

**The 2020 International Workshop on the High Energy
Circular Electron Positron Collider
(Oct. 26-28, 2020)**

CEPC Linac and damping ring R&D

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Outline

1 Linac baseline design

2 R&D activities

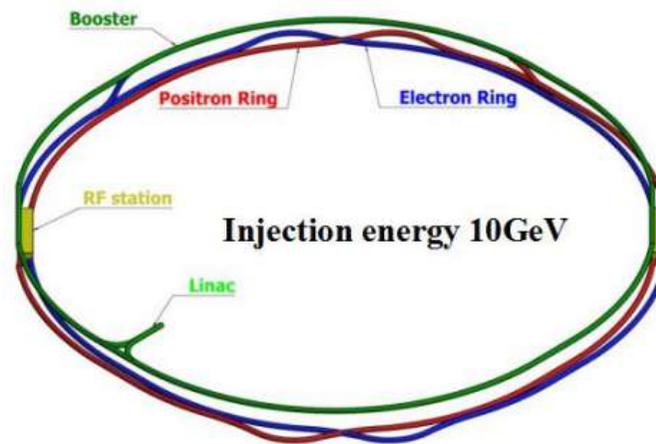
3 Linac alternative

4 Summary



Linac design

- CEPC consists of Linac, Booster and Collider
 - The energy electron and positron of the Collider is 120 GeV
 - The booster and collider circumference is about 100 km
 - The injector linac provides 10 GeV electron and positron beam to the Booster
 - The length of the linac is about 1.2 km





Linac design

- The requirements of the booster to the linac

Parameter	Symbol	Unit	Value
e^- / e^+ beam energy	E_{e^-} / E_{e^+}	GeV	10
Repetition rate	f_{rep}	Hz	100
Bunch numbers per pulse			1
e^- / e^+ bunch population	N_{e^-} / N_{e^+}		$>9.4 \times 10^9$
		nC	>1.5
Energy spread (e^- / e^+)	σ_E		$<2 \times 10^{-3}$
Emittance (e^- / e^+)	ε_r	nm	<40



Linac design

- Linac design goals

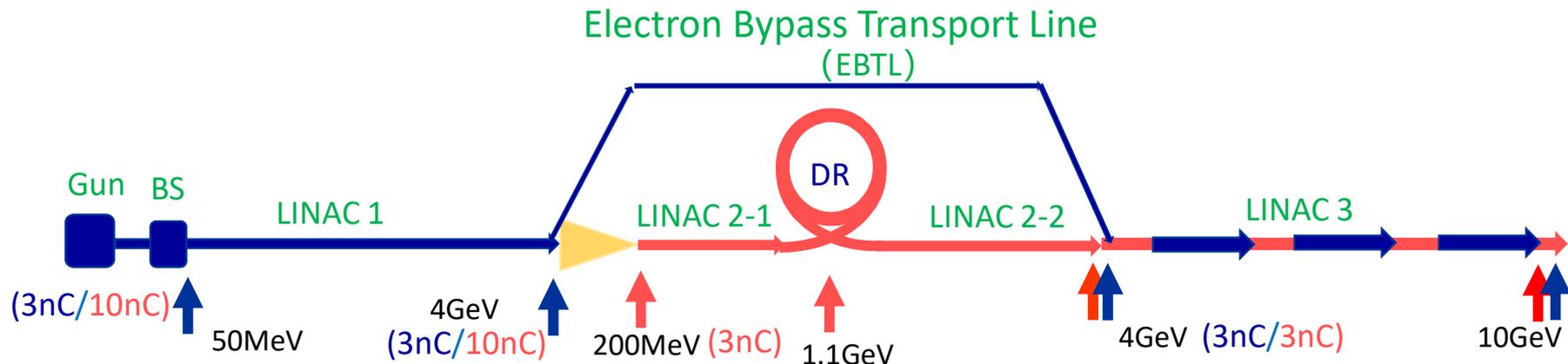
- Meet the requirements of booster injector
- Top-up injection can be implemented
- High availability and reliability
 - ◆ About 15% backups for linac RF units
- More potential
 - ◆ Have potential to provide electron/positron beam with bunch charge large than 3 nC
 - ◆ Lower emittance with more cycles in Damping Ring



