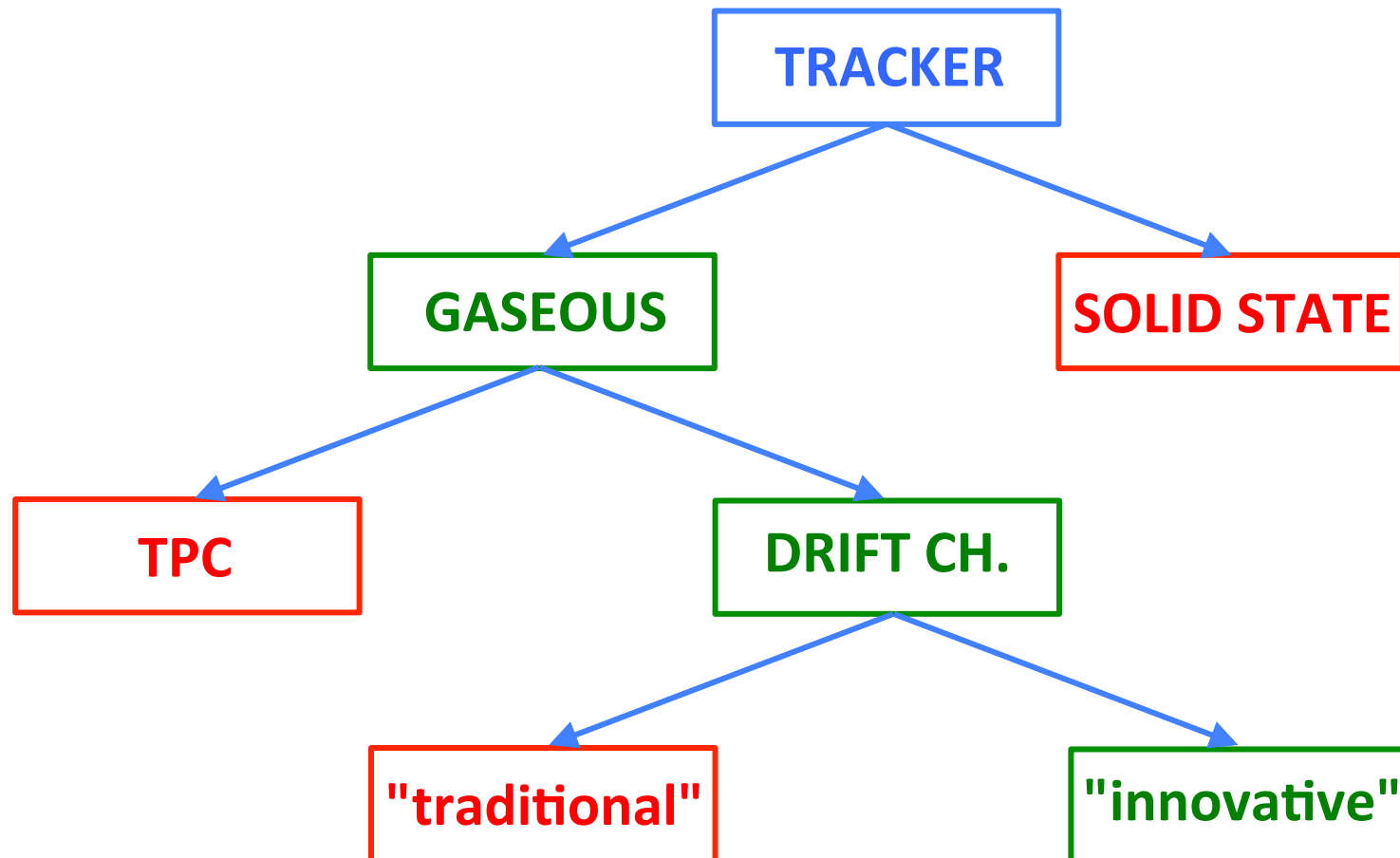


An ultra-light drift chamber with particle identification capabilities

F. Grancagnolo
INFN – Lecce, ITALY

CEPC-SppC Study Group Meeting
Beihang University
2-3 September 2016

Tracker alternatives



Road to proposal

- Ancestor chamber: **KLOE** at **INFN LNF Daφne φ factory** (commissioned in 1998 and currently operating)
- **CluCou** Chamber proposed for the **4th-Concept** at **ILC** (2009)
- **I-tracker** chamber proposed for the **Mu2e experiment** at **Fermilab** (2013)
- **DCH** for the **MEG2 upgrade** at **PSI** (under construction at INFN and to be commissioned during spring 2017)

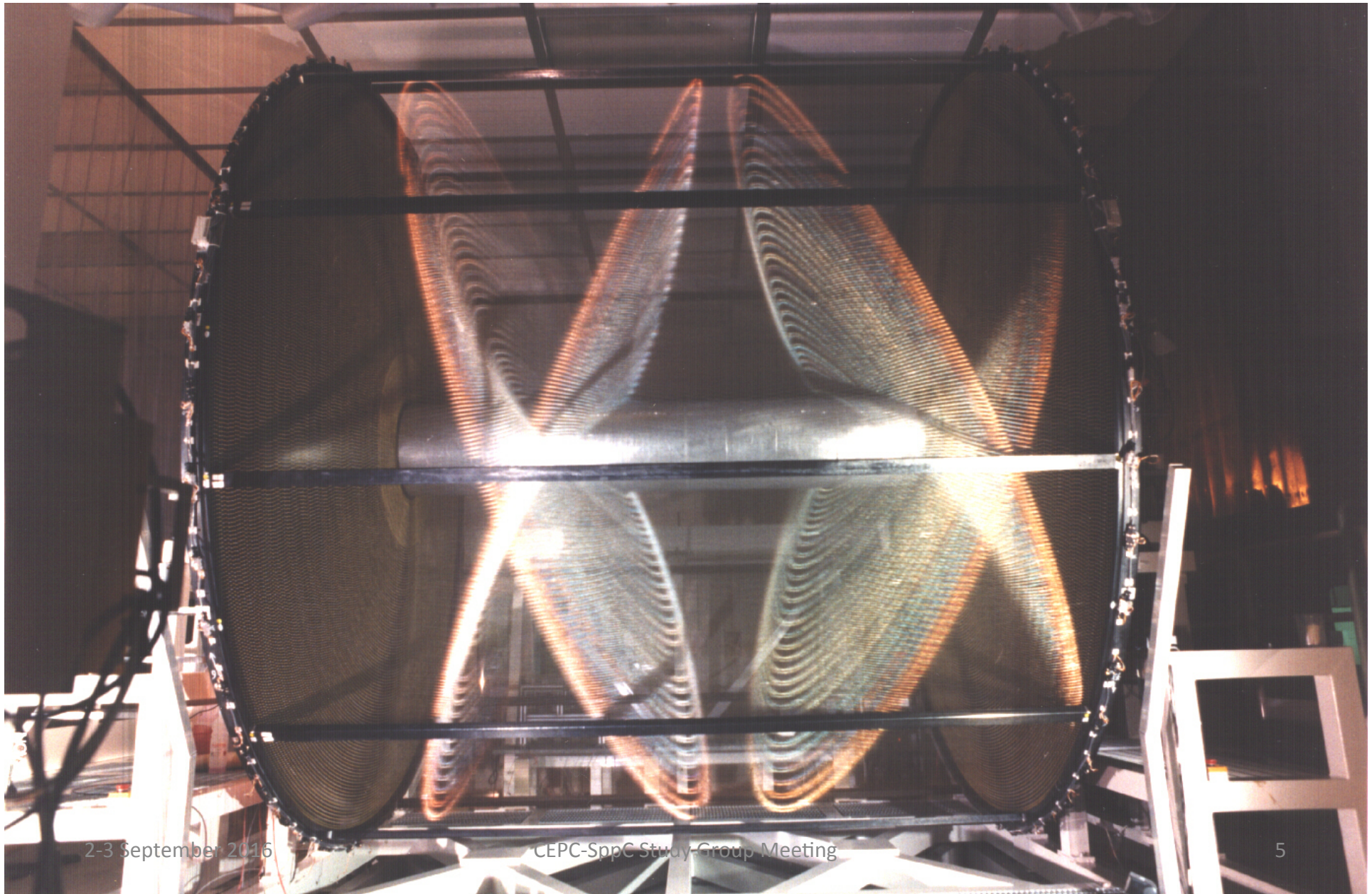
"Traditional" Drift Chamber

A cylindrically symmetric gas volume with (para-)axial wires defining a strong electric field, strung under mechanical tension for electrostatic stability and fixed at their extremities to the end walls by means of feed-through.

