

Higgs Searches: A Status Report

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- The procedure for doing the statistics is defined by;

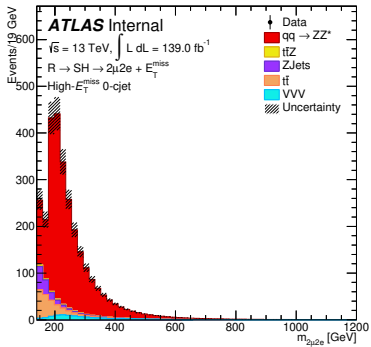
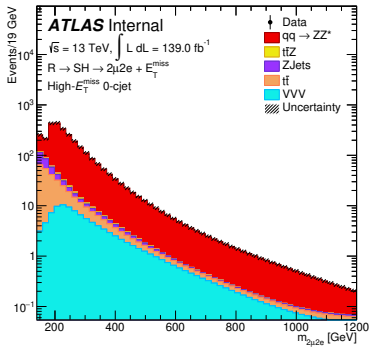
$$\mathcal{L}(x_1 \dots x_n | \sigma_{ggRSH}) = \text{Pois}(n | S + B) \times \left[\prod_{i=1}^n \frac{S \cdot f_S(x_i) + B \cdot f_B(x_i)}{S + B} \right]$$

$$S = \sigma_{ggRSH} \times \text{BR}(H \rightarrow ZZ \rightarrow 4\ell) \cdot \text{AC} \int L$$

Update on $R \rightarrow SH \rightarrow 4\ell + E_T^{miss}$ analysis

Statistics strategy

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Thank you!



Signal samples have already been produced, [JIRA](#), as follows:

- ☐ The mass of S is fixed to 160 GeV;
- ☐ The masses of R are 390 GeV, 450 GeV, 800 GeV and 1500 GeV:
 - $m_R = 390$ GeV: $m_H = 220$ GeV
 - $m_R = 450$ GeV: $m_H = 220$ GeV and 250 GeV
 - $m_R = 800$ GeV: $m_H = 220$ GeV, 300 GeV and 500 GeV
 - $m_R = 1500$ GeV: $m_H = 220$ GeV, 250 GeV and 1000 GeV
- ☐ Requested HIGG2D1 derivation with cache: 21.2.55 and p-tag: p3782. All jobs are finished see [here](#); and
- ☐ The mini-tree production is done using [HZZAnalRun2Code](#).

Background samples

- ☐ $qqZZ^*$, $ggZZ^*$, $t\bar{t}Z$, $Z + jets$, $t\bar{t}$ and VVV .

- Signal and background are mc16a, mc16d and mc16e combined;
- The signal cross section ($xsection \times BR$) is 1 fb^{-1} (set by hand);
- The significance is calculated using $S/\sqrt{S+B}$ and $S/\sqrt{B}$;
- S , and B are the signal and background event, respectively;
- Background events are normalised to cross section for the $m_{4\ell} > 200 \text{ GeV}$;
- Scaling background events by 20.3% uncertainty. It's calculated as follow:

The background scaled by a number extracted as follows: For instance, for $m_H = 220$, and $m_R = 390$: events in $m_{4\ell}(210 - 230) \text{ GeV}$ over the full range of $m_{4\ell}(> 200) \text{ GeV}$.

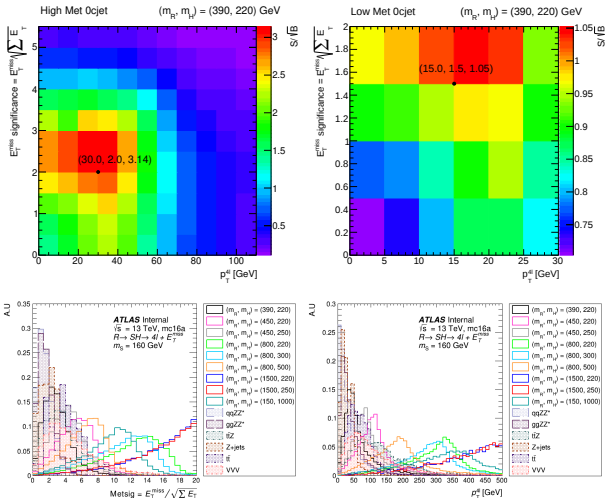
Event Selection	
QUADRUPLET SELECTION	- Require at least one quadruplet of leptons consisting of two pairs of same-flavour opposite-charge leptons fulfilling the following requirements: - p_T thresholds for three leading leptons in the quadruplet: 20, 15 and 10 GeV - At most 1 calo-tagged, stand-alone or silicon-associated muon per quadruplet - Leading di-lepton mass requirement: $50 < m_{12} < 106$ GeV - Sub-leading di-lepton mass requirement: $m_{\text{threshold}} < m_{34} < 115$ GeV - $\Delta R(\ell, \ell') > 0.10$ for all lepton pairs in the quadruplet - Remove quadruplet if alternative same-flavour opposite-charge di-lepton gives $m_{\ell\ell} < 5$ GeV - Keep all quadruplets passing the above selection
ISOLATION NEEDS UPDATING	- Contribution from the other leptons of the quadruplet is subtracted - Muon track isolation ($\Delta R = 0.30$): $\Sigma p_T/p_T < 0.15$ - Muon calorimeter isolation ($\Delta R = 0.20$): $\Sigma E_T/p_T < 0.30$ - Electron track isolation ($\Delta R = 0.20$): $\Sigma E_T/E_T < 0.15$ - Electron calorimeter isolation ($\Delta R = 0.20$): $\Sigma E_T/E_T < 0.20$
IMPACT PARAMETER SIGNIFICANCE	- Apply impact parameter significance cut to all leptons of the quadruplet - For electrons: $d_0/\sigma_{d_0} < 5$ - For muons: $d_0/\sigma_{d_0} < 3$
BEST QUADRUPLET	- If more than one quadruplet has been selected, choose the quadruplet with highest Higgs decay ME according to channel: 4μ, $2e2\mu$, $2\mu 2e$ and $4e$
VERTEX SELECTION	- Require a common vertex for the leptons: - $\chi^2/\text{ndof} < 5$ for 4μ and < 9 for others decay channels

Update on $R \rightarrow SH \rightarrow 4\ell + E_T^{miss}$ analysis

Signal optimisation

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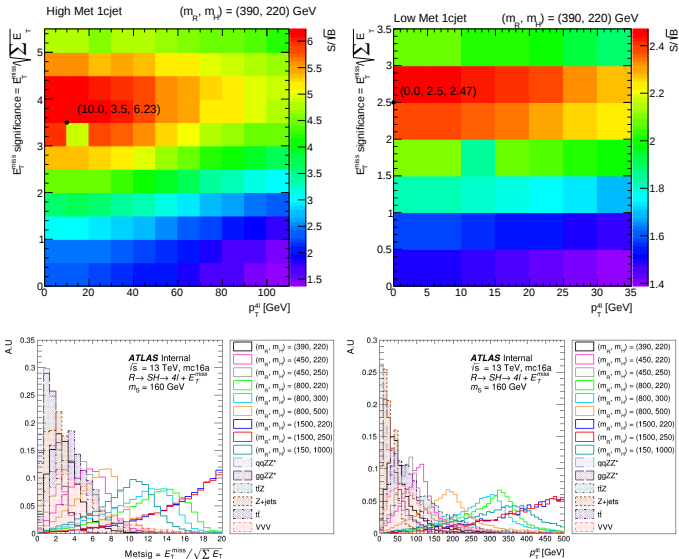
- Categorize event into 4 categories: Using $S/\sqrt{B}$ instead of $S/\sqrt{S+B}$ to avoid the cross-section dependency



Update on $R \rightarrow SH \rightarrow 4\ell + E_T^{miss}$ analysis

Signal optimisation

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Update on $R \rightarrow SH \rightarrow 4\ell + E_T^{\text{miss}}$ analysis

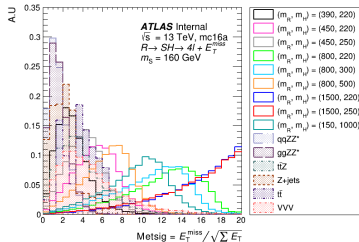
Summary of the signal optimisation

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Remark

- We avoid the dependency of the cross-section by using $S/\sqrt{B}$. For the optimisation we used only $(m_R, m_H) = (390, 220)$ GeV mass point. So no need to use other mass points because the new categories cover the low and the high Met region.

- ☐ High met 0 central jet $\Rightarrow 30 \setminus 2.0$
- ☐ Low met 0 central jet $\Rightarrow 15 \setminus 1.5$
- ☐ High met 1 central jet $\Rightarrow 10 \setminus 3.5$
- ☐ Low met 1 central jet $\Rightarrow 0.0 \setminus 2.5$



See tables for the categories on backup slides.

Update on $R \rightarrow SH \rightarrow 4\ell + E_T^{\text{miss}}$ analysis

Signal acceptance

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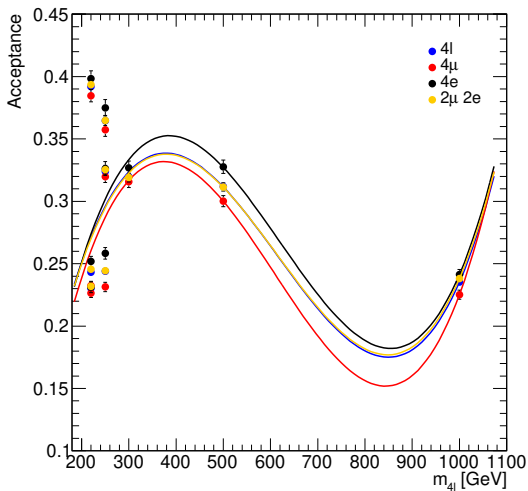
(m_R, m_H) GeV	4ℓ	4μ	$4e$	$2\mu 2e$
390, 220	23.01%	22.65%	23.11%	23.19%
450, 220	39.18%	38.46%	39.84%	39.34%
450, 250	36.46%	35.72%	37.50%	36.49%
800, 220	32.39%	31.97%	32.63%	32.53%
800, 300	31.97%	31.57%	32.67%	31.91%
800, 500	31.18%	30.01%	32.76%	31.15%
1500, 220	24.32%	23.24%	25.18%	24.56%
1500, 250	24.39%	23.14%	25.83%	24.44%
1500, 1000	23.53%	22.52%	24.13%	23.81%

Table: Signal efficiencies for the $4\ell + E_T^{\text{miss}}$ final states. The numbers recovered with simulated MC of mc16a, mc16d and mc16e for the High- E_T^{miss} with zero central jet category. For the signal masses (m_R, m_H) of (390,220), (450,220), (450,250), (800, 220), (800, 300), (800, 500), (1500, 220), (1500, 220), and (1500, 1000) GeV. The efficiency is calculated by the ratio of the number of reconstructed events after all pre-selection requirements to the number of simulated events after the final selection the for inclusive lepton channel (4ℓ)

Update on $R \rightarrow SH \rightarrow 4\ell + E_{\text{T}}^{\text{miss}}$ analysis

Signal acceptance

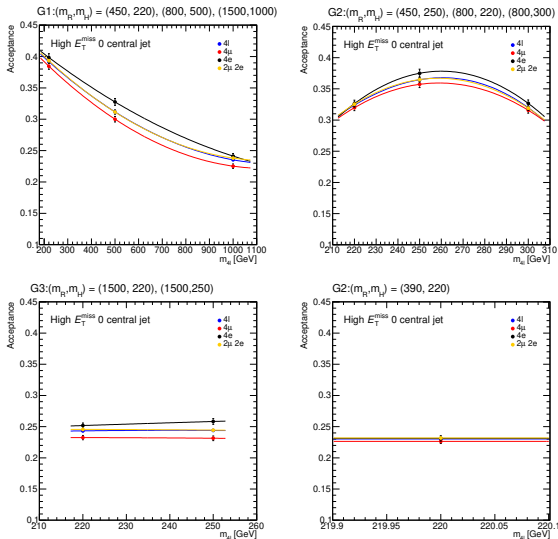
12



Update on $R \rightarrow SH \rightarrow 4\ell + E_T^{miss}$ analysis

Signal acceptance

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□ The Crystal ball, CB, plus Gaussian, G, Pdf has the following form:

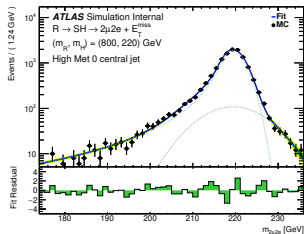
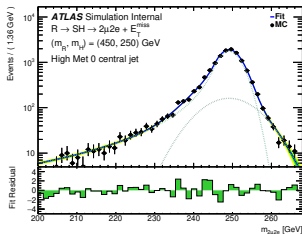
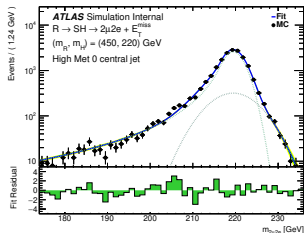
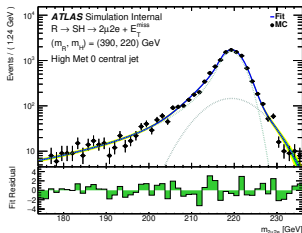
$$f(m_{4\ell}) = f_{\text{CB}} \cdot \text{CB}(m_{4\ell}; \mu, \sigma_{\text{CB}}, \alpha_{\text{CB}}, n_{\text{CB}}) + (1 - f_{\text{CB}}) \cdot \text{G}(m_{4\ell}; \mu, \sigma_{\text{G}})$$

- σ_{CB} and σ_{G} represent the invariant mass resolution;
- μ is the mean value fixed to same parameter for both Pdf;
- n_{CB} and α_{CB} model the shape and position of the non-Gaussian tail;
- Where n_{CB} is the slop of the tail and α_{CB} measures how far from the peak the distribution become non-Gaussian;
- f_{CB} is the relative normalisation of the Pdf.