Linac design

- Layout of linac

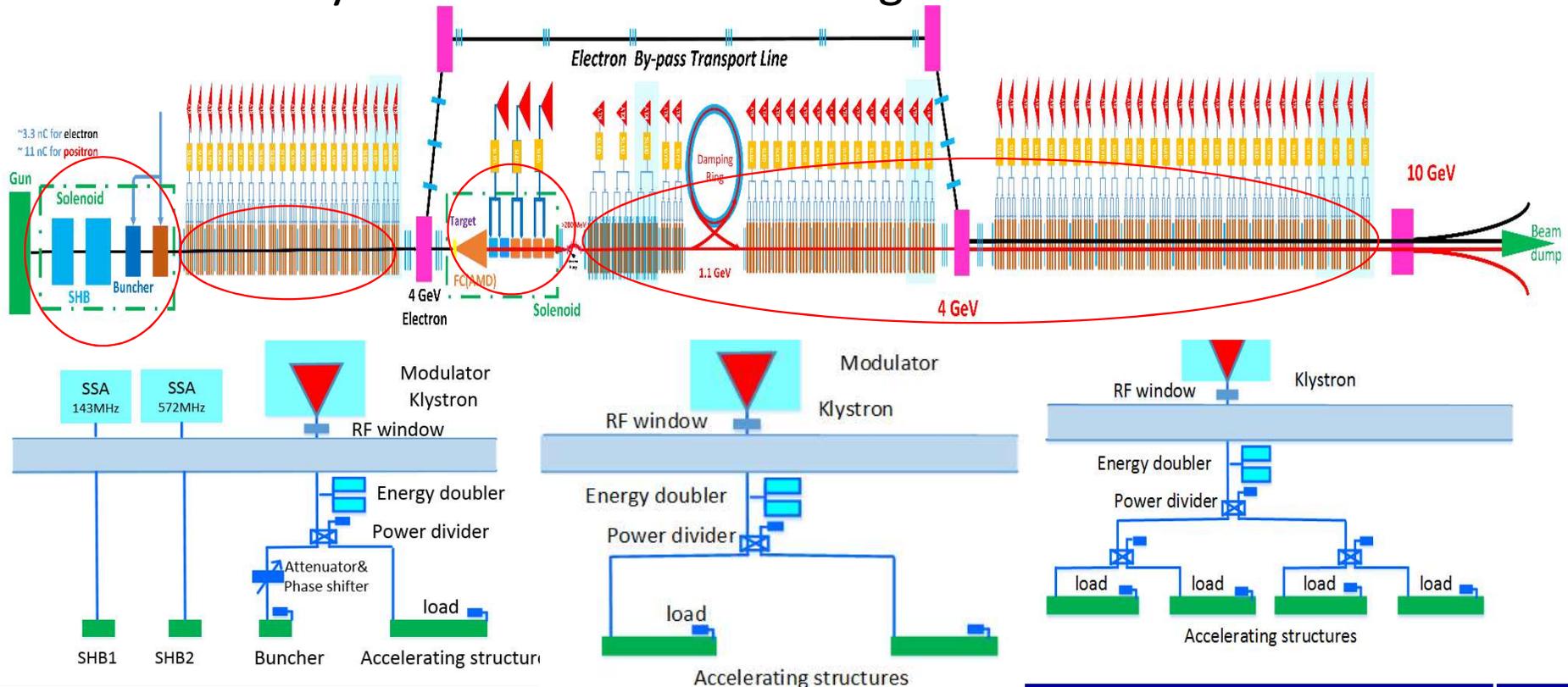
- Electron linac (Pre-injector+Linac 1+EBTL+Linac 3)
- Positron linac (Pre-injector+Linac 1+PS+Linac 2-1+DR+Linac 2-2+Linac 3)
- Mature technologies: Thermionic gun, Fixed positron target, S-band RF system





Linac design

- RF distribution of the linac (80MW klystron)
 - Bunching system
 - Big hole accelerating structure after positron target
 - One klystron to four accelerating structures





R&D activities

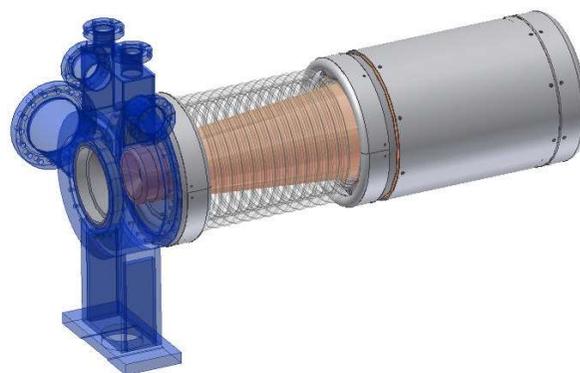
- Key components of baseline linac
 - Electron gun
 - SHBs
 - Buncher
 - S-band accelerating structure
 - Pulse compressor
 - Positron source
 - Big hole accelerating structure
 - **DR 650MHz RF cavity**
 - LLRF
 - Phase reference line
 -



Electron gun

- Traditional thermionic triode gun

Parameter	Unit	Value
Type		Thermionic Triode Gun
Cathode		Y796 (Eimac) Dispenser
Beam Current (max.)	A	10
High Voltage of Anode	kV	120 ~ 200
Bias Voltage of Grid	V	0 ~ -200
Pulse duration	ns	1





SHB & buncher

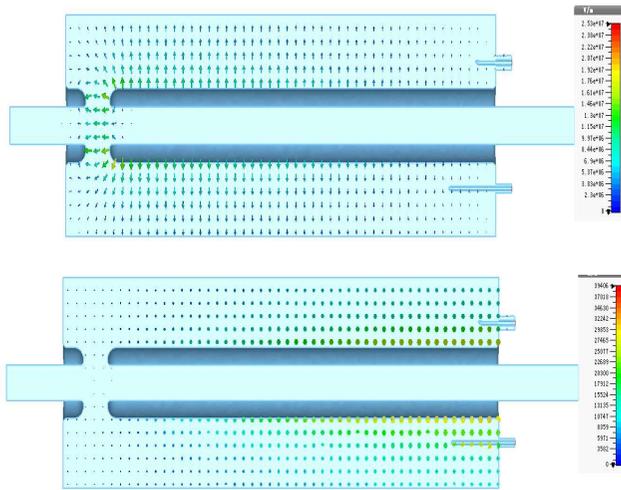
- Sub-harmonic buncher (SHB)