CONSTRAINTS:

- The **end walls**, holding the feed-through (which limit the chamber granularity), the FE electronics and the relative cabling, must be rigid enough to transfer the load due to the wire tension (of the order of several Tons) to the **outer cylindrical wall**, without deforming.
- The **inner cylindrical wall**, usually, does not bear any load, to minimize the multiple scattering of incoming particles.
- The **gas tightness** relies on the hermetic properties of all surfaces and of all their relative joints.

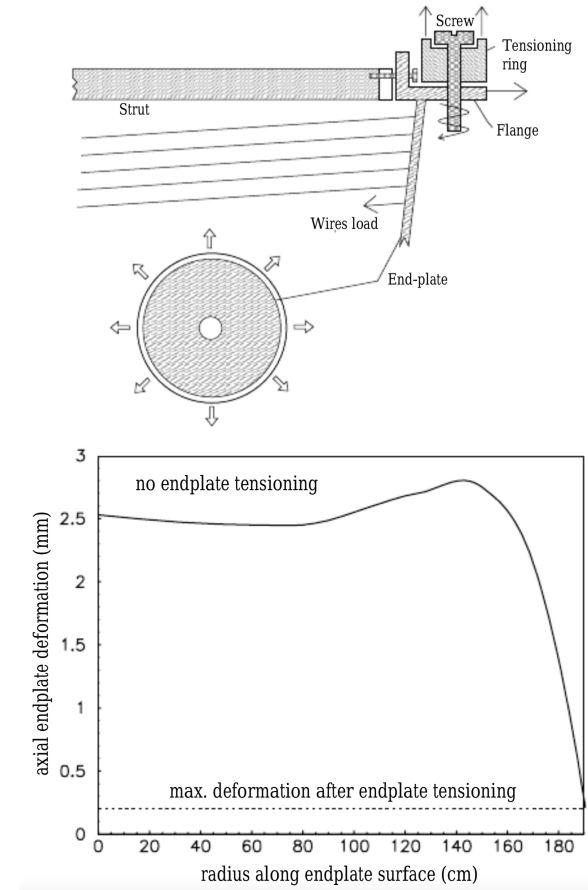
The KLOE Drift Chamber



The KLOE Drift Chamber

Mechanical and construction characteristics

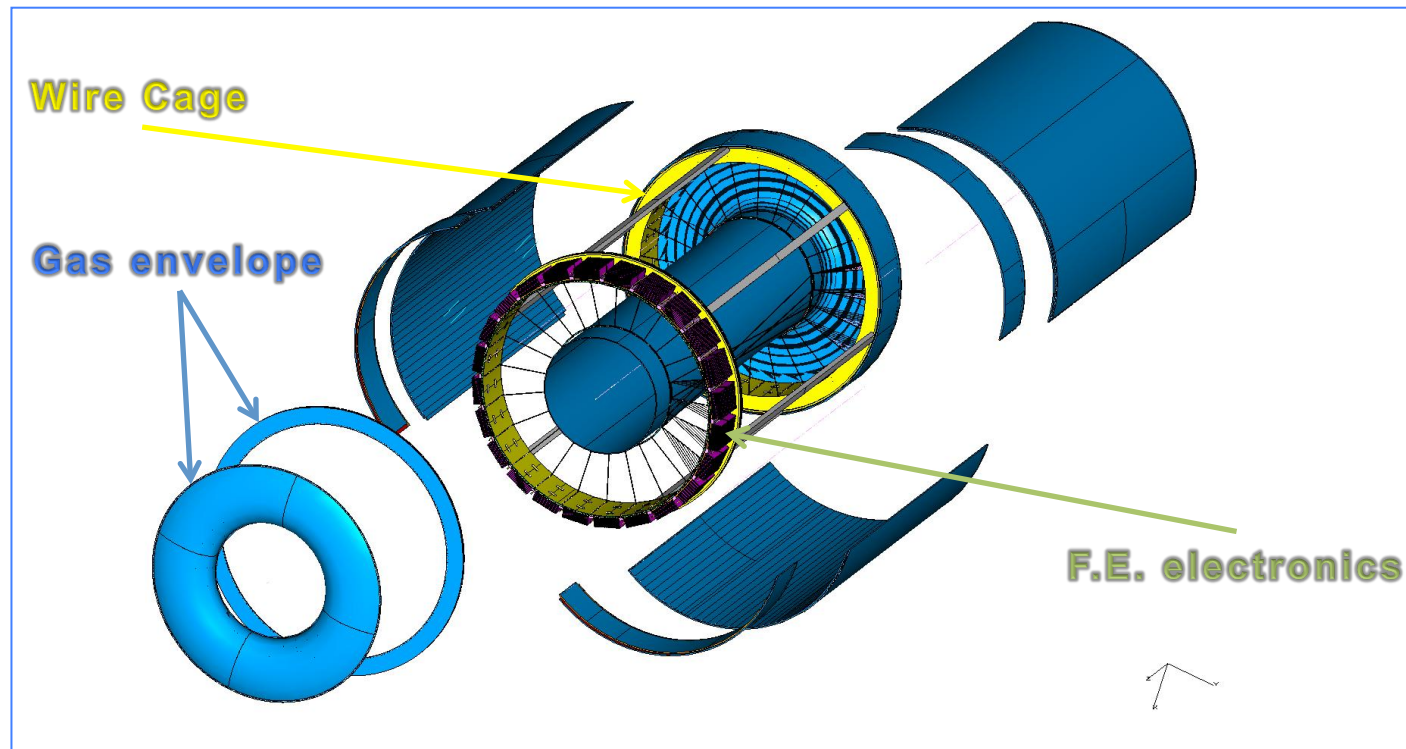
Outer radius	1980 mm
Outer panels thickness	39.0 mm
Inner cylinder radius	250 mm
Inner cylinder thickness	1.1 mm
End-plate radius of curvature	9760 mm
End-plate thickness	9 mm ($0.03 X_0$)
C-fiber X_0	26.7 cm
Maximum length	3320 mm
Minimum length	2800 mm
Number of drift cells	12,582
Number of wires	52,140
End-plate wire load	3500 kg



Drift Chamber "Innovations"

1. Separating **gas containment** from **wire support** functions
2. Using **a larger number** of **thinner** (and **lighter** wires)
3. No **feed-through** wiring
4. Using **cluster timing** for improved spatial resolution
5. Using **cluster counting** for particle identification

Gas containment and Wire support



Gas containment **Gas envelope** can freely deform without affecting the internal wire position and tension.

Wire support **Wire cage** structure not subject to differential pressure can be light and feed-through-less.