Update on $R \rightarrow SH \rightarrow 4\ell + E_T^{miss}$ analysis

High Met 0 central jet for $2\mu 2e$ channel

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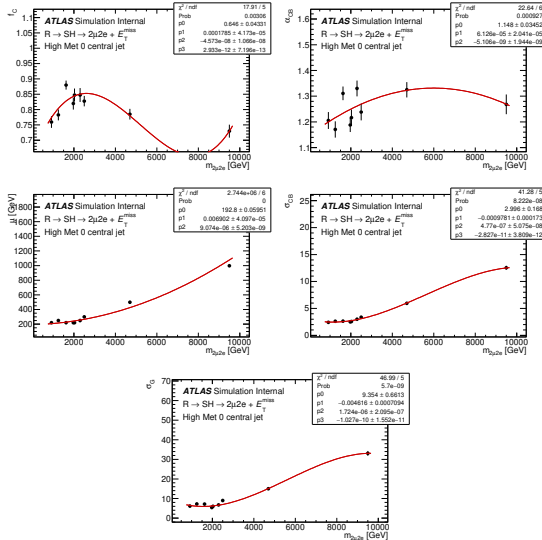


- The samples have more high p_T events will have different resolution of the mass.

Update on $R \rightarrow SH \rightarrow 4\ell + E_T^{miss}$ analysis

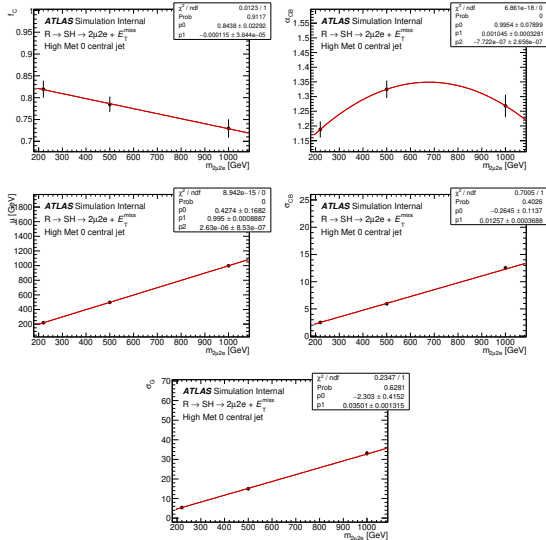
Interpolation of μ , f_{CB} , σ_G , σ_{CB} and α_{CB} parameters

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Update on $R \rightarrow SH \rightarrow 4\ell + E_T^{miss}$ analysis

Interpolation of μ , f_{CB} , σ_G , σ_{CB} and α_{CB} parameters



Update on $R \rightarrow SH \rightarrow 4\ell + E_{\tau}^{miss}$ analysis

Background parametrisation

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$$f^{ggZZ/qqZZ}(m_{4\ell}) = (f_1(m_{4\ell}) + f_2(m_{4\ell})) \times H(m_0 - m_{4\ell}) \times C_0 + f_3^{ggZZ/qqZZ}(m_{4\ell}) \times H(m_{4\ell} - m_0),$$

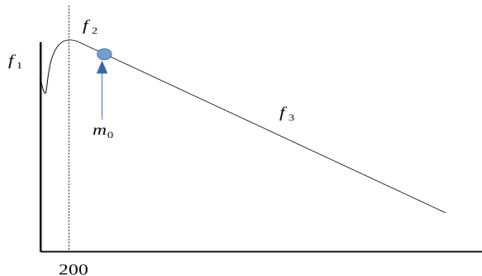
where:

$$f_1(m_{4\ell}) = \exp(a_1 + a_2 \cdot m_{4\ell} + a_3 \cdot m_{4\ell}^2),$$

$$f_2(m_{4\ell}) = \left\{ \frac{1}{2} + \frac{1}{2} \operatorname{erf} \left(\frac{m_{4\ell} - b_1}{b_2} \right) \right\} \times \frac{1}{1 + \exp \left(\frac{m_{4\ell} - b_1}{b_3} \right)},$$

$$f_3^{qqZZ/ggZZ}(m_{4\ell}) = \exp \left(c_1 + c_2 \cdot m_{4\ell} + c_3 \cdot m_{4\ell}^2 + c_4 \cdot m_{4\ell}^3 + c_5 \cdot m_{4\ell}^4 + c_6 \cdot m_{4\ell}^5 \right),$$

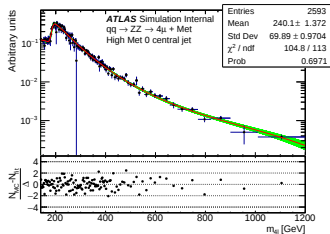
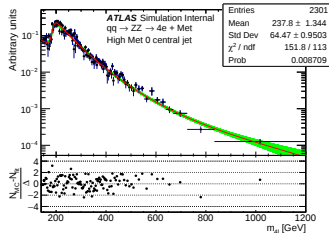
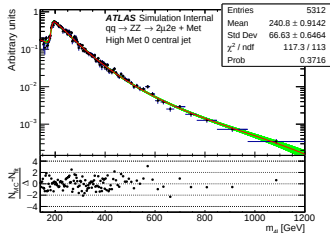
$$C_0 = \frac{f_3(m_0)}{f_1(m_0) + f_2(m_0)}.$$



Update on $R \rightarrow SH \rightarrow 4\ell + E_{\text{T}}^{\text{miss}}$ analysis

Background parametrisation

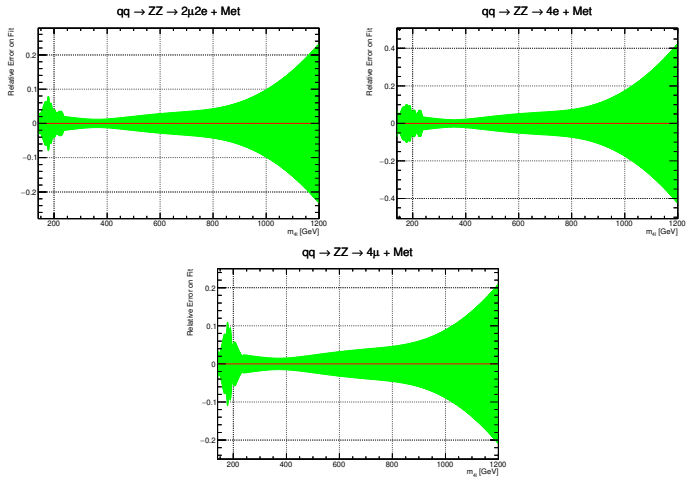
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Update on $R \rightarrow SH \rightarrow 4\ell + E_{\text{T}}^{\text{miss}}$ analysis

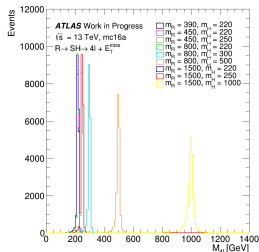
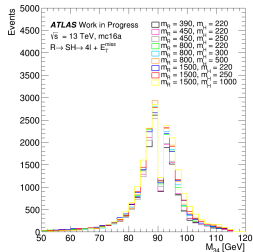
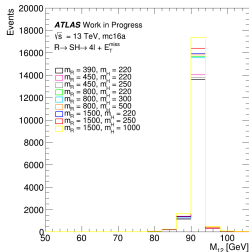
Background parametrisation

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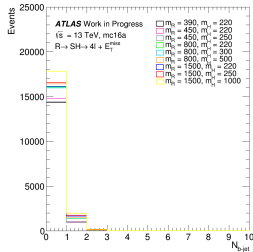
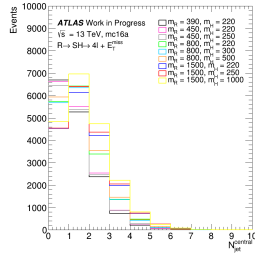
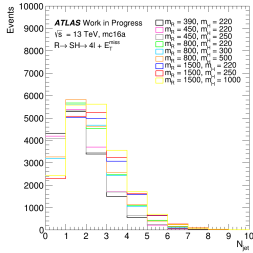
Additional slides

Kinematic distributions for the signal



Additional slides

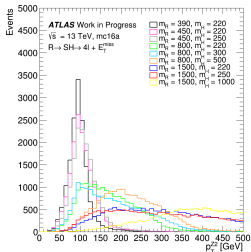
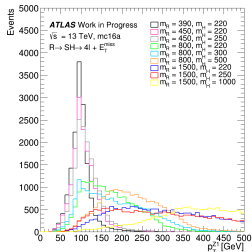
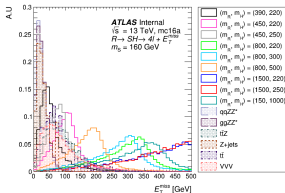
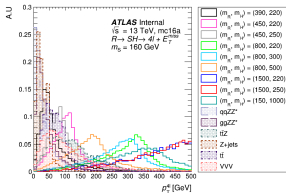
Kinematic distributions for the signal



Additional slides

Kinematic distributions for the signal

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Additional slides

Kinematic distributions for signal & background

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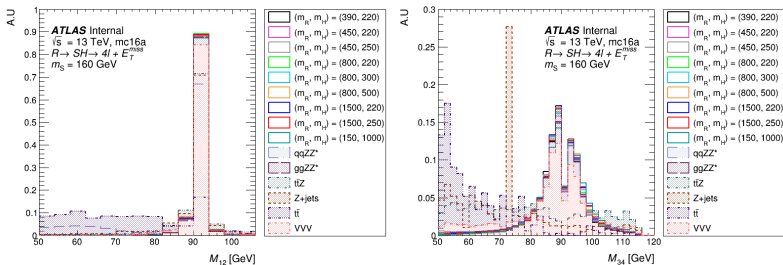


Figure: The invariant mass of the first (left) and the second (right) lepton pairs.

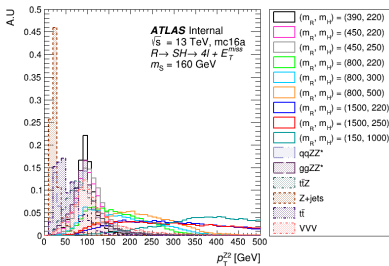
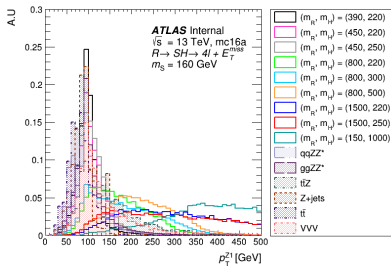
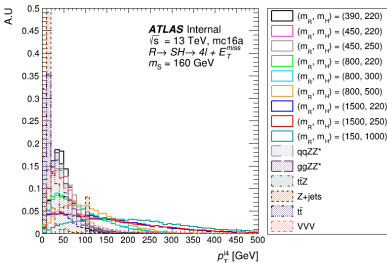
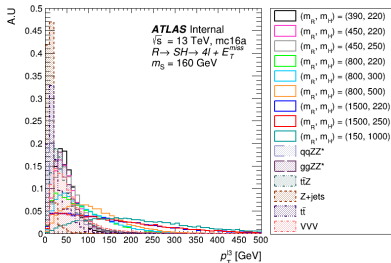
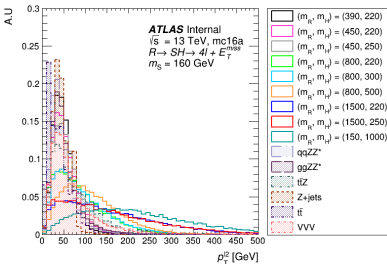
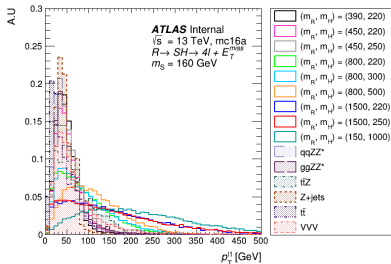


Figure: The invariant mass of the first (left) and the second (right) lepton pairs.