- Capacitively loaded structure

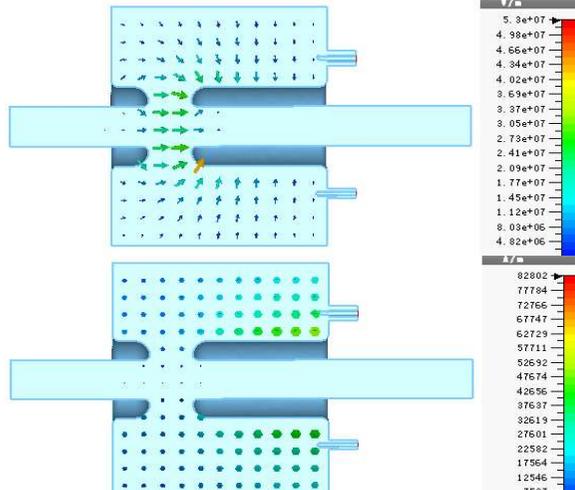
- Buncher

- Travelling wave
 - $2\pi/3$
 - $\beta=0.75$, 6 cells

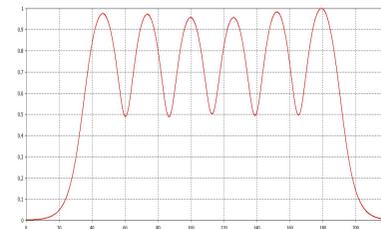
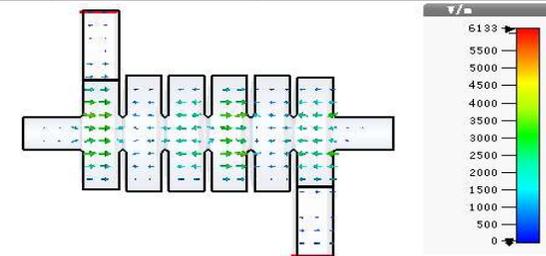
Parameters	Value			Unit
	SHB1	SHB2	B	
Frequency	143	572	2860	MHz
Shunt Impedance	1.39	2.89	7.5	MΩ
Unloaded Q	8139	13458	11083	-
Bunching Voltage(Max)	100	120	1200	kV
RF Structure	SW	SW	TW	-



SHB1



SHB2

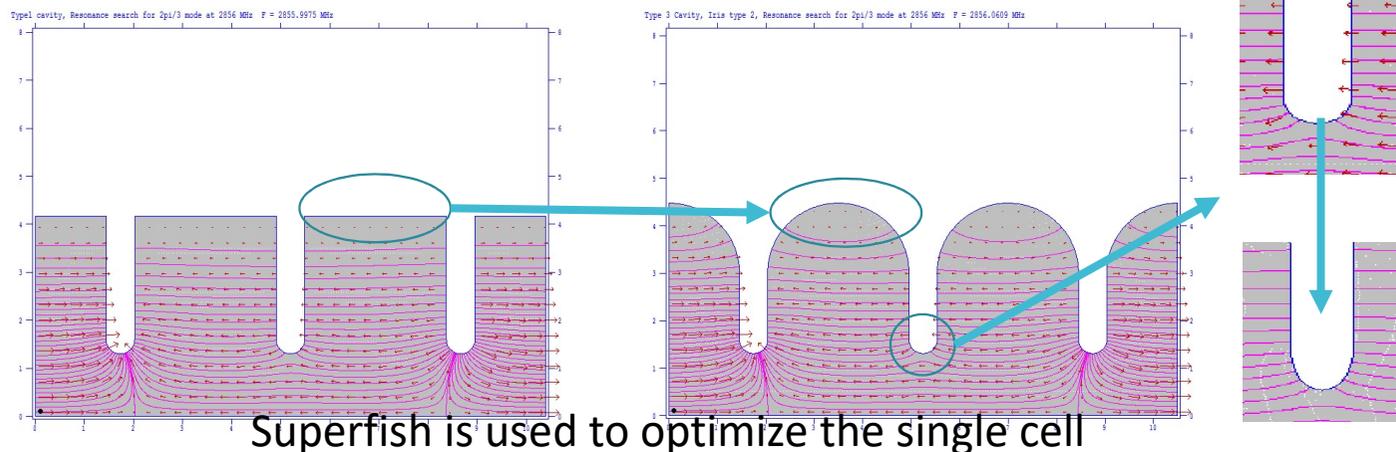


Buncher



Accelerating structure

- 3 meters long S band accelerating structure
- Cavity shape optimization
 - Rounding the cell :
 - ◆ Improve the quality factor by >12%
 - ◆ Reduce the power consumption
 - ◆ Increase the shunt impedance by ~10.9%
 - elliptical the irises shape ($r2/r1=1.8$)
 - ◆ Reduce the peak surface electrical field by 13%





Accelerating structure

- The main parameters of the whole structure

Parameters	Values	Unit
No. of Cells	84+2*0.5	-
Phase advance	$2\pi/3$	rad
Total length	3.1	m
Length of cell (d)	34.988	mm
Disk thickness (t)	5.5	mm
Shunt impedance (Rs)	60.3~67.8	MΩ/m
Quality factor	15465~15373	-
Group velocity: Vg/c (%)	2% ~ 0.94%	-
Filling time (t _f)	784	ns
Attenuation factor (τ)	0.46	Np
Power (@30MV/m)	74	MW



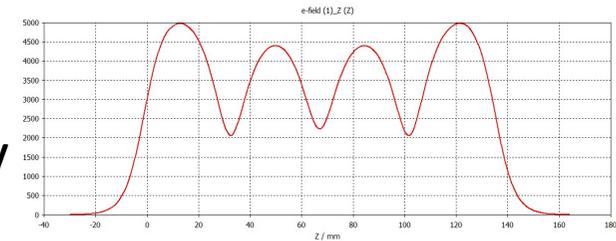
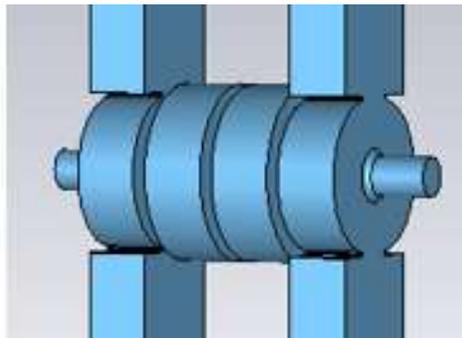
Accelerating structure