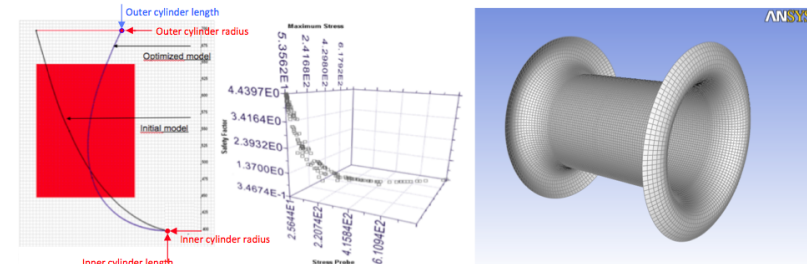
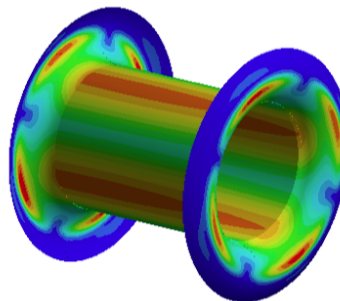
Example: The Mu2e I-Tracker proposal

Gas Envelope

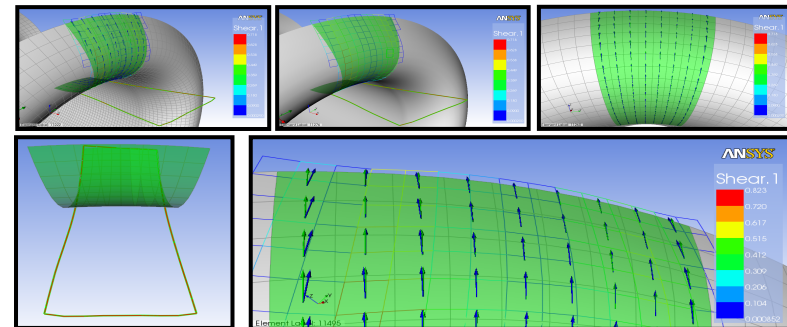
A structural multivariate analysis software (**ModeFrontier®**) has enabled to find the optimal shape for the **profile of the end plates** by minimizing maximum stress and stress on inner cylinder

ANSYS ACP® has chosen the proper unidirectional prepreg to form **ply**, **draping** of the laminates and **flat-wrap** of the optimized model

Solve buckling problems of inner cylinder by increasing the **moment of inertia** with use of proper light core composite sandwich



parameters	Initial model	Optimized model
Maximum stress	357.5 MPa	58.7 MPa
Stress at inner boundary	267.4 MPa	26.6 MPa
Safety factor	0.783	4.44



End plates:

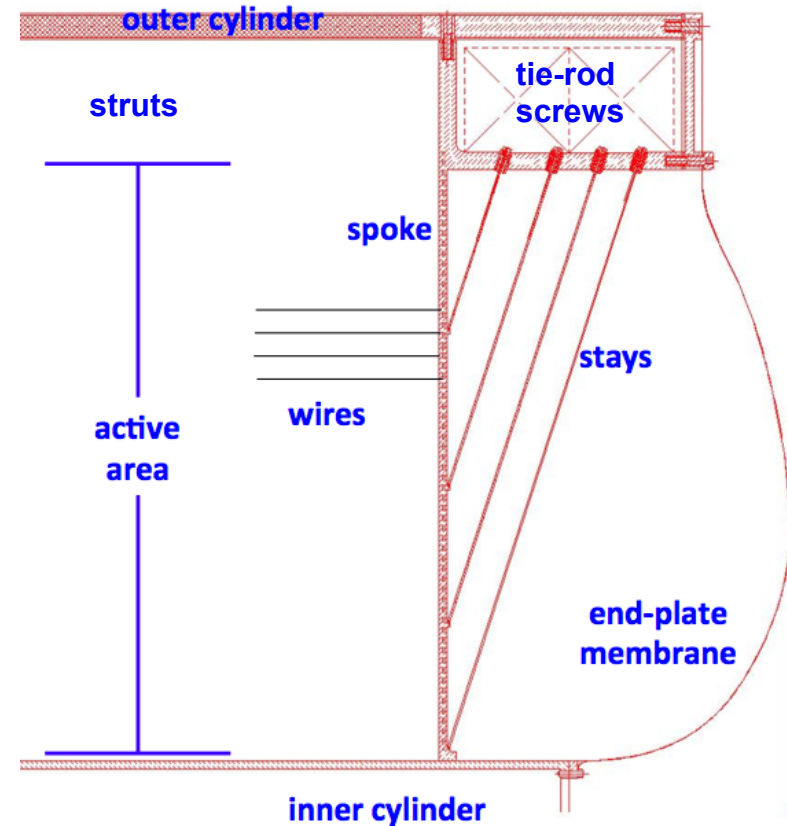
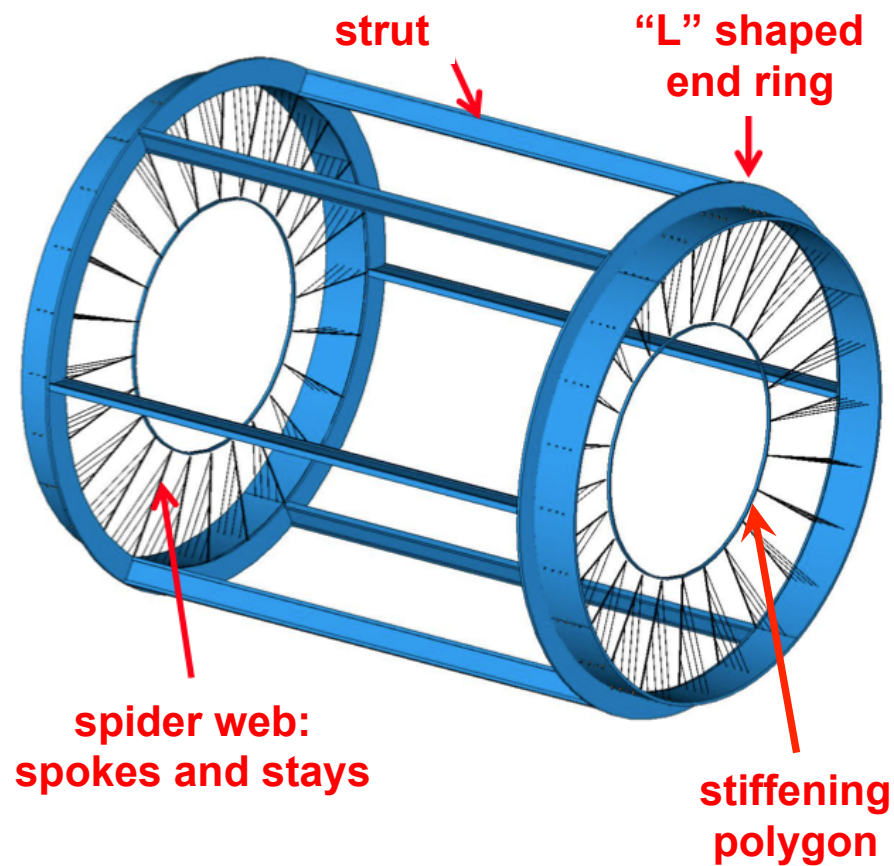
4-ply 38 μ m/ply
orthotropic (0/90/90/0)
0.021 g/cm²
5 $\times 10^{-4}$ X₀

Inner cylinder:

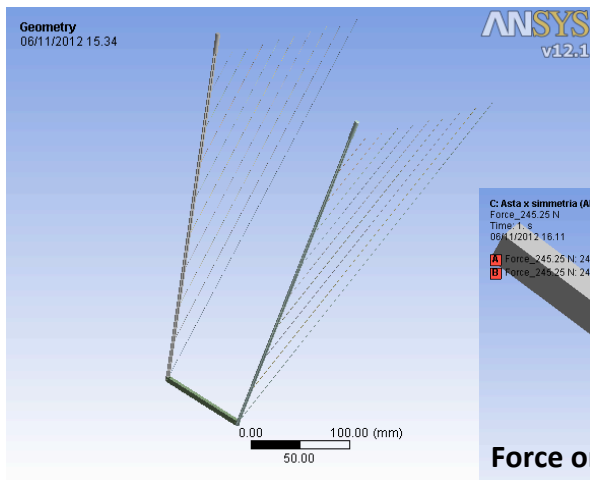
2 C-fiber skins, 2-ply,
C-foam core, 5 mm
0.036 g/cm²
9 $\times 10^{-4}$ X₀