Additional slides

Kinematic distributions

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Additional slides

High Met O central jet

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	[GeV, mV]	[200, 200]	muC1	muC2	muZ	Z, mu	3,5,5,5,5	3,5,5,5,5	3,5,5,5,5	3,5,5,5,5	3,5,5,5,5	3,5,5,5,5
0-10	64.51-0.24	2010.45-5.75	349.64-0.91	0.94-0.00	0.87-0.04	3.55-0.23	19.08-0.11	1.991				
10-20	66.07-0.20	2394.86-5.97	394.96-0.99	1.72-0.02	2.88-0.04	3.22-0.15	17.78-0.11	2.560				
20-30	66.97-0.19	2697.81-5.99	411.64-0.95	0.42-0.01	2.14-0.03	3.40-0.14	17.86-0.11	1.763				
30-40	67.00-0.19	2802.00-6.00	460.36-1.00	0.42-0.00	2.10-0.00	3.50-0.10	19.30-0.10	1.613				
40-50	67.00-0.19	2947.47-0.60	536.12-0.60	0.41-0.00	1.98-0.00	3.54-0.00	19.54-0.00	1.453				
50-60	67.00-0.19	3045.30-0.60	617.63-0.60	0.40-0.00	1.92-0.00	3.59-0.00	19.77-0.00	1.360				
60-70	67.00-0.19	3250.60-0.60	742.26-0.60	0.38-0.00	1.97-0.00	3.70-0.00	19.78-0.00	1.190				
70-80	67.00-0.19	3436.00-0.60	866.12-0.60	0.36-0.00	1.93-0.00	3.78-0.00	19.80-0.00	1.060				
80-90	67.00-0.19	3616.00-0.60	974.00-0.60	0.35-0.00	1.90-0.00	3.80-0.00	19.80-0.00	0.950				
90-100	67.00-0.19	3784.00-0.60	1074.00-0.60	0.34-0.00	1.88-0.00	3.80-0.00	19.80-0.00	0.850				
100-110	67.00-0.19	3944.00-0.60	1166.00-0.60	0.33-0.00	1.87-0.00	3.80-0.00	19.80-0.00	0.760				
110-120	67.00-0.19	4094.00-0.60	1250.00-0.60	0.32-0.00	1.86-0.00	3.80-0.00	19.80-0.00	0.680				
120-130	67.00-0.19	4234.00-0.60	1326.00-0.60	0.31-0.00	1.85-0.00	3.80-0.00	19.80-0.00	0.610				
130-140	67.00-0.19	4364.00-0.60	1394.00-0.60	0.30-0.00	1.84-0.00	3.80-0.00	19.80-0.00	0.550				
140-150	67.00-0.19	4484.00-0.60	1454.00-0.60	0.29-0.00	1.83-0.00	3.80-0.00	19.80-0.00	0.500				
150-160	67.00-0.19	4594.00-0.60	1506.00-0.60	0.28-0.00	1.82-0.00	3.80-0.00	19.80-0.00	0.460				
160-170	67.00-0.19	4694.00-0.60	1550.00-0.60	0.27-0.00	1.81-0.00	3.80-0.00	19.80-0.00	0.430				
170-180	67.00-0.19	4784.00-0.60	1586.00-0.60	0.26-0.00	1.80-0.00	3.80-0.00	19.80-0.00	0.400				
180-190	67.00-0.19	4864.00-0.60	1614.00-0.60	0.25-0.00	1.79-0.00	3.80-0.00	19.80-0.00	0.380				
190-200	67.00-0.19	4934.00-0.60	1634.00-0.60	0.24-0.00	1.78-0.00	3.80-0.00	19.80-0.00	0.360				
200-210	67.00-0.19	4994.00-0.60	1646.00-0.60	0.23-0.00	1.77-0.00	3.80-0.00	19.80-0.00	0.340				
210-220	67.00-0.19	5044.00-0.60	1650.00-0.60	0.22-0.00	1.76-0.00	3.80-0.00	19.80-0.00	0.330				
220-230	67.00-0.19	5084.00-0.60	1654.00-0.60	0.21-0.00	1.75-0.00	3.80-0.00	19.80-0.00	0.320				
230-240	67.00-0.19	5114.00-0.60	1654.00-0.60	0.20-0.00	1.74-0.00	3.80-0.00	19.80-0.00	0.310				
240-250	67.00-0.19	5134.00-0.60	1654.00-0.60	0.19-0.00	1.73-0.00	3.80-0.00	19.80-0.00	0.300				
250-260	67.00-0.19	5144.00-0.60	1654.00-0.60	0.18-0.00	1.72-0.00	3.80-0.00	19.80-0.00	0.290				
260-270	67.00-0.19	5144.00-0.60	1654.00-0.60	0.17-0.00	1.71-0.00	3.80-0.00	19.80-0.00	0.280				
270-280	67.00-0.19	5134.00-0.60	1654.00-0.60	0.16-0.00	1.70-0.00	3.80-0.00	19.80-0.00	0.270				
280-290	67.00-0.19	5114.00-0.60	1654.00-0.60	0.15-0.00	1.69-0.00	3.80-0.00	19.80-0.00	0.260				
290-300	67.00-0.19	5084.00-0.60	1654.00-0.60	0.14-0.00	1.68-0.00	3.80-0.00	19.80-0.00	0.250				
300-310	67.00-0.19	5044.00-0.60	1654.00-0.60	0.13-0.00	1.67-0.00	3.80-0.00	19.80-0.00	0.240				
310-320	67.00-0.19	5004.00-0.60	1654.00-0.60	0.12-0.00	1.66-0.00	3.80-0.00	19.80-0.00	0.230				
320-330	67.00-0.19	4964.00-0.60	1654.00-0.60	0.11-0.00	1.65-0.00	3.80-0.00	19.80-0.00	0.220				
330-340	67.00-0.19	4924.00-0.60	1654.00-0.60	0.10-0.00	1.64-0.00	3.80-0.00	19.80-0.00	0.210				
340-350	67.00-0.19	4884.00-0.60	1654.00-0.60	0.09-0.00	1.63-0.00	3.80-0.00	19.80-0.00	0.200				
350-360	67.00-0.19	4844.00-0.60	1654.00-0.60	0.08-0.00	1.62-0.00	3.80-0.00	19.80-0.00	0.190				
360-370	67.00-0.19	4804.00-0.60	1654.00-0.60	0.07-0.00	1.61-0.00	3.80-0.00	19.80-0.00	0.180				
370-380	67.00-0.19	4764.00-0.60	1654.00-0.60	0.06-0.00	1.60-0.00	3.80-0.00	19.80-0.00	0.170				
380-390	67.00-0.19	4724.00-0.60	1654.00-0.60	0.05-0.00	1.59-0.00	3.80-0.00	19.80-0.00	0.160				
390-400	67.00-0.19	4684.00-0.60	1654.00-0.60	0.04-0.00	1.58-0.00	3.80-0.00	19.80-0.00	0.150				
400-410	67.00-0.19	4644.00-0.60	1654.00-0.60	0.03-0.00	1.57-0.00	3.80-0.00	19.80-0.00	0.140				
410-420	67.00-0.19	4604.00-0.60	1654.00-0.60	0.02-0.00	1.56-0.00	3.80-0.00	19.80-0.00	0.130				
420-430	67.00-0.19	4564.00-0.60	1654.00-0.60	0.01-0.00	1.55-0.00	3.80-0.00	19.80-0.00	0.120				
430-440	67.00-0.19	4524.00-0.60	1654.00-0.60	0.00-0.00	1.54-0.00	3.80-0.00	19.80-0.00	0.110				
440-450	67.00-0.19	4484.00-0.60	1654.00-0.60	0.00-0.00	1.53-0.00	3.80-0.00	19.80-0.00	0.100				
450-460	67.00-0.19	4444.00-0.60	1654.00-0.60	0.00-0.00	1.52-0.00	3.80-0.00	19.80-0.00	0.090				
460-470	67.00-0.19	4404.00-0.60	1654.00-0.60	0.00-0.00	1.51-0.00	3.80-0.00	19.80-0.00	0.080				
470-480	67.00-0.19	4364.00-0.60	1654.00-0.60	0.00-0.00	1.50-0.00	3.80-0.00	19.80-0.00	0.070				
480-490	67.00-0.19	4324.00-0.60	1654.00-0.60	0.00-0.00	1.49-0.00	3.80-0.00	19.80-0.00	0.060				
490-500	67.00-0.19	4284.00-0.60	1654.00-0.60	0.00-0.00	1.48-0.00	3.80-0.00	19.80-0.00	0.050				
500-510	67.00-0.19	4244.00-0.60	1654.00-0.60	0.00-0.00	1.47-0.00	3.80-0.00	19.80-0.00	0.040				
510-520	67.00-0.19	4204.00-0.60	1654.00-0.60	0.00-0.00	1.46-0.00	3.80-0.00	19.80-0.00	0.030				
520-530	67.00-0.19	4164.00-0.60	1654.00-0.60	0.00-0.00	1.45-0.00	3.80-0.00	19.80-0.00	0.020				
530-540	67.00-0.19	4124.00-0.60	1654.00-0.60	0.00-0.00	1.44-0.00	3.80-0.00	19.80-0.00	0.010				
540-550	67.00-0.19	4084.00-0.60	1654.00-0.60	0.00-0.00	1.43-0.00	3.80-0.00	19.80-0.00	0.000				
550-560	67.00-0.19	4044.00-0.60	1654.00-0.60	0.00-0.00	1.42-0.00	3.80-0.00	19.80-0.00	0.000				
560-570	67.00-0.19	4004.00-0.60	1654.00-0.60	0.00-0.00	1.41-0.00	3.80-0.00	19.80-0.00	0.000				
570-580	67.00-0.19	3964.00-0.60	1654.00-0.60	0.00-0.00	1.40-0.00	3.80-0.00	19.80-0.00	0.000				
580-590	67.00-0.19	3924.00-0.60	1654.00-0.60	0.00-0.00	1.39-0.00	3.80-0.00	19.80-0.00	0.000				
590-600	67.00-0.19	3884.00-0.60	1654.00-0.60	0.00-0.00	1.38-0.00	3.80-0.00	19.80-0.00	0.000				
600-610	67.00-0.19	3844.00-0.60	1654.00-0.60	0.00-0.00	1.37-0.00	3.80-0.00	19.80-0.00	0.000				
610-620	67.00-0.19	3804.00-0.60	1654.00-0.60	0.00-0.00	1.36-0.00	3.80-0.00	19.80-0.00	0.000				
620-630	67.00-0.19	3764.00-0.60	1654.00-0.60	0.00-0.00	1.35-0.00	3.80-0.00	19.80-0.00	0.000				
630-640	67.00-0.19	3724.00-0.60	1654.00-0.60	0.00-0.00	1.34-0.00	3.80-0.00	19.80-0.00	0.000				
640-650	67.00-0.19	3684.00-0.60	1654.00-0.60	0.00-0.00	1.33-0.00	3.80-0.00	19.80-0.00	0.000				
650-660	67.00-0.19	3644.00-0.60	1654.00-0.60	0.00-0.00	1.32-0.00	3.80-0.00	19.80-0.00	0.000				
660-670	67.00-0.19	3604.00-0.60	1654.00-0.60	0.00-0.00	1.31-0.00	3.80-0.00	19.80-0.00	0.000				
670-680	67.00-0.19	3564.00-0.60	1654.00-0.60	0.00-0.00	1.30-0.00	3.80-0.00	19.80-0.00	0.000				
680-690	67.00-0.19	3524.00-0.60	1654.00-0.60	0.00-0.00	1.29-0.00	3.80-0.00	19.80-0.00	0.000				
690-700	67.00-0.19	3484.00-0.60	1654.00-0.60	0.00-0.00	1.28-0.00	3.80-0.00	19.80-0.00	0.000				
700-710	67.00-0.19	3444.00-0.60	1654.00-0.60	0.00-0.00	1.27-0.00	3.80-0.00	19.80-0.00	0.000				
710-720	67.00-0.19	3404.00-0.60	1654.00-0.60	0.00-0.00	1.26-0.00	3.80-0.00	19.80-0.00	0.000				
720-730	67.00-0.19	3364.00-0.60	1654.00-0.60	0.00-0.00	1.25-0.00	3.80-0.00	19.80-0.00	0.000				
730-740	67.00-0.19	3324.00-0.60	1654.00-0.60	0.00-0.00	1.24-0.00	3.80-0.00	19.80-0.00	0.000				
740-750	67.00-0.19	3284.00-0.60	1654.00-0.60	0.00-0.00	1.23-0.00	3.80-0.00	19.80-0.00	0.000				
750-760	67.00-0.19	3244.00-0.60	1654.00-0.60	0.00-0.00	1.22-0.00	3.80-0.00	19.80-0.00	0.000				
760-770	67.00-0.19	3204.00-0.60	1654.00-0.60	0.00-0.00	1.21-0.00	3.80-0.00	19.80-0.00	0.000				
770-780	67.00-0.19	3164.00-0.60	1654.00-0.60	0.00-0.00	1.20-0.00	3.80-0.00	19.80-0.00	0.000				
780-790	67.00-0.19	3124.00-0.60	1654.00-0.60	0.00-0.00	1.19-0.00	3.80-0.00	19.80-0.00	0.000				
790-800	67.00-0.19	3084.00-0.60	1654.00-0.60	0.00-0.00	1.18-0.00	3.80-0.00	19.80-0.00	0.000				
800-810	67.00-0.19	3044.00-0.60	1654.00-0.60	0.00-0.00	1.17-0.00	3.80-0.00	19.80-0.00	0.000				