• Coupler design

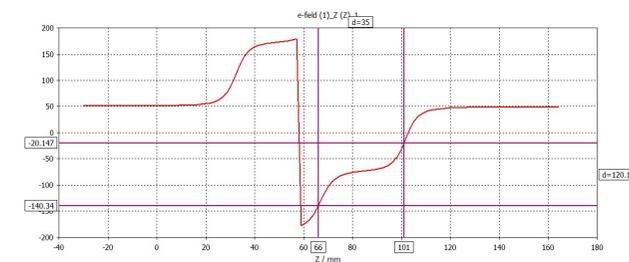
- The asymmetry of the coupling cavity will cause emittance growth
- The shape of the coupling cavity is racetrack dual-feed type

$$\varepsilon_{n-fin} = \sqrt{\varepsilon_{n-initial}^2 + \sigma_x^2 \left(\frac{\sigma_{\Delta p_x}}{mc} \right)^2}$$

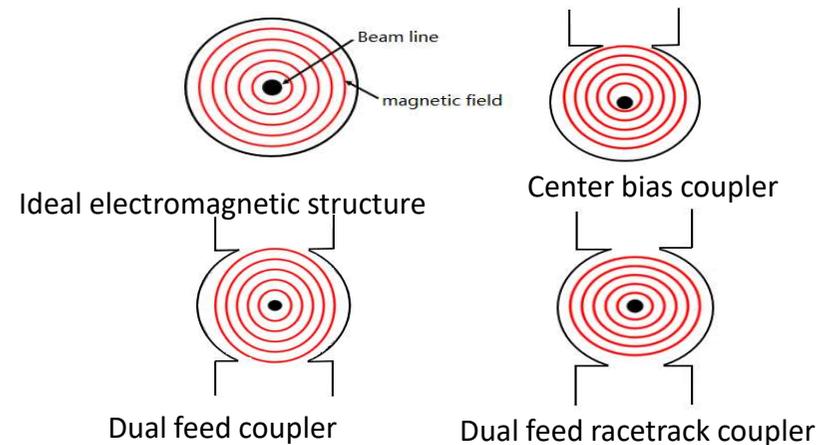
$$\Delta p_x = -\frac{e\Delta z E_0}{2\omega a} \left[\Delta\theta * \sin\varphi - \frac{\Delta E}{E_0} \cos\varphi \right]$$



The distribution of the electric field on axis



Phase advance per cell





Accelerating structure

- Factors to limit the gradient (cavity):

- Peak surface electric field (E_{peak})

- ◆ $E_{\text{peak}} < 160 \text{ MV/m}$ at S-band

- Peak surface magnetic field (H_{peak})

- ◆ pulsed heating effect will cause the temperature rise at the

coupler window. $\Delta T = \frac{|H_{\text{peak}}|^2 \sqrt{t_p}}{\sigma \delta \sqrt{\pi \rho c k}}$, for S-band $\Delta T < 50^\circ\text{C}$ is safe

- Modified Poynting vector (S_c)

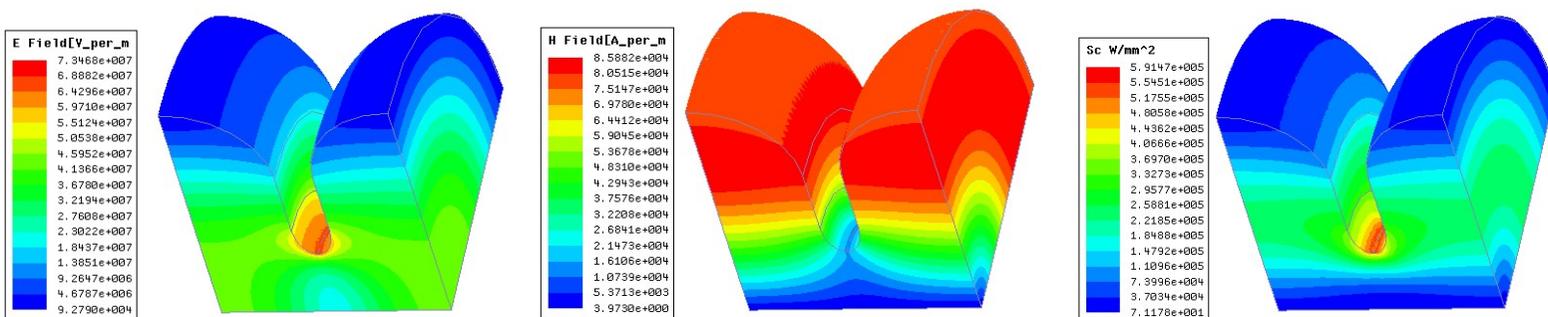
- ◆ $S_c = \text{Re}\{\bar{S}\} + \frac{\text{Im}\{\bar{S}\}}{6}$, $\frac{S_c^{15} t_p^5}{BDR} = \text{const.}$ If the beam break down rate is $1 \cdot 10^{-6} \text{ bpp/m}$, the safe value for $1 \mu\text{s}$ pulse length is 2.3 MW/mm^2

- Pulse length ($1 \mu\text{s}$)



Accelerating structure

- Factors to limit the gradient (cavity):
 - 3D program HFSS is used to confirm the design
 - The 1st cell adjacent the input coupler is simulated for $P_{in}=75$ MW
 - The values are safe. Both E_{peak} and Sc locates at the iris area