Example: The Mu2e I-Tracker proposal

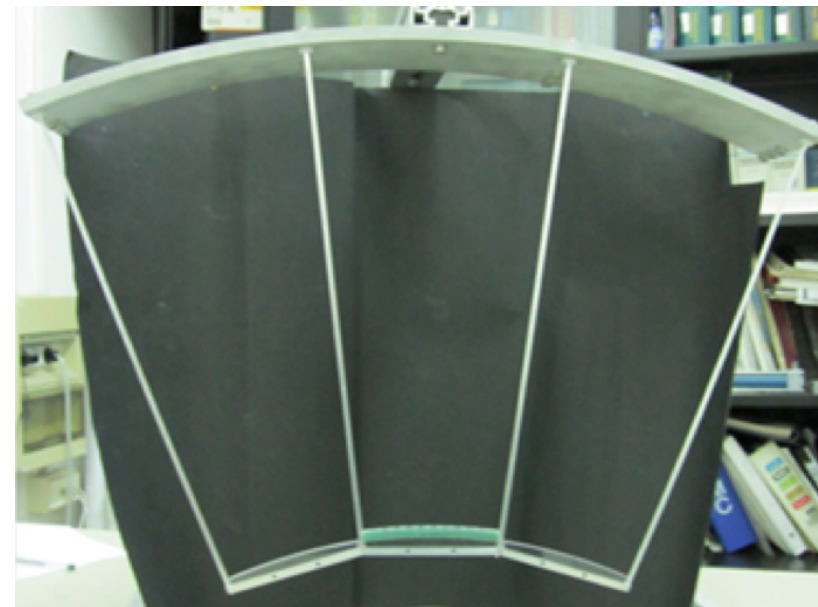
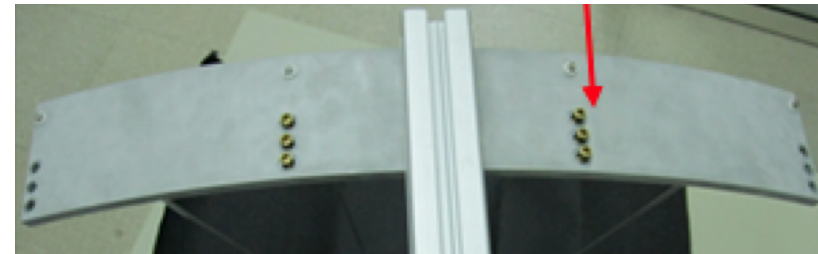
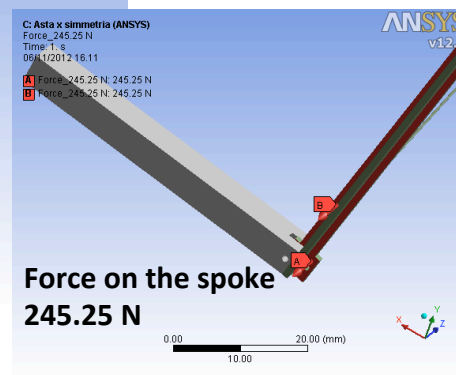
Wire cage (conceptual)



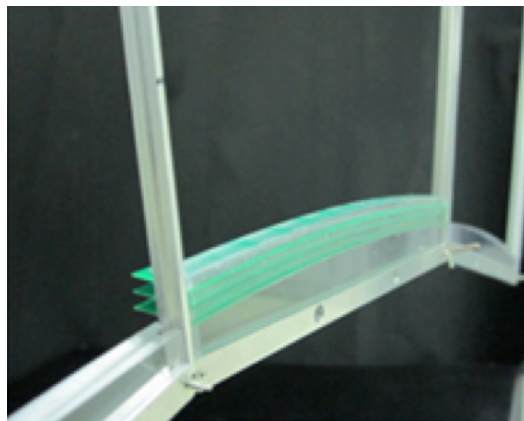
Verification of validity of principle



ANSYS
FEM
analysis



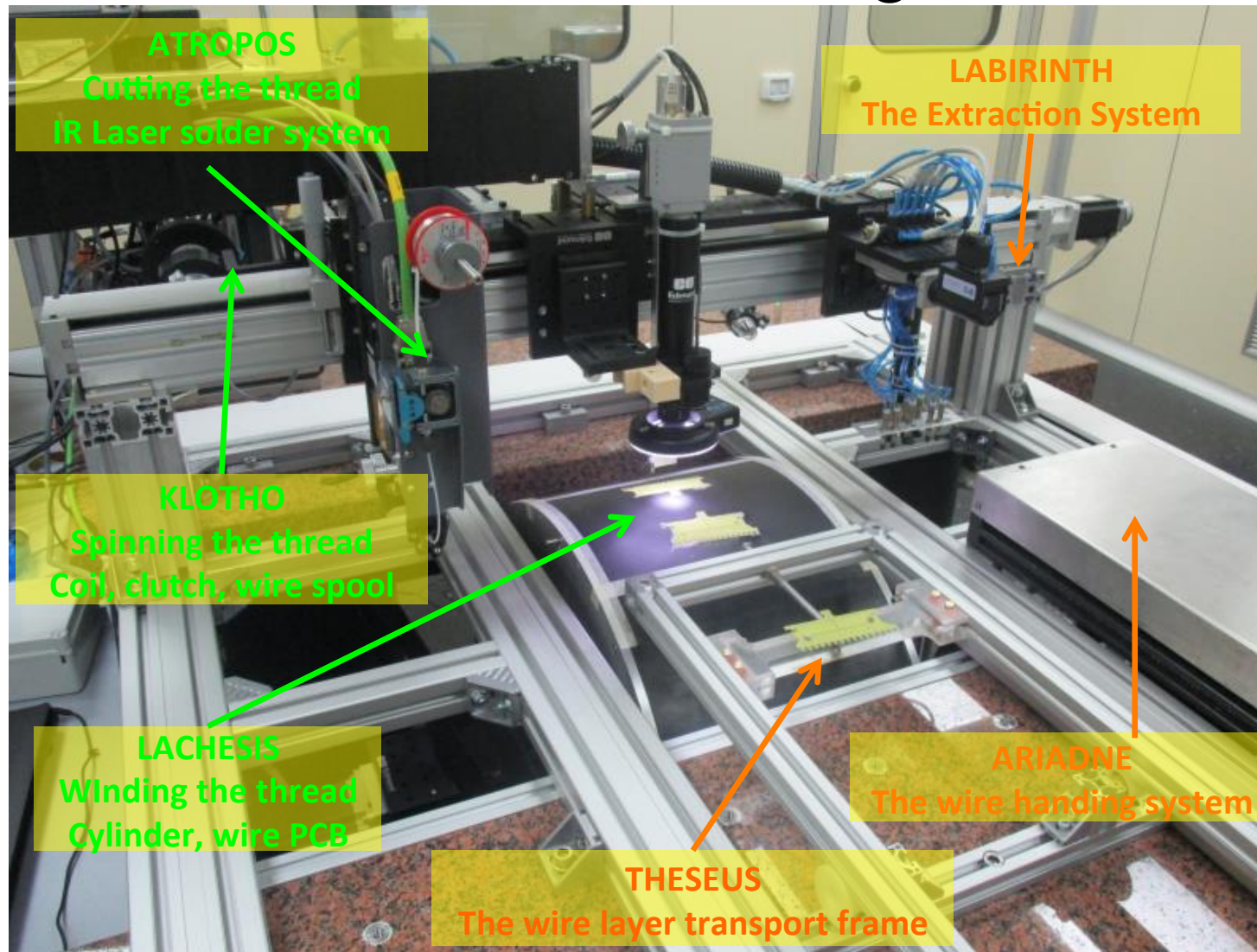
scale 1:1
model
to verify
validity
of principle