Additional slides

Low Met 0 central jet

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	$(m_{\ell\ell}, m_{\nu}) = (390, 220)$	$qqZZ^*$	$ggZZ^*$	$t\bar{t}Z$	$Z + \text{jets}$	$t\bar{t}$	VVV	$s/\sqrt{s}$
4ℓ	64.51±0.24	2510.45±5.75	349.64±0.71	8.94±0.05	3.87±0.84	3.55±0.23	19.08±0.11	2.661
B-veto	60.07±0.23	2394.48±5.70	334.96±0.69	1.72±0.02	3.63±0.84	2.27±0.16	17.79±0.11	2.540
$N_{\text{jet}}^{\text{central}} = 0$	28.02±0.16	1607.35±5.06	211.64±0.55	0.42±0.01	2.10±0.15	0.99±0.10	9.30±0.07	1.453
$p_T^{\ell} > 0.00 \ \& \ \text{Metsig} > 0.00$	13.15±0.00	1526.61±0.00	190.77±0.00	0.09±0.00	1.55±0.00	0.36±0.00	2.17±0.00	0.703
$p_T^{\ell} > 0.00 \ \& \ \text{Metsig} > 0.50$	12.60±0.00	1155.38±0.00	159.47±0.00	0.08±0.00	1.43±0.00	0.31±0.00	2.03±0.00	0.770
$p_T^{\ell} > 0.00 \ \& \ \text{Metsig} > 1.00$	10.74±0.00	604.62±0.00	96.81±0.00	0.07±0.00	1.07±0.00	0.27±0.00	1.64±0.00	0.898
$p_T^{\ell} > 0.00 \ \& \ \text{Metsig} > 1.50$	7.73±0.00	265.55±0.00	45.24±0.00	0.05±0.00	0.73±0.00	0.16±0.00	1.06±0.00	0.970
$p_T^{\ell} > 10.00 \ \& \ \text{Metsig} > 0.00$	12.30±0.00	982.74±0.00	159.35±0.00	0.08±0.00	1.27±0.00	0.32±0.00	2.03±0.00	0.807
$p_T^{\ell} > 10.00 \ \& \ \text{Metsig} > 0.50$	11.88±0.01	832.47±1.03	139.00±0.12	0.08±0.00	1.21±0.02	0.30±0.02	1.91±0.00	0.844
$p_T^{\ell} > 10.00 \ \& \ \text{Metsig} > 1.00$	10.25±0.02	486.36±1.44	88.59±0.18	0.07±0.00	0.94±0.04	0.26±0.02	1.56±0.01	0.946
$p_T^{\ell} > 10.00 \ \& \ \text{Metsig} > 1.50$	7.39±0.02	210.36±1.55	41.54±0.20	0.05±0.00	0.65±0.05	0.15±0.02	1.01±0.01	1.030
$p_T^{\ell} > 15.00 \ \& \ \text{Metsig} > 0.00$	11.22±0.00	689.13±0.00	128.27±0.00	0.08±0.00	0.96±0.00	0.31±0.00	1.83±0.00	0.869
$p_T^{\ell} > 15.00 \ \& \ \text{Metsig} > 0.50$	10.86±0.01	600.82±1.18	113.76±0.15	0.07±0.00	0.91±0.03	0.30±0.03	1.74±0.01	0.900
$p_T^{\ell} > 15.00 \ \& \ \text{Metsig} > 1.00$	9.49±0.02	386.30±1.79	76.84±0.25	0.06±0.00	0.73±0.05	0.26±0.03	1.45±0.01	0.976
$p_T^{\ell} > 15.00 \ \& \ \text{Metsig} > 1.50$	6.89±0.03	172.44±1.98	36.85±0.28	0.04±0.00	0.53±0.06	0.15±0.03	0.95±0.01	1.052
$p_T^{\ell} > 20.00 \ \& \ \text{Metsig} > 0.00$	9.60±0.00	490.87±0.00	97.73±0.00	0.07±0.00	0.70±0.00	0.30±0.00	1.59±0.00	0.877
$p_T^{\ell} > 20.00 \ \& \ \text{Metsig} > 0.50$	9.31±0.02	429.91±1.31	87.10±0.17	0.07±0.00	0.67±0.03	0.28±0.03	1.51±0.01	0.906
$p_T^{\ell} > 20.00 \ \& \ \text{Metsig} > 1.00$	8.19±0.03	287.96±3.95	60.95±0.29	0.06±0.00	0.53±0.06	0.24±0.03	1.26±0.01	0.970
$p_T^{\ell} > 20.00 \ \& \ \text{Metsig} > 1.50$	6.04±0.04	136.29±4.13	30.49±0.33	0.04±0.00	0.41±0.07	0.14±0.03	0.84±0.01	1.033
$p_T^{\ell} > 25.00 \ \& \ \text{Metsig} > 0.00$	7.54±0.00	345.05±0.00	70.89±0.00	0.07±0.00	0.53±0.00	0.25±0.00	1.29±0.00	0.818
$p_T^{\ell} > 25.00 \ \& \ \text{Metsig} > 0.50$	7.29±0.02	300.51±1.44	62.89±0.18	0.06±0.00	0.51±0.03	0.23±0.03	1.21±0.01	0.846
$p_T^{\ell} > 25.00 \ \& \ \text{Metsig} > 1.00$	6.37±0.03	202.95±4.09	44.15±0.31	0.05±0.00	0.38±0.06	0.22±0.03	1.00±0.01	0.896
$p_T^{\ell} > 25.00 \ \& \ \text{Metsig} > 1.50$	4.64±0.05	98.43±4.36	22.49±0.37	0.03±0.00	0.28±0.08	0.13±0.03	0.66±0.02	0.932
$p_T^{\ell} > 5.00 \ \& \ \text{Metsig} > 0.00$	12.94±0.00	1333.50±0.00	182.83±0.00	0.09±0.00	1.45±0.00	0.36±0.00	2.14±0.00	0.737
$p_T^{\ell} > 5.00 \ \& \ \text{Metsig} > 0.50$	12.42±0.01	1058.18±0.68	154.94±0.07	0.08±0.00	1.34±0.01	0.31±0.00	2.00±0.00	0.791
$p_T^{\ell} > 5.00 \ \& \ \text{Metsig} > 1.00$	10.61±0.01	568.66±0.88	95.02±0.09	0.07±0.00	1.01±0.02	0.27±0.00	1.62±0.00	0.912
$p_T^{\ell} > 5.00 \ \& \ \text{Metsig} > 1.50$	7.64±0.01	247.18±0.93	44.36±0.10	0.05±0.00	0.69±0.02	0.16±0.00	1.05±0.00	0.990

Additional slides

	60 m/s (1960-2021)	g2C2	g2C2	H2	Z 2 ms	H	VVV	RA
4	66.31 ± 0.24	2010.45 ± 0.76	149.54 ± 0.47	0.94 ± 0.05	0.94 ± 0.04	0.95 ± 0.20	0.98 ± 0.11	2.661
5	71.72 ± 0.21	2010.45 ± 0.76	149.54 ± 0.47	0.94 ± 0.05	0.94 ± 0.04	0.95 ± 0.20	0.98 ± 0.11	2.661
6	36.95 ± 0.17	1897.12 ± 0.82	131.01 ± 0.42	1.30 ± 0.05	1.30 ± 0.05	1.30 ± 0.13	1.30 ± 0.13	2.341
7	-0.03 Gyr & Metallo -0.50	35.05 ± 0.17	1897.12 ± 0.82	1.30 ± 0.05	1.30 ± 0.05	1.30 ± 0.13	1.30 ± 0.13	2.341
8	-0.03 Gyr & Metallo -0.50	35.05 ± 0.17	1897.12 ± 0.82	1.30 ± 0.05	1.30 ± 0.05	1.30 ± 0.13	1.30 ± 0.13	2.341
9	-0.03 Gyr & Metallo -1.00	26.70 ± 0.16	1899.10 ± 0.73	1.23 ± 0.04	1.23 ± 0.04	1.23 ± 0.12	1.23 ± 0.12	2.341
10	-0.03 Gyr & Metallo -1.00	26.70 ± 0.16	1899.10 ± 0.73	1.23 ± 0.04	1.23 ± 0.04	1.23 ± 0.12	1.23 ± 0.12	2.341
11	-0.03 Gyr & Metallo -1.50	22.82 ± 0.15	1912.74 ± 0.64	1.23 ± 0.04	1.23 ± 0.04	1.23 ± 0.12	1.23 ± 0.12	2.341
12	-0.03 Gyr & Metallo -1.50	22.82 ± 0.15	1912.74 ± 0.64	1.23 ± 0.04	1.23 ± 0.04	1.23 ± 0.12	1.23 ± 0.12	2.341
13	-0.03 Gyr & Metallo -2.00	18.80 ± 0.11	1928.81 ± 0.55	1.23 ± 0.04	1.23 ± 0.04	1.23 ± 0.12	1.23 ± 0.12	2.341
14	-0.03 Gyr & Metallo -2.00	18.80 ± 0.11	1928.81 ± 0.55	1.23 ± 0.04	1.23 ± 0.04	1.23 ± 0.12	1.23 ± 0.12	2.341
15	-0.03 Gyr & Metallo -2.50	11.39 ± 0.13	1910.43 ± 0.21	0.89 ± 0.01	0.89 ± 0.01	0.89 ± 0.01	0.89 ± 0.01	2.188
16	-0.03 Gyr & Metallo -2.50	11.39 ± 0.13	1910.43 ± 0.21	0.89 ± 0.01	0.89 ± 0.01	0.89 ± 0.01	0.89 ± 0.01	2.188
17	-0.03 Gyr & Metallo -3.00	8.98 ± 0.08	1910.43 ± 0.21	0.89 ± 0.01	0.89 ± 0.01	0.89 ± 0.01	0.89 ± 0.01	2.188
18	-0.03 Gyr & Metallo -3.00	8.98 ± 0.08	1910.43 ± 0.21	0.89 ± 0.01	0.89 ± 0.01	0.89 ± 0.01	0.89 ± 0.01	2.188
19	-0.03 Gyr & Metallo -4.50	6.41 ± 0.08	2.36 ± 0.10	0.74 ± 0.02	0.74 ± 0.02	0.74 ± 0.02	0.74 ± 0.02	2.361
20	-0.03 Gyr & Metallo -4.50	6.41 ± 0.08	2.36 ± 0.10	0.74 ± 0.02	0.74 ± 0.02	0.74 ± 0.02	0.74 ± 0.02	2.361
21	-0.03 Gyr & Metallo -5.00	5.11 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
22	-0.03 Gyr & Metallo -5.00	5.11 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
23	-0.03 Gyr & Metallo -5.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
24	-0.03 Gyr & Metallo -5.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
25	-0.03 Gyr & Metallo -6.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
26	-0.03 Gyr & Metallo -6.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
27	-0.03 Gyr & Metallo -6.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
28	-0.03 Gyr & Metallo -6.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
29	-0.03 Gyr & Metallo -7.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
30	-0.03 Gyr & Metallo -7.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
31	-0.03 Gyr & Metallo -7.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
32	-0.03 Gyr & Metallo -7.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
33	-0.03 Gyr & Metallo -8.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
34	-0.03 Gyr & Metallo -8.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
35	-0.03 Gyr & Metallo -8.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
36	-0.03 Gyr & Metallo -8.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
37	-0.03 Gyr & Metallo -9.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
38	-0.03 Gyr & Metallo -9.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
39	-0.03 Gyr & Metallo -9.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
40	-0.03 Gyr & Metallo -9.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
41	-0.03 Gyr & Metallo -10.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
42	-0.03 Gyr & Metallo -10.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
43	-0.03 Gyr & Metallo -10.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
44	-0.03 Gyr & Metallo -10.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
45	-0.03 Gyr & Metallo -11.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
46	-0.03 Gyr & Metallo -11.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
47	-0.03 Gyr & Metallo -11.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
48	-0.03 Gyr & Metallo -11.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
49	-0.03 Gyr & Metallo -12.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
50	-0.03 Gyr & Metallo -12.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
51	-0.03 Gyr & Metallo -12.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
52	-0.03 Gyr & Metallo -12.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
53	-0.03 Gyr & Metallo -13.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
54	-0.03 Gyr & Metallo -13.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
55	-0.03 Gyr & Metallo -13.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
56	-0.03 Gyr & Metallo -13.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
57	-0.03 Gyr & Metallo -14.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
58	-0.03 Gyr & Metallo -14.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
59	-0.03 Gyr & Metallo -14.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
60	-0.03 Gyr & Metallo -14.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
61	-0.03 Gyr & Metallo -15.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
62	-0.03 Gyr & Metallo -15.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
63	-0.03 Gyr & Metallo -15.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
64	-0.03 Gyr & Metallo -15.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
65	-0.03 Gyr & Metallo -16.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
66	-0.03 Gyr & Metallo -16.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
67	-0.03 Gyr & Metallo -16.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
68	-0.03 Gyr & Metallo -16.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
69	-0.03 Gyr & Metallo -17.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
70	-0.03 Gyr & Metallo -17.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
71	-0.03 Gyr & Metallo -17.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
72	-0.03 Gyr & Metallo -17.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
73	-0.03 Gyr & Metallo -18.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
74	-0.03 Gyr & Metallo -18.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
75	-0.03 Gyr & Metallo -18.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
76	-0.03 Gyr & Metallo -18.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
77	-0.03 Gyr & Metallo -19.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
78	-0.03 Gyr & Metallo -19.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
79	-0.03 Gyr & Metallo -19.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
80	-0.03 Gyr & Metallo -19.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
81	-0.03 Gyr & Metallo -20.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
82	-0.03 Gyr & Metallo -20.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
83	-0.03 Gyr & Metallo -20.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
84	-0.03 Gyr & Metallo -20.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
85	-0.03 Gyr & Metallo -21.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
86	-0.03 Gyr & Metallo -21.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
87	-0.03 Gyr & Metallo -21.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
88	-0.03 Gyr & Metallo -21.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
89	-0.03 Gyr & Metallo -22.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
90	-0.03 Gyr & Metallo -22.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
91	-0.03 Gyr & Metallo -22.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
92	-0.03 Gyr & Metallo -22.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
93	-0.03 Gyr & Metallo -23.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
94	-0.03 Gyr & Metallo -23.00	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
95	-0.03 Gyr & Metallo -23.50	3.65 ± 0.07	1.95 ± 0.11	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	0.61 ± 0.01	2.188
96	-0.03 Gyr & Metallo -23.50	3.65 ± 0.07	1.95 ± 0.11	0.61				