$E_{peak}=73$ MV/m.
Surface electric field

$H_{peak}=86$ kA/m.
Surface magnetic field

$Sc_{max}=0.59$ MW/mm².
Modified Poynting vector



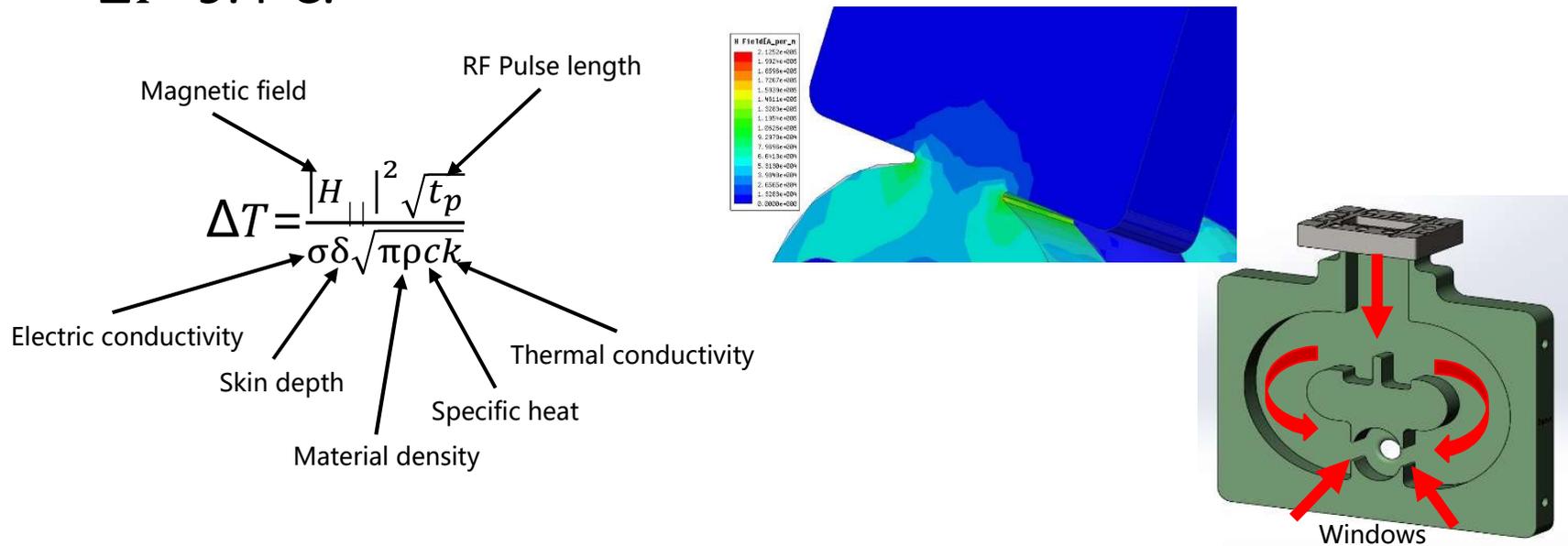
Accelerating structure

- Factors to limit the gradient (coupler):

- To reduce the pulsed heating, the coupler window edge is rounded.

- For S-band copper: $\Delta T [^{\circ}\text{C}] = 127 |H_{||} [\text{MA}/\text{m}]|^2 \sqrt{f \cdot [\text{GHz}] \cdot t_p [\mu\text{S}]}$

- For 75 MW input power, the maximum value of the peak surface magnetic field is $2.1 \cdot 10^5$ A/m. for $1 \mu\text{S}$ pulse length, $\Delta T = 9.4^{\circ}\text{C}$.

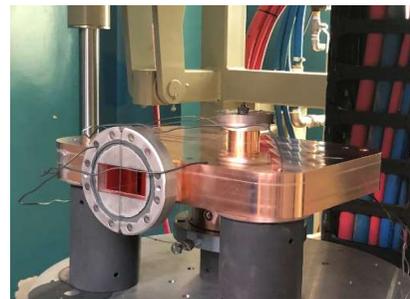




Accelerating structure

- Mechanical design

- Inner water-cooling has been adopted. 8 pipes are around the cavity.
- Compact coupler arrangements. The splitter is milling together with the coupling cavity.
- Two tuners are outside the cavity.

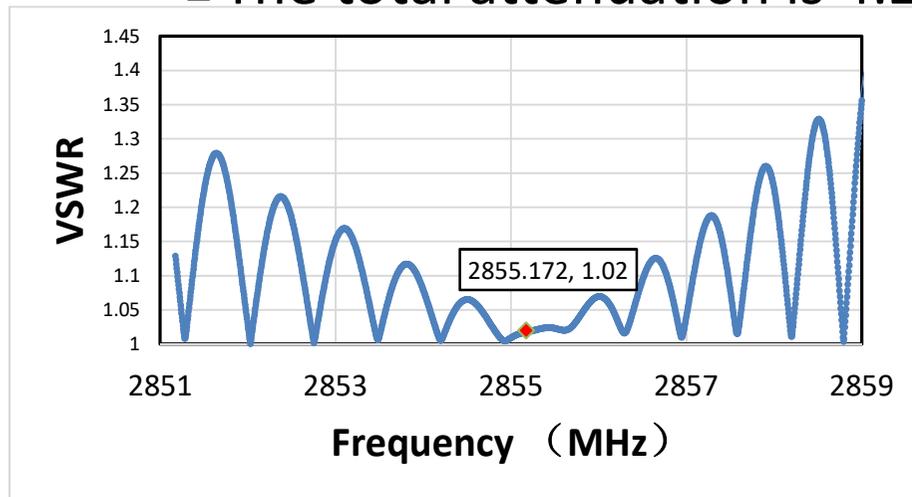
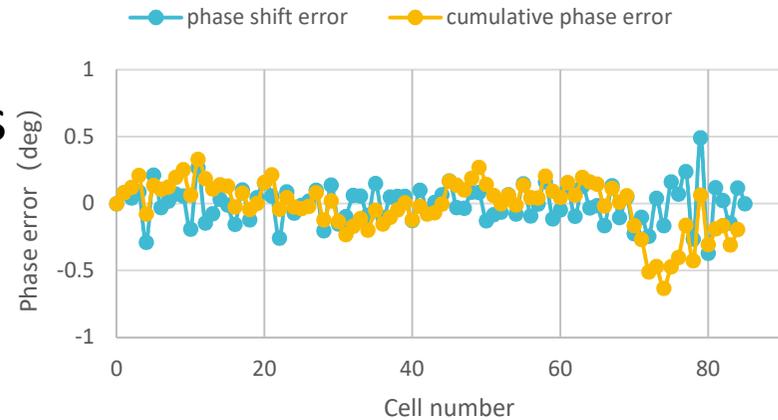