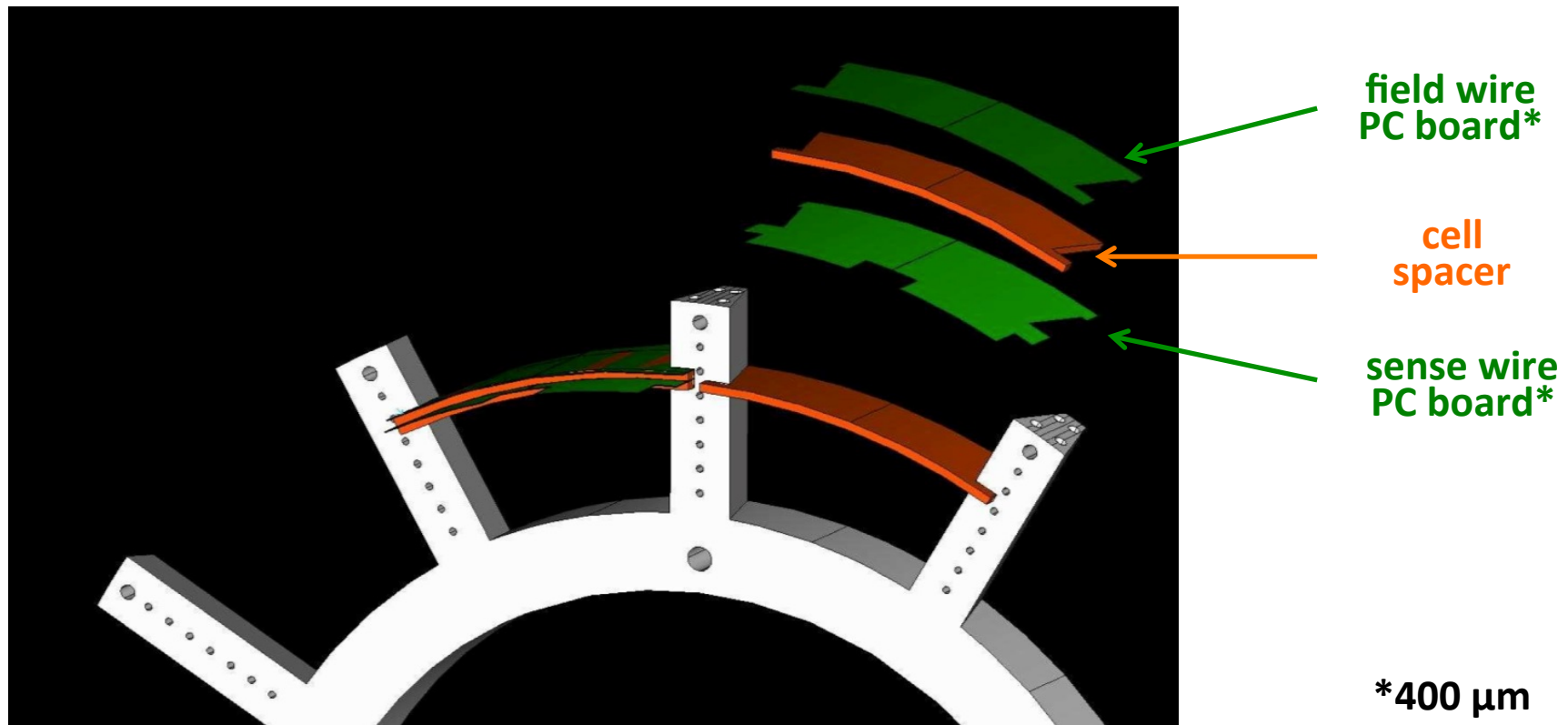
Wire Cage

- This scheme does not require **wire feed-through** thus allowing for denser wire spacing, i.e. **smaller cells** (finer chamber granularity) and for **larger field to sense wires ratios**.
- **Larger field to sense wires ratio** and, therefore, **thinner field wires**, help reducing **multiple scattering contribution** and **total wire tension** on support structure.
- Large number of wires and small cells, however, require complex and cumbersome **assembly procedures**, which call for a **novel approach** to the wiring problem.

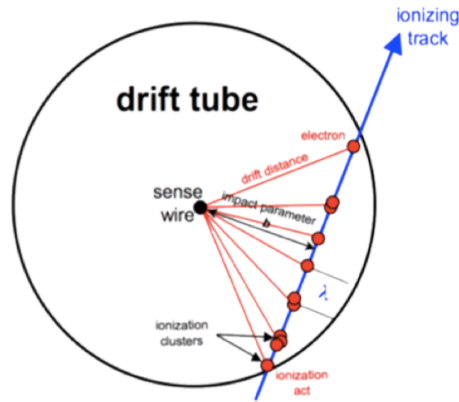
The MEG2 DC approach: **OLIMPUS:** the wiring robot



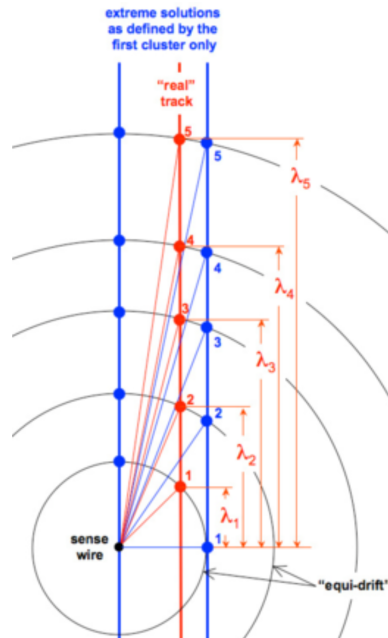
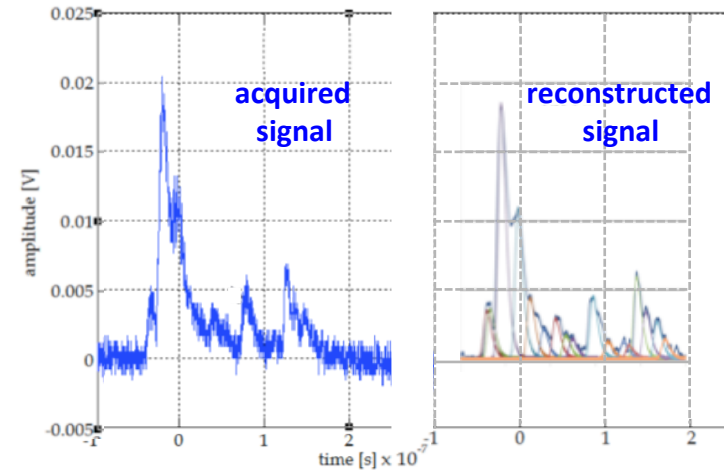
MEG2 DC (under construction) wire support structure



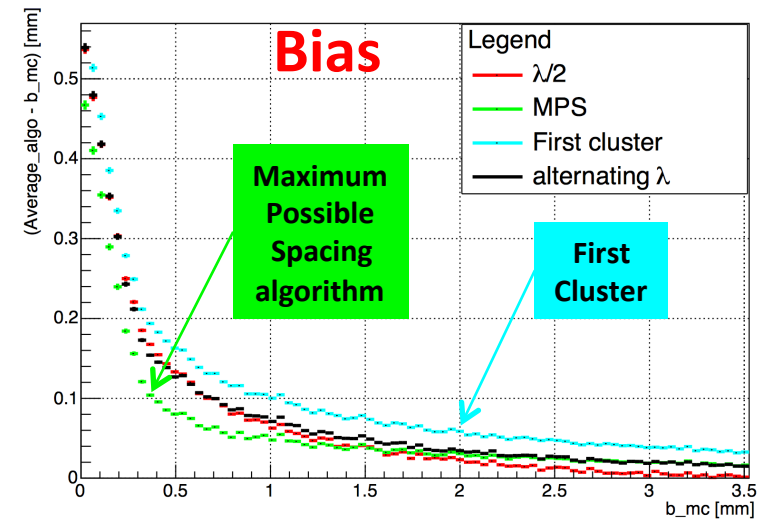
Cluster Timing



From the **ordered sequence of the electrons arrival times**, considering the average time separation between clusters and their time spread due to diffusion, **reconstruct the most probable sequence of clusters drift times**: $\{t_i^{cl}\} \quad i = 1, N_{cl}$