Additional slides

Low Met 1 central jet

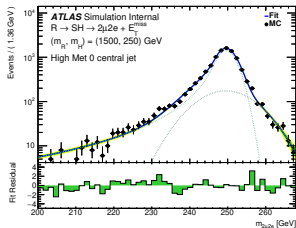
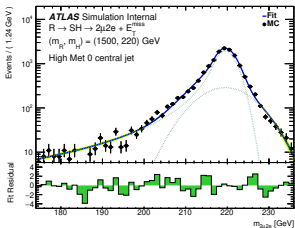
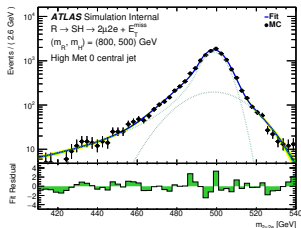
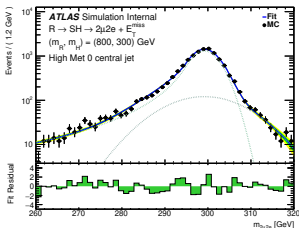
30

	$(m_{\ell\ell}, m_{WZ}) = (390, 220)$	qqZZ*	ggZZ*	t $\bar{t}$ Z	Z + jets	t $\bar{t}$	VVV	s/ $\sqrt{b}$
4 ℓ	64.51 $\pm$ 0.24	2510.45 $\pm$ 5.75	349.64 $\pm$ 0.71	8.94 $\pm$ 0.05	3.87 $\pm$ 0.84	3.55 $\pm$ 0.23	19.08 $\pm$ 0.11	2.661
B-veto	60.07 $\pm$ 0.23	2394.48 $\pm$ 5.70	334.96 $\pm$ 0.69	1.72 $\pm$ 0.02	3.63 $\pm$ 0.84	2.27 $\pm$ 0.16	17.79 $\pm$ 0.11	2.540
$N_{\text{events}}^{\text{MC}} \geq 1$	32.05 $\pm$ 0.17	787.13 $\pm$ 2.63	123.31 $\pm$ 0.42	1.30 $\pm$ 0.02	1.53 $\pm$ 0.83	1.27 $\pm$ 0.13	8.49 $\pm$ 0.08	2.341
$p_T^{\ell} > 0.00 \text{ GeV} \& \text{Metsig} > 0.00$	20.25 $\pm$ 0.14	777.32 $\pm$ 2.62	121.16 $\pm$ 0.42	0.61 $\pm$ 0.01	1.47 $\pm$ 0.83	0.61 $\pm$ 0.09	4.12 $\pm$ 0.05	1.494
$p_T^{\ell} > 0.00 \text{ GeV} \& \text{Metsig} > 0.50$	19.66 $\pm$ 0.13	647.21 $\pm$ 2.44	104.79 $\pm$ 0.39	0.59 $\pm$ 0.01	1.44 $\pm$ 0.83	0.61 $\pm$ 0.09	3.96 $\pm$ 0.05	1.584
$p_T^{\ell} > 0.00 \text{ GeV} \& \text{Metsig} > 1.00$	17.90 $\pm$ 0.13	389.48 $\pm$ 1.52	70.19 $\pm$ 0.32	0.54 $\pm$ 0.01	1.37 $\pm$ 0.83	0.54 $\pm$ 0.08	3.52 $\pm$ 0.05	1.822
$p_T^{\ell} > 0.00 \text{ GeV} \& \text{Metsig} > 1.50$	15.12 $\pm$ 0.12	207.75 $\pm$ 1.10	38.17 $\pm$ 0.24	0.46 $\pm$ 0.01	1.24 $\pm$ 0.82	0.49 $\pm$ 0.06	2.92 $\pm$ 0.05	2.114
$p_T^{\ell} > 0.00 \text{ GeV} \& \text{Metsig} > 2.00$	11.60 $\pm$ 0.10	94.91 $\pm$ 0.79	19.08 $\pm$ 0.17	0.36 $\pm$ 0.01	0.20 $\pm$ 0.04	0.37 $\pm$ 0.07	2.16 $\pm$ 0.04	2.379
$p_T^{\ell} > 0.00 \text{ GeV} \& \text{Metsig} > 2.50$	7.78 $\pm$ 0.08	38.83 $\pm$ 0.57	7.99 $\pm$ 0.11	0.24 $\pm$ 0.01	0.12 $\pm$ 0.03	0.28 $\pm$ 0.06	1.42 $\pm$ 0.03	2.469
$p_T^{\ell} > 0.00 \text{ GeV} \& \text{Metsig} > 3.00$	3.83 $\pm$ 0.06	12.77 $\pm$ 0.25	2.84 $\pm$ 0.06	0.13 $\pm$ 0.01	0.04 $\pm$ 0.02	0.20 $\pm$ 0.06	0.69 $\pm$ 0.02	2.093
$p_T^{\ell} > 5.00 \text{ GeV} \& \text{Metsig} > 0.00$	20.12 $\pm$ 0.14	771.50 $\pm$ 2.61	120.76 $\pm$ 0.42	0.61 $\pm$ 0.01	1.47 $\pm$ 0.83	0.61 $\pm$ 0.09	4.10 $\pm$ 0.05	1.490
$p_T^{\ell} > 5.00 \text{ GeV} \& \text{Metsig} > 0.50$	19.54 $\pm$ 0.13	641.99 $\pm$ 2.43	104.36 $\pm$ 0.39	0.59 $\pm$ 0.01	1.43 $\pm$ 0.83	0.61 $\pm$ 0.09	3.94 $\pm$ 0.05	1.580
$p_T^{\ell} > 5.00 \text{ GeV} \& \text{Metsig} > 1.00$	17.78 $\pm$ 0.13	395.31 $\pm$ 1.51	69.90 $\pm$ 0.32	0.54 $\pm$ 0.01	1.37 $\pm$ 0.83	0.54 $\pm$ 0.08	3.51 $\pm$ 0.05	1.818
$p_T^{\ell} > 5.00 \text{ GeV} \& \text{Metsig} > 1.50$	15.01 $\pm$ 0.12	204.76 $\pm$ 1.09	38.96 $\pm$ 0.24	0.46 $\pm$ 0.01	1.23 $\pm$ 0.82	0.49 $\pm$ 0.06	2.91 $\pm$ 0.05	2.112
$p_T^{\ell} > 5.00 \text{ GeV} \& \text{Metsig} > 2.00$	11.50 $\pm$ 0.10	93.23 $\pm$ 0.79	19.94 $\pm$ 0.17	0.36 $\pm$ 0.01	0.19 $\pm$ 0.04	0.37 $\pm$ 0.07	2.17 $\pm$ 0.04	2.377
$p_T^{\ell} > 5.00 \text{ GeV} \& \text{Metsig} > 2.50$	7.70 $\pm$ 0.08	38.05 $\pm$ 0.57	7.92 $\pm$ 0.11	0.24 $\pm$ 0.01	0.12 $\pm$ 0.03	0.28 $\pm$ 0.06	1.41 $\pm$ 0.03	2.464
$p_T^{\ell} > 5.00 \text{ GeV} \& \text{Metsig} > 3.00$	3.76 $\pm$ 0.06	12.47 $\pm$ 0.25	2.80 $\pm$ 0.06	0.12 $\pm$ 0.01	0.04 $\pm$ 0.02	0.20 $\pm$ 0.06	0.88 $\pm$ 0.02	2.081
$p_T^{\ell} > 10.00 \text{ GeV} \& \text{Metsig} > 0.00$	19.74 $\pm$ 0.13	758.25 $\pm$ 2.60	119.35 $\pm$ 0.41	0.60 $\pm$ 0.01	1.46 $\pm$ 0.83	0.60 $\pm$ 0.09	4.05 $\pm$ 0.05	1.473
$p_T^{\ell} > 10.00 \text{ GeV} \& \text{Metsig} > 0.50$	19.15 $\pm$ 0.13	629.87 $\pm$ 2.42	103.07 $\pm$ 0.39	0.59 $\pm$ 0.01	1.42 $\pm$ 0.83	0.60 $\pm$ 0.09	3.89 $\pm$ 0.05	1.563
$p_T^{\ell} > 10.00 \text{ GeV} \& \text{Metsig} > 1.00$	17.40 $\pm$ 0.13	385.54 $\pm$ 1.49	68.86 $\pm$ 0.32	0.53 $\pm$ 0.01	1.36 $\pm$ 0.83	0.54 $\pm$ 0.08	3.48 $\pm$ 0.05	1.800
$p_T^{\ell} > 10.00 \text{ GeV} \& \text{Metsig} > 1.50$	14.64 $\pm$ 0.12	197.87 $\pm$ 1.07	38.24 $\pm$ 0.24	0.45 $\pm$ 0.01	1.23 $\pm$ 0.82	0.48 $\pm$ 0.06	2.87 $\pm$ 0.05	2.092
$p_T^{\ell} > 10.00 \text{ GeV} \& \text{Metsig} > 2.00$	11.17 $\pm$ 0.10	89.24 $\pm$ 0.77	18.55 $\pm$ 0.16	0.35 $\pm$ 0.01	0.19 $\pm$ 0.04	0.37 $\pm$ 0.07	2.13 $\pm$ 0.04	2.354
$p_T^{\ell} > 10.00 \text{ GeV} \& \text{Metsig} > 2.50$	7.43 $\pm$ 0.08	36.26 $\pm$ 0.56	7.75 $\pm$ 0.11	0.24 $\pm$ 0.01	0.12 $\pm$ 0.03	0.28 $\pm$ 0.06	1.38 $\pm$ 0.03	2.430
$p_T^{\ell} > 10.00 \text{ GeV} \& \text{Metsig} > 3.00$	3.55 $\pm$ 0.06	11.65 $\pm$ 0.24	2.52 $\pm$ 0.06	0.12 $\pm$ 0.01	0.04 $\pm$ 0.02	0.19 $\pm$ 0.06	0.66 $\pm$ 0.02	2.023
$p_T^{\ell} > 15.00 \text{ GeV} \& \text{Metsig} > 0.00$	19.32 $\pm$ 0.13	740.77 $\pm$ 2.58	116.98 $\pm$ 0.41	0.60 $\pm$ 0.01	1.45 $\pm$ 0.83	0.59 $\pm$ 0.09	4.01 $\pm$ 0.05	1.458
$p_T^{\ell} > 15.00 \text{ GeV} \& \text{Metsig} > 0.50$	18.73 $\pm$ 0.13	613.95 $\pm$ 2.40	100.89 $\pm$ 0.38	0.58 $\pm$ 0.01	1.41 $\pm$ 0.83	0.59 $\pm$ 0.09	3.85 $\pm$ 0.05	1.548
$p_T^{\ell} > 15.00 \text{ GeV} \& \text{Metsig} > 1.00$	17.01 $\pm$ 0.13	373.93 $\pm$ 1.46	67.16 $\pm$ 0.31	0.53 $\pm$ 0.01	1.35 $\pm$ 0.83	0.53 $\pm$ 0.08	3.42 $\pm$ 0.05	1.787