Accelerating structure

• Cold test result

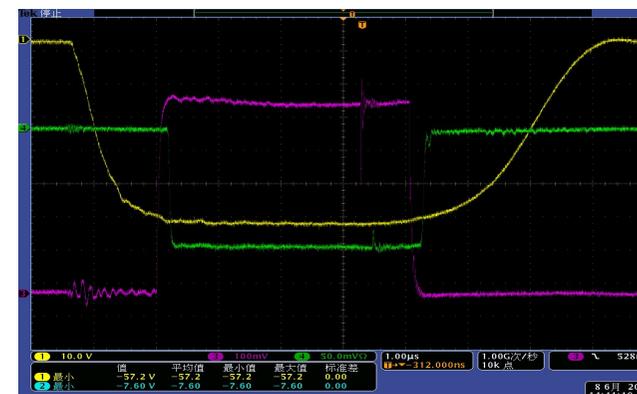
- The phase shift and the cumulative phase shift are less than 1 deg
- The VSWR is 1.02 at working frequency
- Filling time is 780 nS
- The total attenuation is 4.2 dB





Accelerating structure

- High power test result (with SLED)
 - The modulator voltage is 37.5 kV
 - the SLED energy multiplication factor: 1.8
 - The tested gradient has reached 33 MV/m



The waveform without SLED

$$P_{in} = \frac{(V * L)^2}{RL(1 - e^{-2\alpha L})M^2}$$

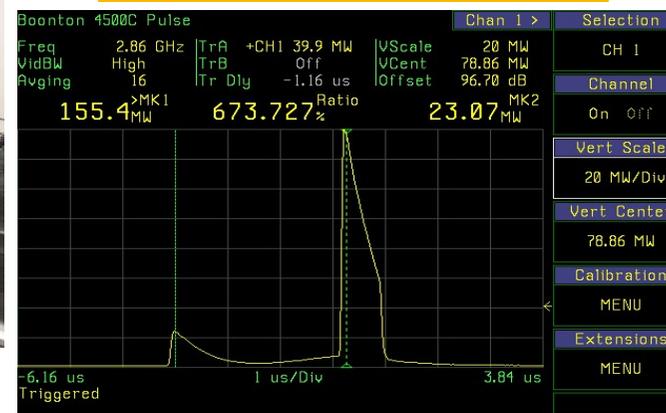


Modulator and klystron



High power test bench

The input power with SLED

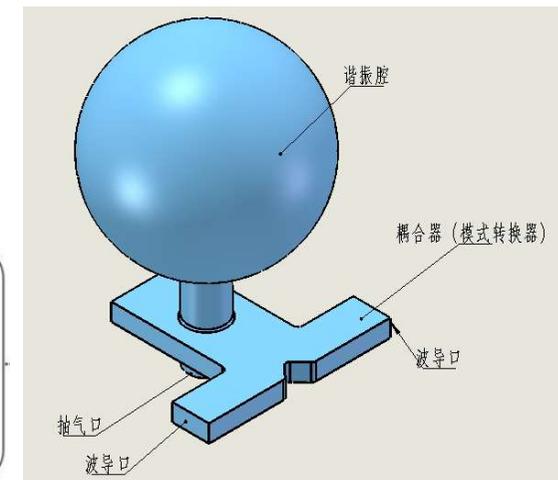
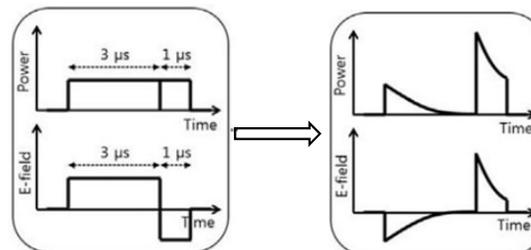
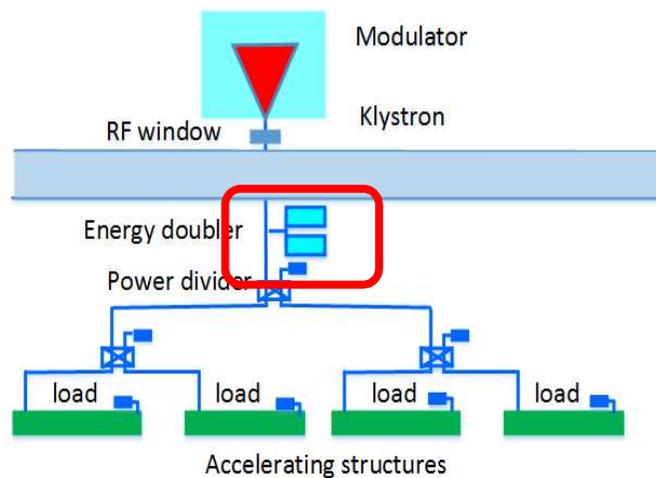




Pulse compressor

- It is used to improve the peak power from the klystron and saving cost
 - Input power: 80 MW
 - Pulse width: be compressed from $4\mu\text{s} \rightarrow 0.8\mu\text{s}$
 - Mode converter & spherical cavity

Parameter	Value
SLED water temperature	30 °C
Room temperature	25 °C
Filling time	780 ns
Klystron output power	80 MW
Pulse width	4 μs
Pulse repetition rate	100 Hz