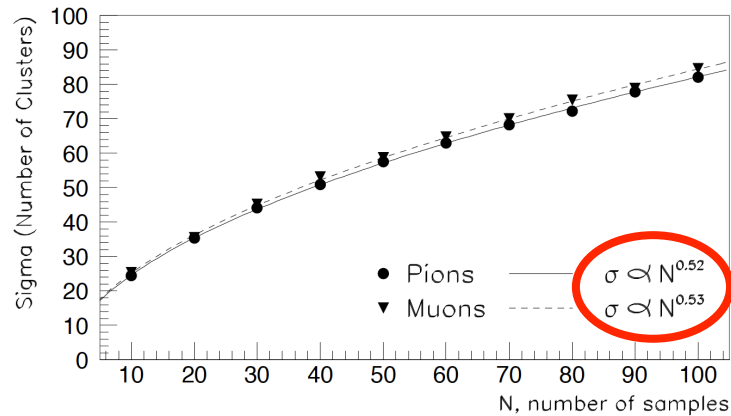


For any given first cluster (FC) drift time, the **cluster timing technique** exploits the drift time distribution of all successive clusters $\{t_i^{cl}\}$ to determine the most probable impact parameter, thus reducing the **bias** and the average **drift distance resolution** with respect to those obtained from with the FC method alone.

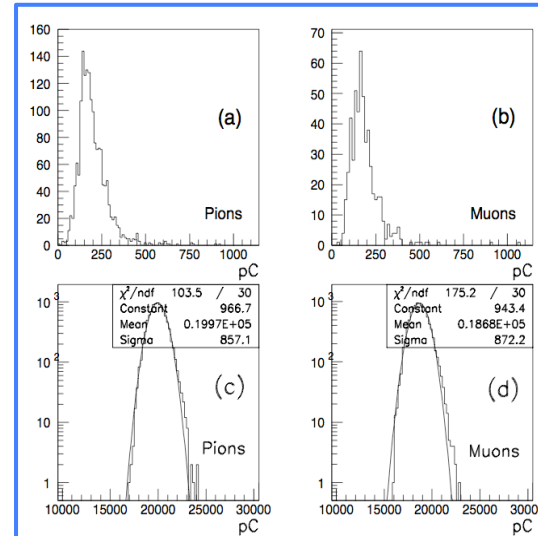


Cluster Counting

Thanks to the **Poisson nature of the ionization process**, by counting the total number of ionization clusters N_{cl} along the trajectory of a charged track, for all the hit cells, one can reach a relative resolution of $N_{cl}^{-1/2}$.



The data taken with a beam of μ and π at 200 MeV/c momentum at PSI, refer to a gas mixture $\text{He}/i\text{C}_4\text{H}_{10}=95/5$, $N_{cl} = 9/\text{cm}$, 100 samples, 2.6cm each at 45° (to avoid space charge effects), for a total track length of 3.7 m. A 25 μm sense wire (gas gain 2×10^5), readout through a high bandwidth (1.7 GHz, gain 10) preamplifier, is digitized with a 2 GSa/s 1.1 GHz, 8 bits digital scope. (NIM A386 (1997) 458-469 and references therein)

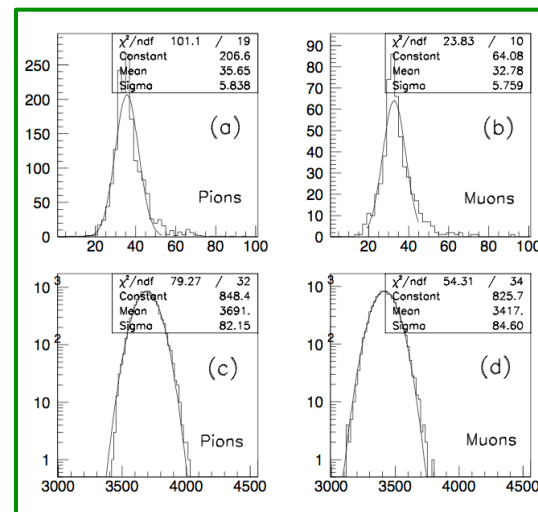


dE/dx

100 samples 3.7 cm
 $(\sigma[\%]=40.7 n^{-0.43} L[\text{m}]^{-0.32})$
 $\sigma = 3.7\%$
 $\approx 2.0\sigma$ separation

20% truncated mean
 $\sigma = 4.5\%$
 $\approx 1.4\sigma$ separation

$\mu-\pi$ 200 MeV/c



dN_{cl}/dx

Poisson distribution
 $\sigma = 1.7\%$
 $\approx 5\sigma$ separation

Experimental distribution
 $\sigma = 2.5\%$
 $\approx 3.2\sigma$ separation
 $\mu-\pi$ 200 MeV/c

"Innovative DC" advantages

- **Gas containment** – **wire support** separation and **feed-through-less wiring**
 - allow to reduce material to $\approx 10^{-3} X_0$ for the inner cylinder and to a few $\times 10^{-2} X_0$ for the end-plates, including FEE, HV supply and signal cables ($1.5 \times 10^{-3} X_0$ and $8 \times 10^{-3} X_0$, respectively, for the Mu2e proposal).
- **Feed-through-less wiring**
 - allows to increase **chamber granularity** and field/sense wire ratio to reduce **multiple scattering** and **total tension on end plates** due to wires
- **Cluster timing**
 - allows to reach **spatial resolution** $< 100 \mu\text{m}$ for 8 mm drift cells in He based gas mixtures (such a technique is going to be implemented in the MEG2 drift chamber under construction)
- **Cluster counting**
 - allows to reach **dN_{cl}/dx resolution** $< 3\%$ for particle identification (a factor 2 better than dE/dx)

Recipe for cluster timing/counting in He based gas mixtures:

FEE: 1 GHz BW, x20 gain (S/N ratio ≈ 10) - digitizer: 2 GSa/s sampling rate, >8 bits

A proposal for CepC (1)

- **24 super-layers**, each one made of **8 para-axial layers (192 total)** at alternating sign stereo angles, arranged in **16 equal azimuthal sectors**;
- **18 square, single sense wire, drift cells** per sector (288 total) on first super-layer with 3 cells increment per sector on each successive super-layer to keep cell size constant as a function of super-layer radius;
- **Cell sizes** ranging from **7.2 mm to 8.7 mm** along r and z;
- **Alternating sign stereo angles** in consecutive layers ranging from **32 to 187 mrad** (constant azimuthal angular displacement)
- **Length: 4000 mm**; fully efficient up to **$\cos\theta=0.975$** (>16 hit)
- **Inner Wall**: made of 25 μm of Kapton plus 0.1 μm of Au (**$1.2\times 10^{-4} X_0$**) at **Radius = 320 mm**;
- **Outer Wall**: Sandwich of 4-ply C-fiber (0° and 90°, total of 250 μm) - 2.5 mm Rohacell30 - 4-ply C-fiber (**$4.2\times 10^{-3} X_0$**) at **Radius = 1950 mm** (must support **15 Tons** - check for buckling over 4 m);
- **End plates:**
 - **Wire cage** (in analogy to Mu2e I-Tracker):
0.6 g/cm² - **$2\times 10^{-2} X_0$** (incl. power distr., decoupling C's, term. resistors and signal and HV cables).
 - **Gas envelope** made of 6 ply (quasi-isotropic, 6 \times 38 μm = 228 μm) C-fiber plus 0.3 μm Au, for a total of 0.060 g/cm² – **$2.1\times 10^{-3} X_0$** ;
- **Gas: 90% He - 10% iC₄H₁₀** ($\delta = 4\times 10^{-4}$ g/cm³, $X_0 = 1410$ m), - 12.5 p.i./cm, gas gain: 4×10^5 at $V \approx 1400$ V on 20 μm wire, $v_{\text{drift}} \sim 2.5$ cm/ μs - **$4.7\times 10^{-4} X_0/1\text{m track}$**
- **Wires:** - **161,280 sense** (20 μm Sn coated Ti); **648,480 field** (40 μm Sn coated C); **164,640 guard** (50 μm Sn coated Al) for a total equivalent thickness of **$9.8\times 10^{-4} X_0/1\text{m track}$**