$p_T^{\ell} > 15.00 \text{ GeV} \& \text{Metsig} > 1.50$	14.28 $\pm$ 0.11	186.79 $\pm$ 1.04	37.14 $\pm$ 0.23	0.45 $\pm$ 0.01	1.23 $\pm$ 0.82	0.47 $\pm$ 0.06	2.83 $\pm$ 0.05	2.081
$p_T^{\ell} > 15.00 \text{ GeV} \& \text{Metsig} > 2.00$	10.87 $\pm$ 0.10	84.88 $\pm$ 0.76	17.98 $\pm$ 0.16	0.35 $\pm$ 0.01	0.18 $\pm$ 0.04	0.37 $\pm$ 0.07	2.11 $\pm$ 0.04	2.345
$p_T^{\ell} > 15.00 \text{ GeV} \& \text{Metsig} > 2.50$	7.21 $\pm$ 0.08	34.46 $\pm$ 0.55	7.49 $\pm$ 0.10	0.24 $\pm$ 0.01	0.11 $\pm$ 0.03	0.28 $\pm$ 0.06	1.36 $\pm$ 0.03	2.413
$p_T^{\ell} > 15.00 \text{ GeV} \& \text{Metsig} > 3.00$	3.45 $\pm$ 0.06	10.96 $\pm$ 0.23	2.45 $\pm$ 0.06	0.12 $\pm$ 0.01	0.04 $\pm$ 0.02	0.19 $\pm$ 0.06	0.65 $\pm$ 0.02	2.015
$p_T^{\ell} > 20.00 \text{ GeV} \& \text{Metsig} > 0.00$	18.75 $\pm$ 0.13	718.82 $\pm$ 2.19	113.33 $\pm$ 0.40	0.59 $\pm$ 0.01	1.43 $\pm$ 0.83	0.58 $\pm$ 0.09	3.93 $\pm$ 0.05	1.437
$p_T^{\ell} > 20.00 \text{ GeV} \& \text{Metsig} > 0.50$	18.18 $\pm$ 0.13	593.98 $\pm$ 1.98	97.53 $\pm$ 0.37	0.58 $\pm$ 0.01	1.39 $\pm$ 0.83	0.58 $\pm$ 0.09	3.77 $\pm$ 0.05	1.527
$p_T^{\ell} > 20.00 \text{ GeV} \& \text{Metsig} > 1.00$	16.47 $\pm$ 0.12	359.47 $\pm$ 1.42	64.85 $\pm$ 0.31	0.52 $\pm$ 0.01	1.33 $\pm$ 0.83	0.52 $\pm$ 0.08	3.35 $\pm$ 0.05	1.763
$p_T^{\ell} > 20.00 \text{ GeV} \& \text{Metsig} > 1.50$	13.80 $\pm$ 0.11	181.78 $\pm$ 1.00	35.63 $\pm$ 0.23	0.45 $\pm$ 0.01	1.21 $\pm$ 0.82	0.46 $\pm$ 0.06	2.77 $\pm$ 0.05	2.054
$p_T^{\ell} > 20.00 \text{ GeV} \& \text{Metsig} > 2.00$	10.47 $\pm$ 0.10	81.00 $\pm$ 0.73	17.20 $\pm$ 0.16	0.35 $\pm$ 0.01	0.17 $\pm$ 0.04	0.37 $\pm$ 0.07	2.07 $\pm$ 0.04	2.310
$p_T^{\ell} > 20.00 \text{ GeV} \& \text{Metsig} > 2.50$	6.92 $\pm$ 0.08	32.84 $\pm$ 0.54	7.16 $\pm$ 0.10	0.24 $\pm$ 0.01	0.10 $\pm$ 0.03	0.28 $\pm$ 0.06	1.34 $\pm$ 0.03	2.373
$p_T^{\ell} > 20.00 \text{ GeV} \& \text{Metsig} > 3.00$	3.91 $\pm$ 0.06	10.40 $\pm$ 0.22	2.94 $\pm$ 0.06	0.12 $\pm$ 0.01	0.03 $\pm$ 0.02	0.19 $\pm$ 0.06	0.63 $\pm$ 0.02	1.961
$p_T^{\ell} > 25.00 \text{ GeV} \& \text{Metsig} > 0.00$	18.08 $\pm$ 0.13	693.64 $\pm$ 2.13	108.53 $\pm$ 0.39	0.58 $\pm$ 0.01	1.42 $\pm$ 0.83	0.58 $\pm$ 0.09	3.85 $\pm$ 0.05	1.411
$p_T^{\ell} > 25.00 \text{ GeV} \& \text{Metsig} > 0.50$	17.51 $\pm$ 0.13	571.60 $\pm$ 1.92	93.22 $\pm$ 0.37	0.57 $\pm$ 0.01	1.39 $\pm$ 0.83	0.58 $\pm$ 0.09	3.69 $\pm$ 0.05	1.501
$p_T^{\ell} > 25.00 \text{ GeV} \& \text{Metsig} > 1.00$	15.84 $\pm$ 0.12	344.28 $\pm$ 1.36	61.60 $\pm$ 0.30	0.52 $\pm$ 0.01	1.32 $\pm$ 0.83	0.51 $\pm$ 0.08	3.28 $\pm$ 0.05	1.743
$p_T^{\ell} > 25.00 \text{ GeV} \& \text{Metsig} > 1.50$	13.24 $\pm$ 0.11	173.81 $\pm$ 0.96	33.86 $\pm$ 0.22	0.44 $\pm$ 0.01	1.20 $\pm$ 0.82	0.45 $\pm$ 0.08	2.71 $\pm$ 0.05	2.017
$p_T^{\ell} > 25.00 \text{ GeV} \& \text{Metsig} > 2.00$	10.01 $\pm$ 0.10	77.39 $\pm$ 0.70	16.32 $\pm$ 0.15	0.34 $\pm$ 0.01	0.17 $\pm$ 0.04	0.37 $\pm$ 0.07	2.02 $\pm$ 0.04	2.261
$p_T^{\ell} > 25.00 \text{ GeV} \& \text{Metsig} > 2.50$	6.59 $\pm$ 0.08	31.16 $\pm$ 0.52	6.76 $\pm$ 0.10	0.23 $\pm$ 0.01	0.10 $\pm$ 0.03	0.28 $\pm$ 0.06	1.31 $\pm$ 0.03	2.319
$p_T^{\ell} > 25.00 \text{ GeV} \& \text{Metsig} > 3.00$	3.13 $\pm$ 0.05	9.72 $\pm$ 0.20	2.21 $\pm$ 0.06	0.12 $\pm$ 0.01	0.03 $\pm$ 0.02	0.19 $\pm$ 0.06	0.62 $\pm$ 0.02	1.938
$p_T^{\ell} > 30.00 \text{ GeV} \& \text{Metsig} > 0.00$	17.36 $\pm$ 0.13	662.22 $\pm$ 2.06	102.50 $\pm$ 0.38	0.57 $\pm$ 0.01	1.40 $\pm$ 0.83	0.56 $\pm$ 0.09	3.76 $\pm$ 0.05	1.388
$p_T^{\ell} > 30.00 \text{ GeV} \& \text{Metsig} > 0.50$	16.81 $\pm$ 0.12	544.79 $\pm$ 1.85	87.93 $\pm$ 0.36	0.55 $\pm$ 0.01	1.38 $\pm$ 0.83	0.56 $\pm$ 0.09	3.60 $\pm$ 0.05	1.477
$p_T^{\ell} > 30.00 \text{ GeV} \& \text{Metsig} > 1.00$	15.19 $\pm$ 0.12	327.41 $\pm$ 1.30	57.95 $\pm$ 0.29	0.50 $\pm$ 0.01	1.32 $\pm$ 0.83	0.50 $\pm$ 0.08	3.20 $\pm$ 0.05	1.705
$p_T^{\ell} > 30.00 \text{ GeV} \& \text{Metsig} > 1.50$	12.68 $\pm$ 0.11	164.88 $\pm$ 0.91	31.77 $\pm$ 0.21	0.43 $\pm$ 0.01	1.20 $\pm$ 0.82	0.45 $\pm$ 0.08	2.85 $\pm$ 0.04	1.962
$p_T^{\ell} > 30.00 \text{ GeV} \& \text{Metsig} > 2.00$	9.54 $\pm$ 0.09	73.18 $\pm$ 0.66	15.29 $\pm$ 0.15	0.33 $\pm$ 0.01	0.17 $\pm$ 0.04	0.36 $\pm$ 0.07	1.98 $\pm$ 0.04	2.216
$p_T^{\ell} > 30.00 \text{ GeV} \& \text{Metsig} > 2.50$	6.28 $\pm$ 0.08	28.35 $\pm$ 0.50	6.30 $\pm$ 0.10	0.22 $\pm$ 0.01	0.10 $\pm$ 0.03	0.28 $\pm$ 0.06	1.28 $\pm$ 0.03	2.268
$p_T^{\ell} > 30.00 \text{ GeV} \& \text{Metsig} > 3.00$	2.96 $\pm$ 0.05	9.07 $\pm$ 0.19	2.05 $\pm$ 0.05	0.11 $\pm$ 0.01	0.03 $\pm$ 0.02	0.19 $\pm$ 0.06	0.61 $\pm$ 0.02	1.891

Signal parametrisation

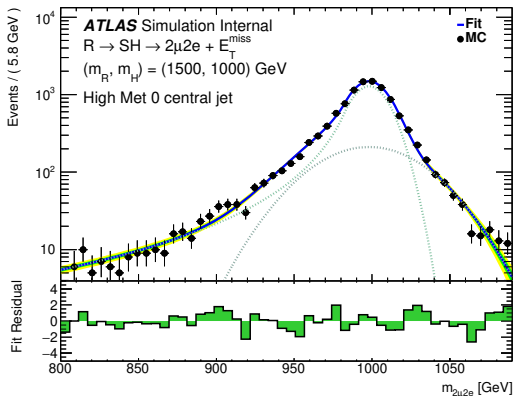
High Met 0 central jet for $2\mu 2e$ channel

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Signal parametrisation

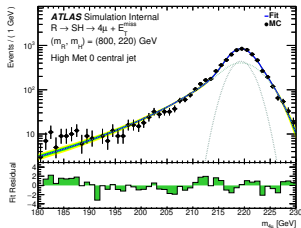
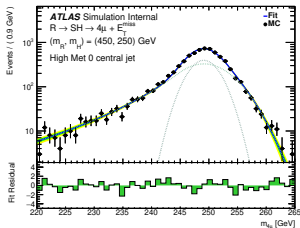
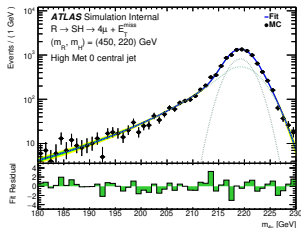
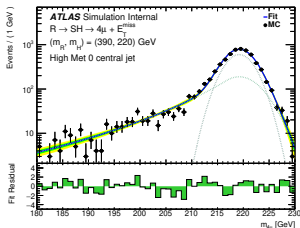
High Met 0 central jet for $2\mu 2e$ channel



Signal parametrisation

High Met 0 central jet for 4μ channel

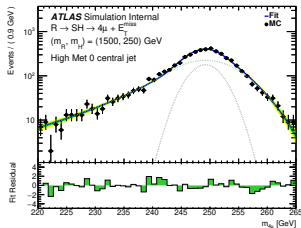
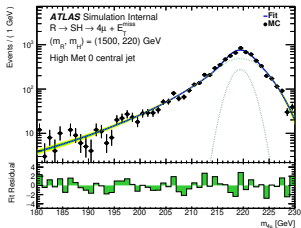
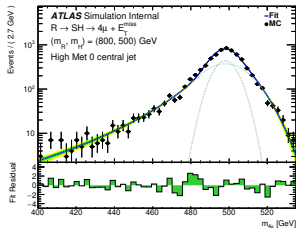
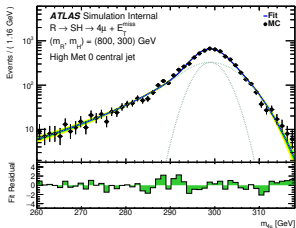
33