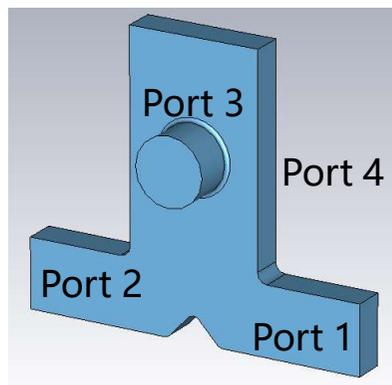




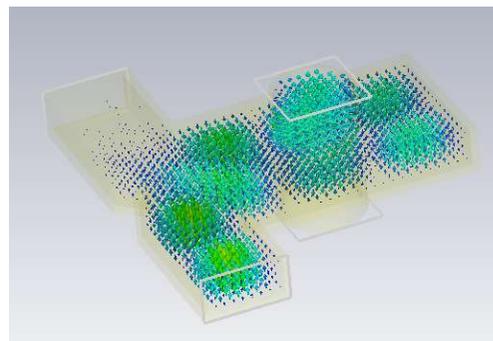
Pulse compressor

• Mode converter

- The TE₁₀ mode input from Port 1 will be converted into two degenerated TE₁₁ modes at Port 3
- There are two degenerated TE₁₁₃ modes in the spherical cavity, The phase difference of the two modes is about 90°
- The input port S₁₁ is -62.7 dB
- The S₄₁ is -71dB for port 4 is for vacuum



Vacuum model



Electromagnetic field

S11 / VSWR	-62.7 dB/1.0016
S21	-42.9 dB
S31(1)	-3.02 dB
S31(2)	-3.02 dB
Phase difference of two modes	89.89°
S41(1)	-70.9 dB
S41(2)	-71.0 dB



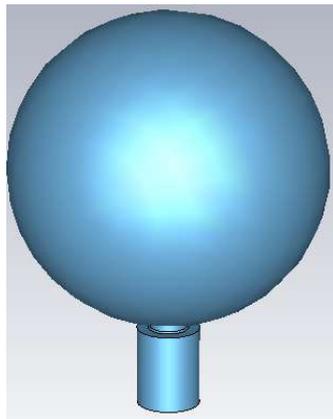
Pulse compressor

- Spherical cavity

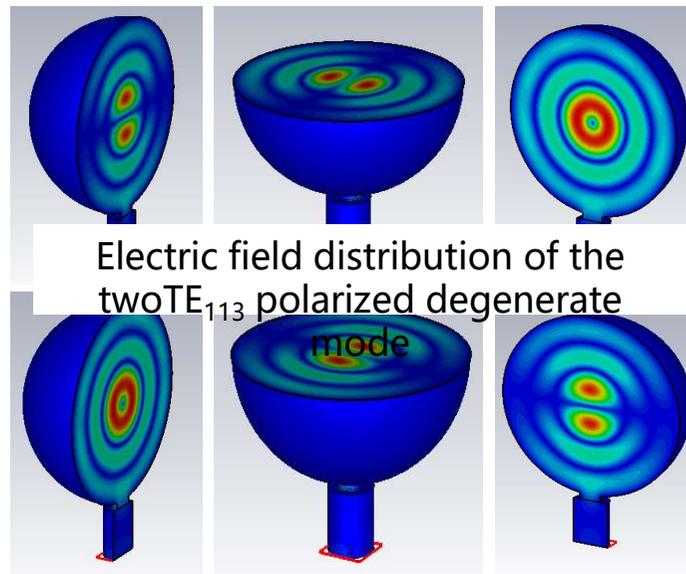
- Two degenerated TE_{113} mode in a single spherical cavity
- $f_0=2855.9986$ MHz, 2855.9994 MHz,
- $Q_0=139583$, 139551

- Cavity diameter

- 365mm



Simulation model



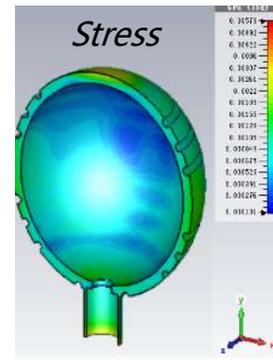
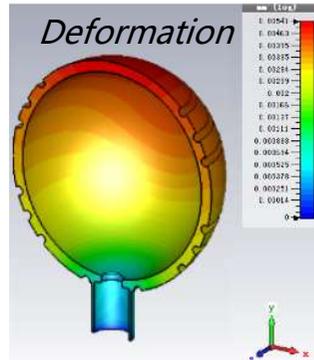
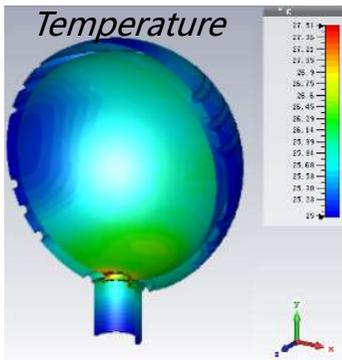
Parameter	value
VSWR	≤ 1.1
Coupling factor	~ 6.9
Tuning rang	$\geq \pm 1$ MHz
Peak power gain	≥ 7 dB
Energy gain factor	~ 1.6



Pulse compressor

- Thermal stress analysis

- The maximal temperature rise is on the coupling hole of 2.5 °C (the water cooling flow set as 50 L/min)
- The frequency tunable range of ± 1 MHz is enough for all the frequency shift resulted from the input power, vacuum pumping, air pressure, etc.