Expected spatial resolution

Expected Performance: Track parameters resolutions

$n = 192$, $B = 3.5$ T, $R_{out} = 1.95$ m, $L = 2.0$ m or $2.8 \times 10^{-3} X_0$, $\sigma_{xy} = 100$ μm , $\sigma_z = 1.0$ mm

measurement

$$\frac{\Delta p_{\perp}}{p_{\perp}} = \frac{8\sqrt{5}\sigma}{3BL^2\sqrt{n}} p_{\perp} = 3.1 \times 10^{-5} p_{\perp} [\text{GeV}/c]$$

$$\Delta\phi_0 = \frac{4\sqrt{3}\sigma}{R_{out}\sqrt{n}} = 3.2 \times 10^{-5}$$

$$\Delta\theta = \frac{\sqrt{12}\sigma_z}{R_{out}\sqrt{n}} \frac{1 + \tan^2 \theta}{\tan^2 \theta} = 1.6 \times 10^{-4} \frac{1 + \tan^2 \theta}{\tan^2 \theta}$$

multiple scattering (gas + wires)

$$\frac{\Delta p_{\perp}}{p_{\perp}} = \frac{0.0523 [\text{GeV}/c]}{\beta p B L \sin \theta} \sqrt{\frac{L}{X_0}} = \frac{3.4 \times 10^{-4} [\text{GeV}/c]}{\beta p \sin \theta}$$

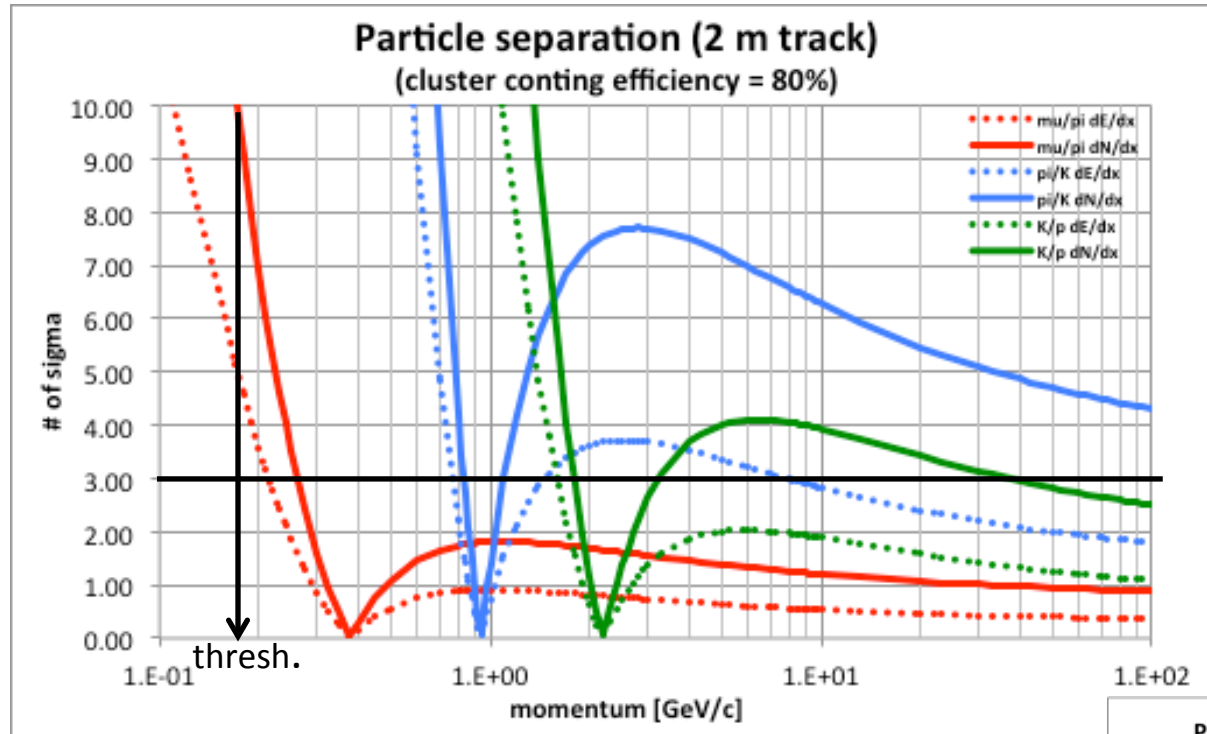
$$\Delta\phi_0 = \frac{13.6 \times 10^{-3} [\text{GeV}/c]}{\beta p} \sqrt{\frac{L}{X_0}} = \frac{7.2 \times 10^{-4} [\text{GeV}/c]}{\beta p}$$

$$\Delta\theta = \frac{13.6 \times 10^{-3} [\text{GeV}/c]}{\beta p} \sqrt{\frac{L}{X_0}} = \frac{7.2 \times 10^{-4} [\text{GeV}/c]}{\beta p}$$

$$\frac{\Delta p_{\perp}}{p_{\perp}} = 2.2 \times 10^{-4}; \quad \frac{\Delta p}{p} = \frac{\Delta p_{\perp}}{p_{\perp}} \oplus \frac{\Delta\theta}{\tan \theta} = 4.0 \times 10^{-4}$$

for $p = 10$ GeV/c and $\theta = 45^\circ$

Expected p. id. capabilities



$$\sigma_{dE/dx/dE/dx} = 5.4 L[m]^{-0.37} \%$$

(Lehraus parametrization)

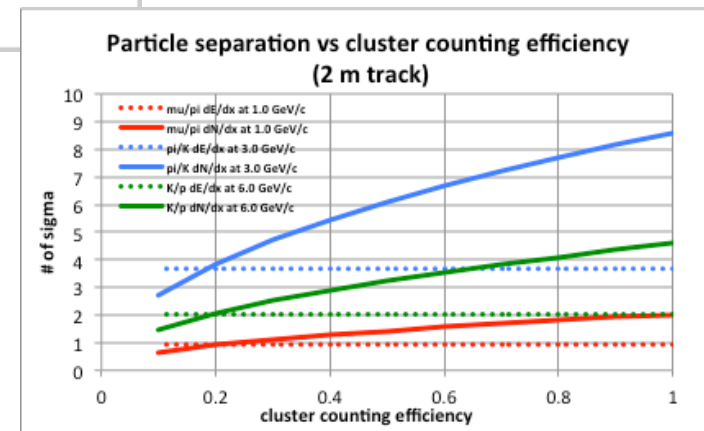
4.2% for L=2m

cluster counting efficiency

$$\varepsilon = 80\%$$

$$\sigma_{dN_{cl}/dx/dN_{cl}/dx} = \varepsilon \times L \times 12.5/\text{cm} = 2.2\% \text{ for } L=2\text{m}$$

Particle separation power as a function of cluster counting efficiency for 2m tracks.
Cluster counting outperforms dE/dx for counting efficiencies as low as 20%.