Signal parametrisation

High Met 0 central jet for 4μ channel

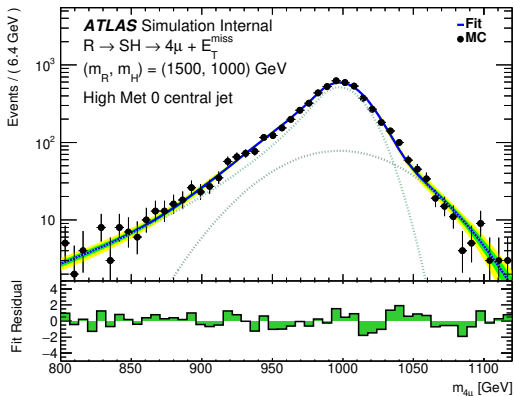
34



Signal parametrisation

High Met 0 central jet for 4μ channel

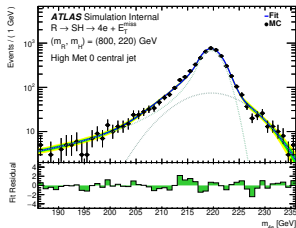
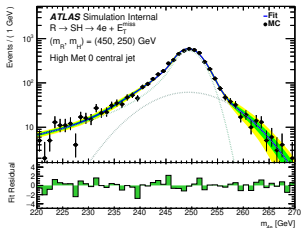
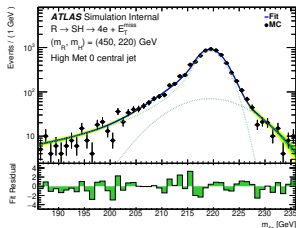
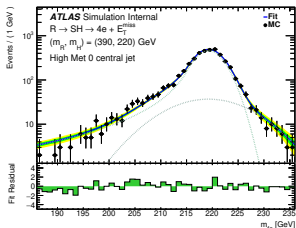
35



Signal parametrisation

High Met 0 central jet for 4e channel

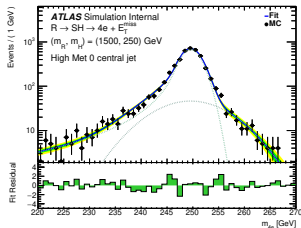
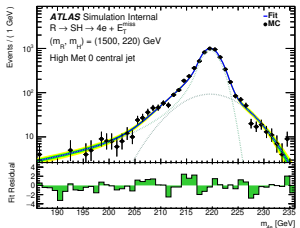
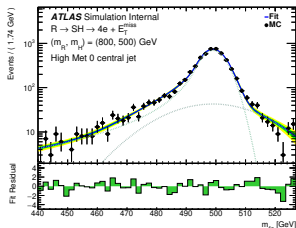
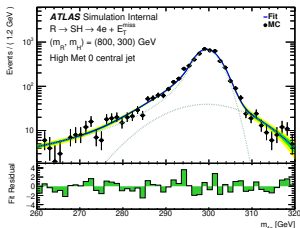
36



Signal parametrisation

High Met 0 central jet for 4e channel

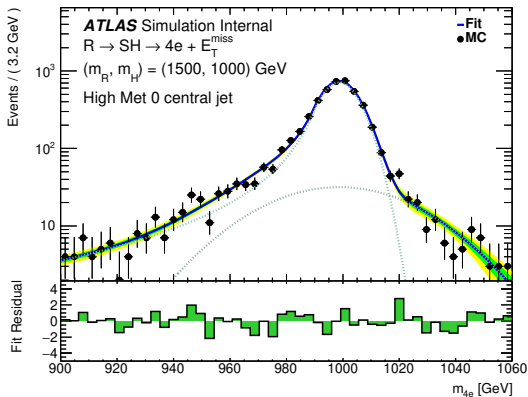
37



Signal parametrisation

High Met 0 central jet for 4e channel

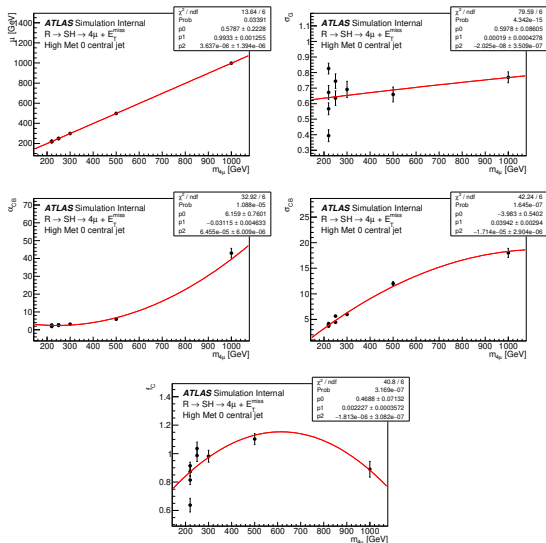
38



Interpolation of μ , f_C , σ_G , σ_C and α_C parameters

4 μ -channel

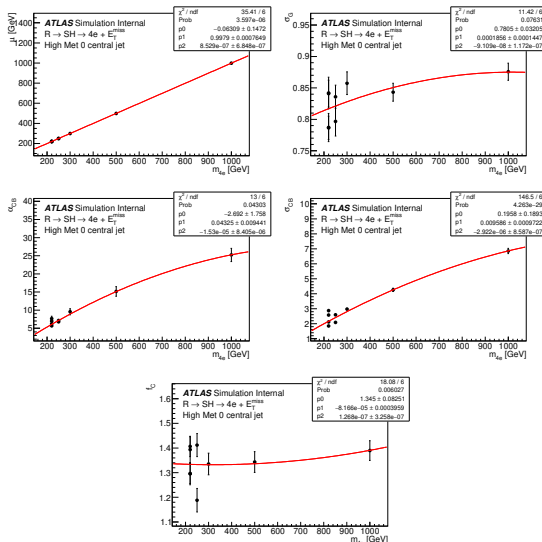
39



Interpolation of μ , f_C , σ_G , σ_C and α_C parameters

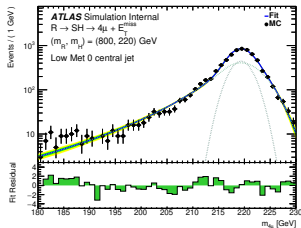
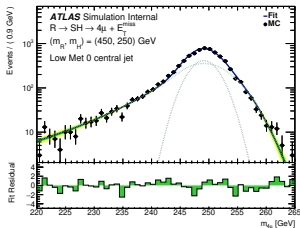
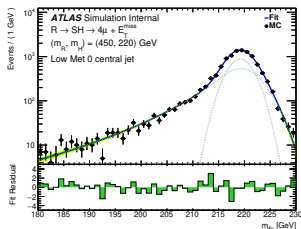
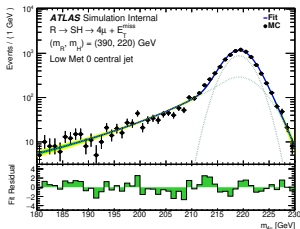
4e-channel

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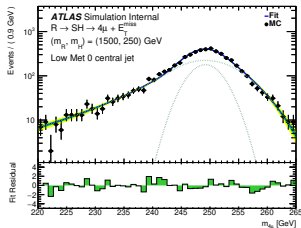
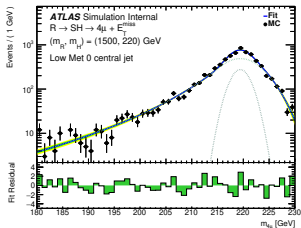
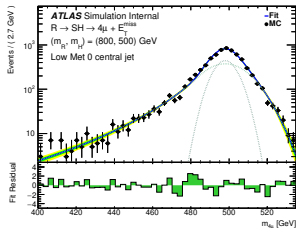
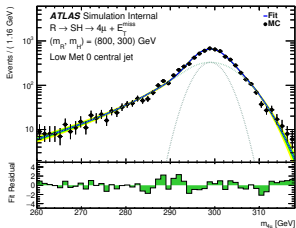
Signal parametrisation

Low Met 0 central jet for 4μ channel



Signal parametrisation

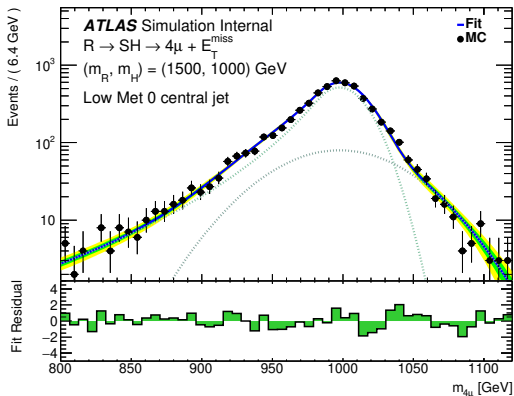
Low Met 0 central jet for 4μ channel



Signal parametrisation

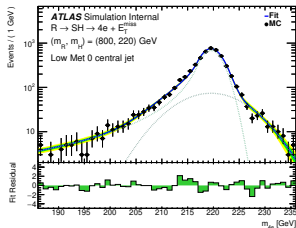
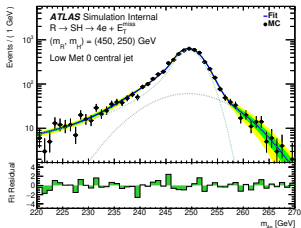
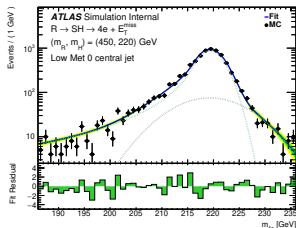
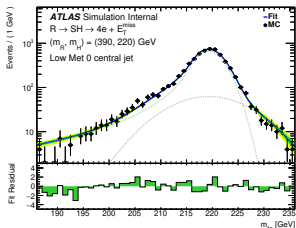
Low Met 0 central jet for 4μ channel

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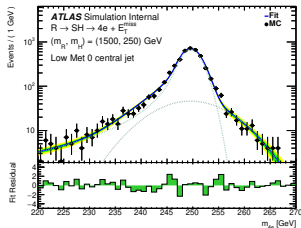
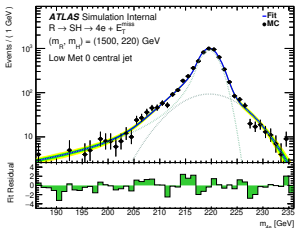
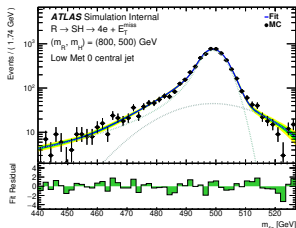
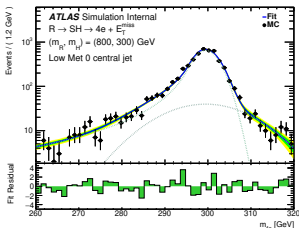
Signal parametrisation

Low Met 0 central jet for 4e channel



Signal parametrisation

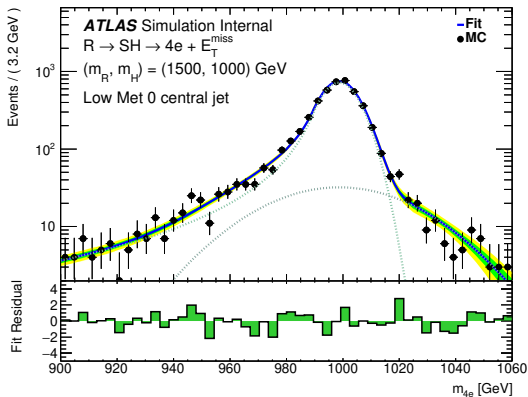
Low Met 0 central jet for 4e channel



Signal parametrisation

Low Met 0 central jet for 4e channel

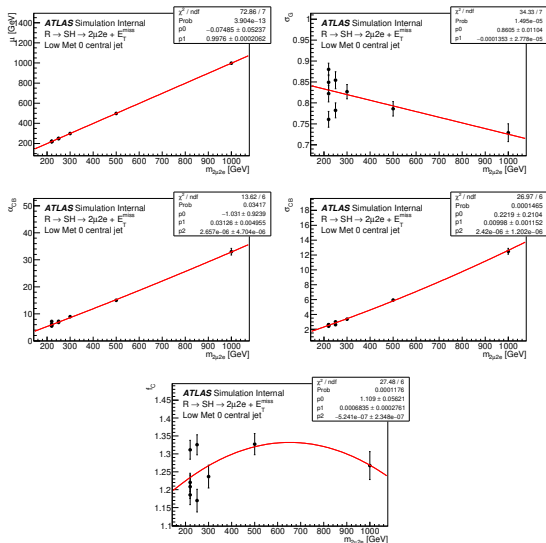
46



Interpolation of μ , f_C , σ_G , σ_C and α_C parameters

$2\mu 2e$ -channel

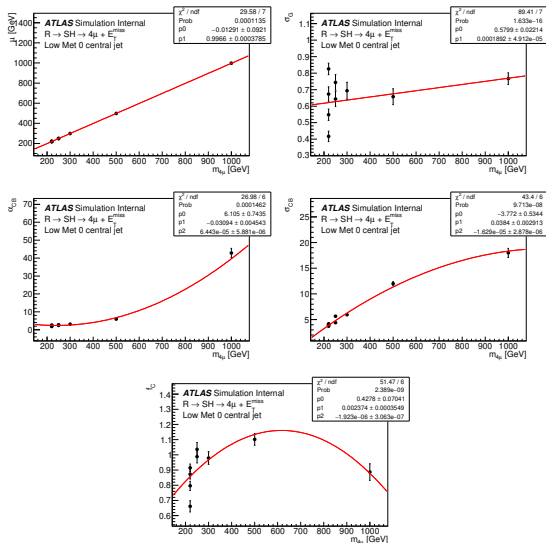
47



Interpolation of μ , f_C , σ_G , σ_C and α_C parameters

4 μ -channel

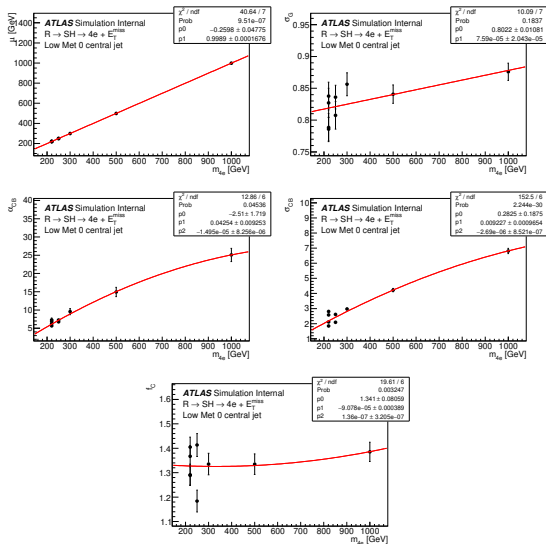
48



Interpolation of μ , f_C , σ_G , σ_C and α_C parameters

4e-channel

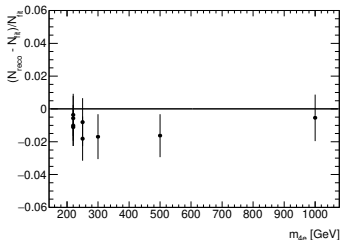
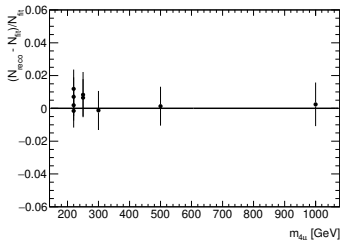
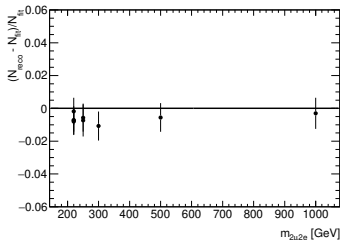
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Study the bias induced by the signal extraction

Low Met 0 central jet for all the channels

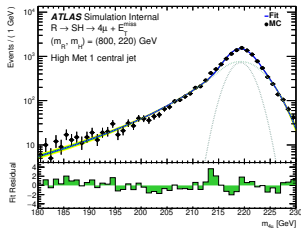
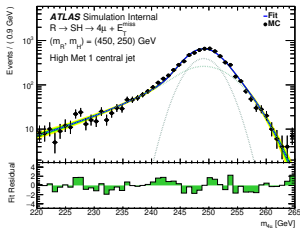
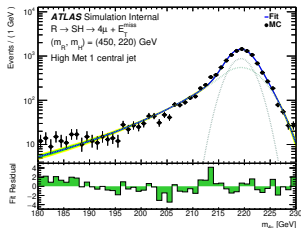
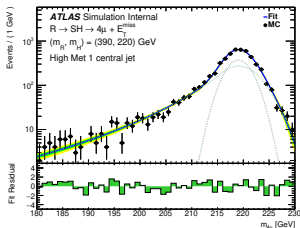
50



Signal parametrisation

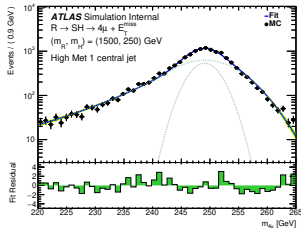
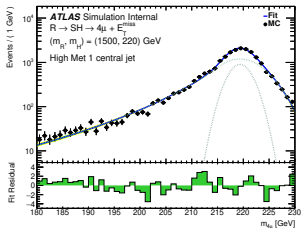
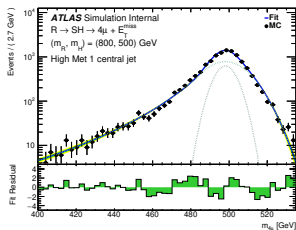
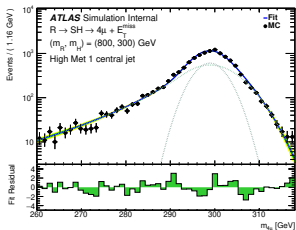
High Met 1 central jet for 4μ channel

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Signal parametrisation

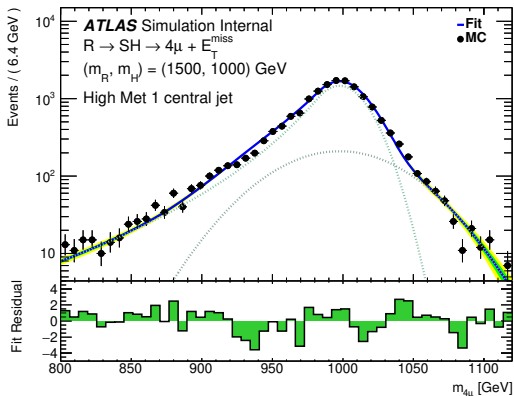
High Met 1 central jet for 4μ channel



Signal parametrisation

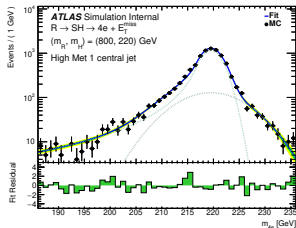
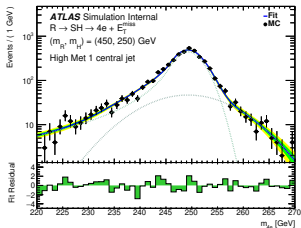
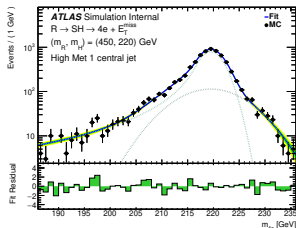
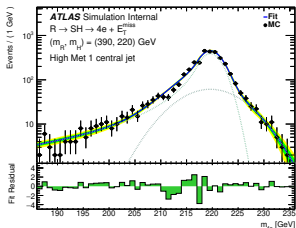
High Met 1 central jet for 4μ channel

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Signal parametrisation

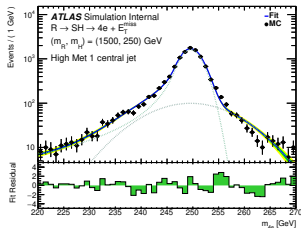
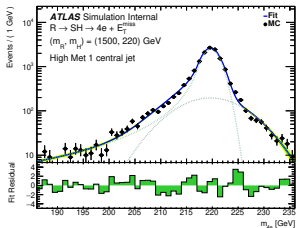
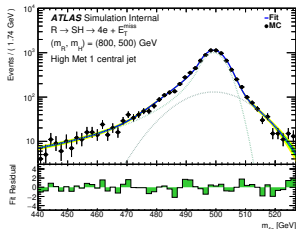
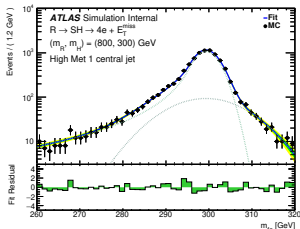
High Met 1 central jet for 4e channel



Signal parametrisation

High Met 1 central jet for 4e channel

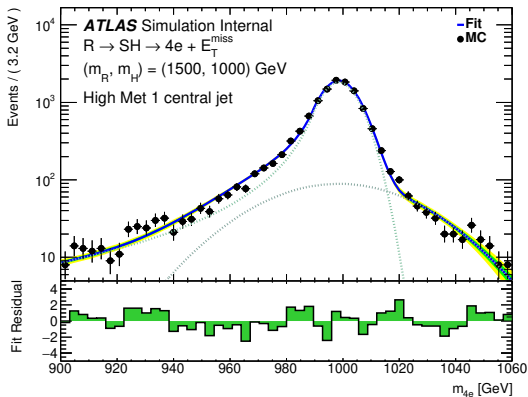
55



Signal parametrisation

High Met 1 central jet for 4e channel

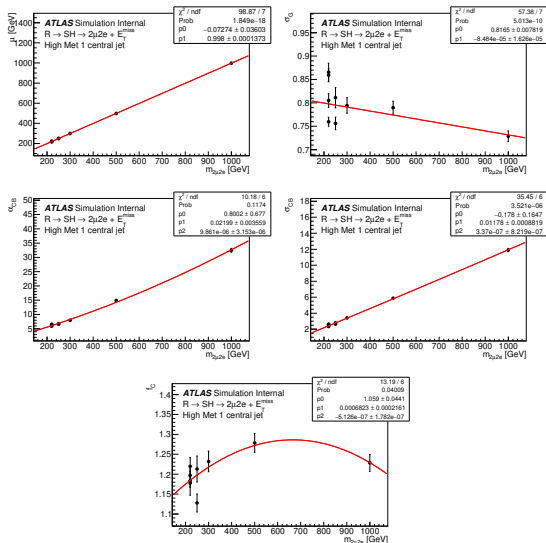
56



Interpolation of μ , f_C , σ_G , σ_C and α_C parameters

$2\mu 2e$ -channel

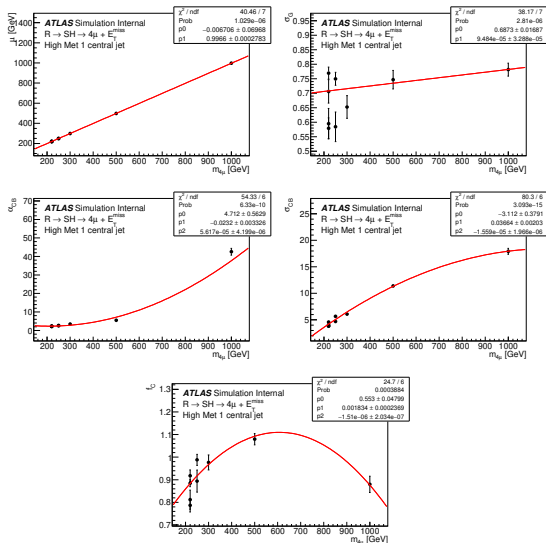
57



Interpolation of μ , f_C , σ_G , σ_C and α_C parameters

4 μ -channel

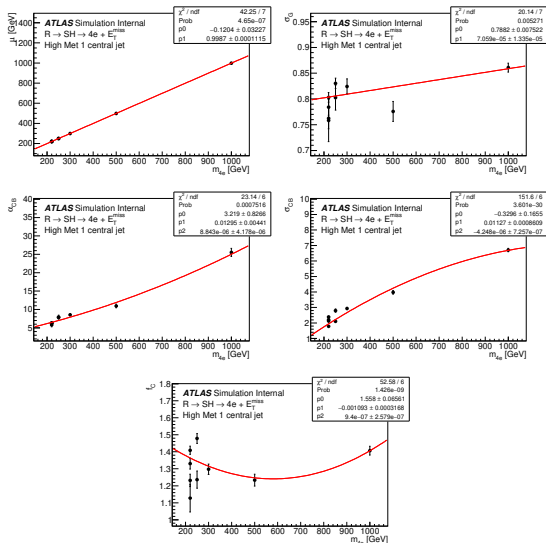
58



Interpolation of μ , f_C , σ_G , σ_C and α_C parameters

4e-channel

59



Study the bias induced by the signal extraction

High Met 1 central jet for all the channels

60