Conclusions

- We propose for CepC an innovative tracking system based on a **"ultra-light drift chamber with peculiar particle identification capabilities"** using cluster timing/counting techniques.
- It consists of a full stereo, single sense wire, small size square cells:
 - $R_{in} = 32 \text{ cm}$; $R_{out} = 195 \text{ cm}$; $L = 400 \text{ cm}$; **192 layers \times 8.2 mm; 160,000 cells**; >16 hits (90% efficiency) down to **$\cos\vartheta = 0.975$** ; stereo angles ranging from **32 mrad to 187 mrad**;
 - Inner cylindrical wall: **$1.2 \times 10^{-4} X_0$**
 - Outer cylindrical wall: **$4.2 \times 10^{-3} X_0$**
 - End plates (fully instrumented): **$2.2 \times 10^{-2} X_0$**
 - Gas + wires: **$4.7 \times 10^{-4} X_0/\text{1m track} + 9.8 \times 10^{-4} X_0/\text{1m track}$**
- Expected spatial resolutions: **$\sigma_{r\varphi} < 100 \mu\text{m}$, $\sigma_z < 1 \text{ mm}$**
- Expected momentum resolution: **$\Delta p_t/p_t = 2.2 \times 10^{-4}$, $\Delta p/p = 4.0 \times 10^{-4}$** for $p=10\text{GeV}/c$ and $\vartheta=45^\circ$
- Expected p. id.: π/κ separation **$> 3\sigma$ for $p < 820 \text{ MeV}/c$ and $p > 1100 \text{ MeV}/c$**

At current status of art: it doesn't need any major R&D

Back up slides

solid state drawbacks (1)

- multiple scattering

- Si detector + electronics + cooling + mechanical supports amounts to $> 5\% X_0$ per layer, for a total of $> 25\% X_0$ in the barrel region and $> 30\% X_0$ in the end-cap region, in front of the electromagnetic calorimeters (from SiD at ILC)

- redundancy

- despite the excellent space resolution ($\sigma \approx 10 \mu\text{m}$) per layer, only a limited number ($N \approx 5$) of layers can be implemented, for a momentum resolution $\propto \frac{\sigma}{\sqrt{N}}$, equivalent to a gas tracker ($\sigma \approx 100 \mu\text{m}$ and $N \approx 200$).
- However, because of the small N , it suffers from lack of redundancy, against inefficiencies and background hits, and high combinatorial for pattern recognition

solid state drawbacks (2)

- **number of channels and cost**

- necessary of the order of 30 million channels (SiD at ILC) for only 5 space points with a leverage compatible with the momenta to be measured
- implications on system complexity, cost, power consumption, ...

- **alignment**

- relative alignment at the level of $< 5 \mu\text{m}$ among the many staves, the barrel layers and the forward planes constituting the tracker
- absolute alignment with inner vertex detector and beam axis at same level
- stability of alignment parameters w.r.t. temperature, CO_2 cooling flow, mechanical vibrations, ...

- **particle identification**

- no particle identification possible

TPC drawbacks (1)

- **gas mixture**

- at $v_{\text{drift}} = 5 \text{ cm}/\mu\text{s}$, total drift time $\approx 50 \mu\text{s}$, integrating ≈ 15 bunch crossings (occupancy at low p_t : curling for $170 < p_t < 950 \text{ MeV}/c$).
- $\Delta v_{\text{drift}}/v_{\text{drift}} \approx 1\%/10 \text{ ppm (H}_2\text{O)}$!
- attachment (O_2 , electronegative impurities $< \text{a few ppm!}$)?

- **positive ions backflow**

- no sufficiently efficient gating strategy envisioned yet for a continuous beam, leading to large track distortions.
- ion space charge density affects ion backflow even in triple GEM configuration, particularly at smaller radii.

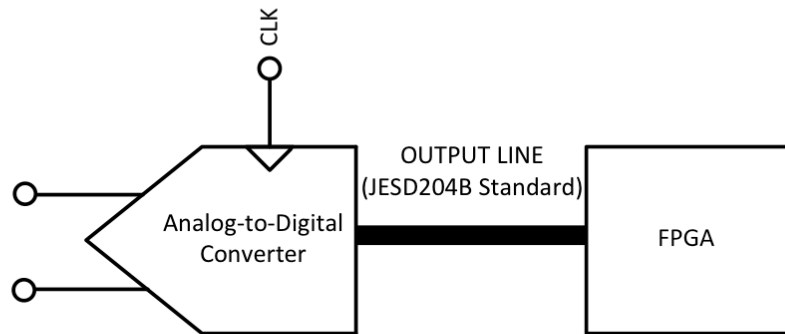
- **alignment**

- relative alignments must be below $50 \mu\text{m}$ (\ll distortion corrections).

TPC drawbacks (2)

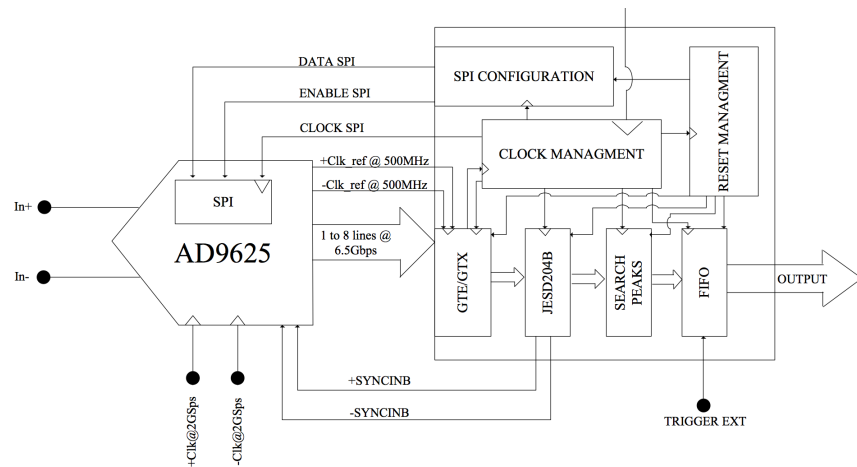
- **number of readout channels**
 - expected point resolution requires readout pad sizes of a few mm² for a total of millions of channels per endplate ($\approx 10 \text{ m}^2$).
- **power consumption**
 - even at 10 mW/ch (ALICE TPC: 40 mW/ch), tens of kW per end plate necessary (no power pulsing like ILC) requiring sophisticated cooling systems (more material in front of the end-cap calorimeter).
- **multiple scattering**
 - end plates must support field cage, MPGD readout system, cooling system, power and FEE cables: hard to keep equivalent end plates thickness in front of the electromagnetic calorimeter below $30\% X_0$.

BLOCK DIAGRAM



CLUSTER TIMING/COUNTING PROTOTYPE READOUT SCHEME

- **Analog to Digital Converter:** Analog Devices AD9625
 - Sampling frequency: 2.0 GSPS
 - Resolution: 12 bits
 - Supply voltage: 1.3V, 2.5
- **FPGA:** Virtex 6 xc6vlx240t-1ff1156



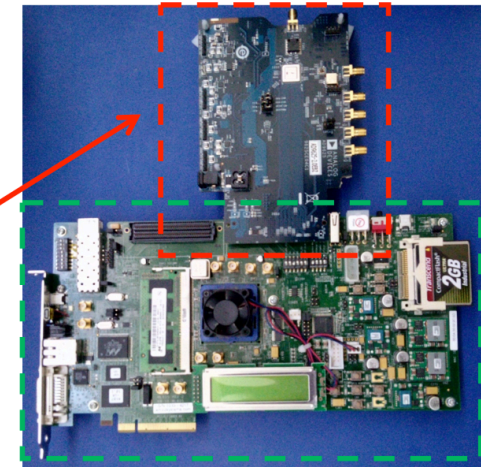
EVALUATION BOARDS USED

AD9625 evaluation board:
AD9625-2.0EBZ ⁽⁴⁾

**xc6vlx240t-1ff1156
evaluation board:**
UG534 ML605 ⁽⁵⁾

AD9625-2.0EBZ

UG534 ML605



⁽⁴⁾ <http://www.analog.com/en/design-center/evaluation-hardware-and-software/evaluation-boards-kits/eval-ad9625.html#eb-overview>
⁽⁵⁾ http://www.xilinx.com/support/documentation/boards_and_kits/ug534.pdf