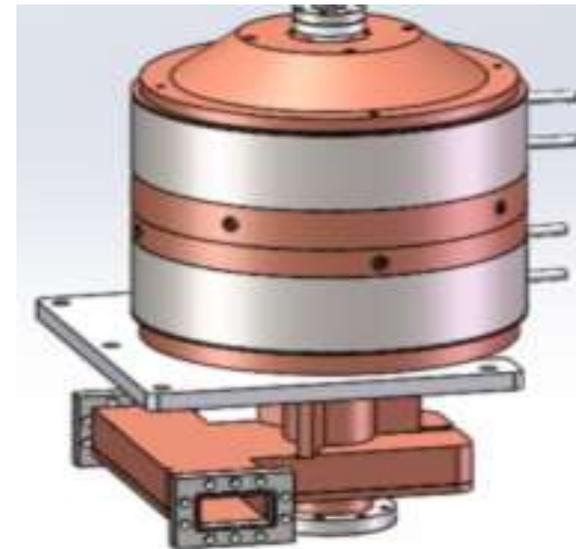
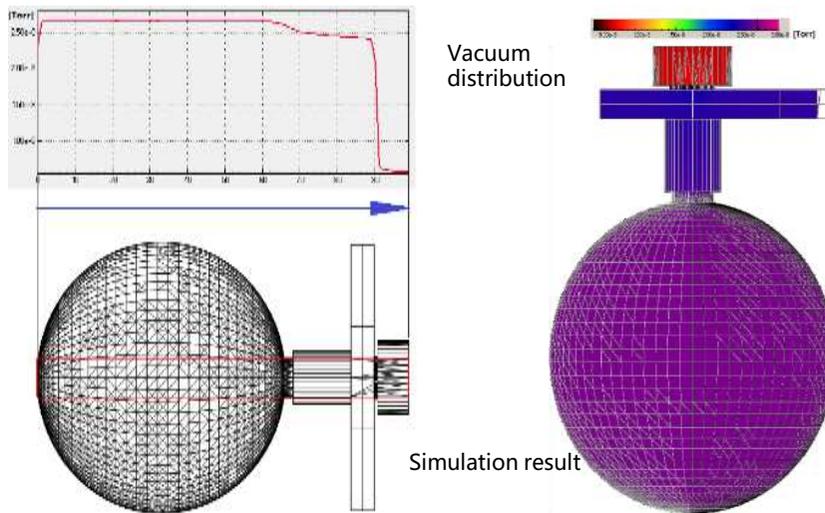


- Accordingly, if we use the water temperature to tune the frequency, the temperature need to be ± 3.6 °C change



Pulse compressor

- Vacuum speed and vacuum level
 - The pumping speed of the ion pump is 100 L/s
- Finished mechanical design





Positron Source

Layout of positron source

◆ Target (Conventional)

- ✓ tungsten@15 mm
- ✓ Beam size: 0.5 mm

◆ Electron Beam

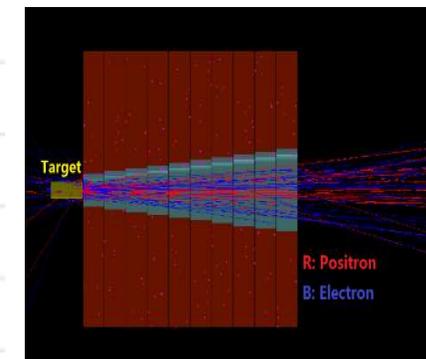
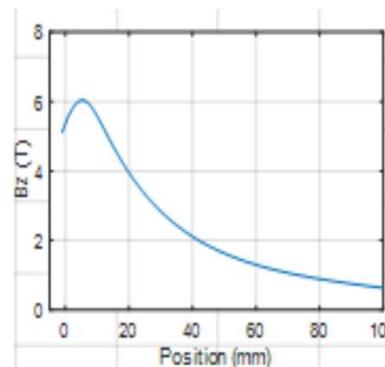
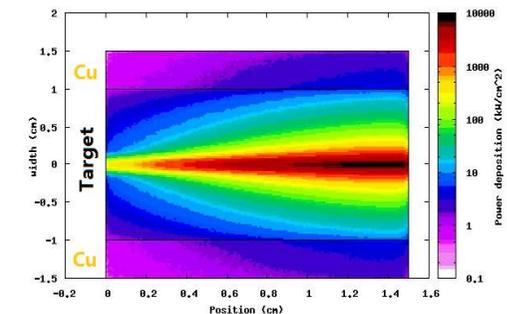
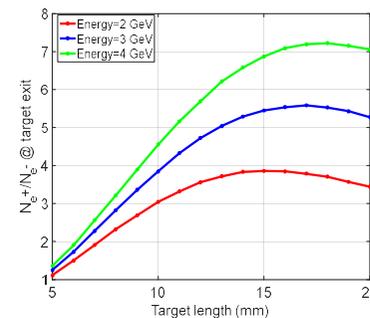
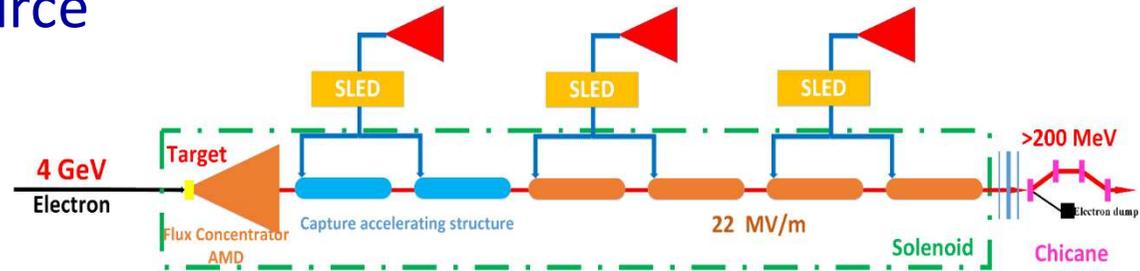
- ✓ 4GeV/10nC/100Hz
- ✓ Beam power 4kW

◆ Energy deposition

- ✓ 0.784 GeV/e⁻ @ FLUKA
- ✓ 784 W → water cooling

◆ AMD (Adiabatic Matching Device)

- ✓ Flux Concentrator
- ✓ Length: 100mm
- ✓ Aperture: 8mm → 26mm
- ✓ Magnetic field: (5.5T → 0T) + 0.5T

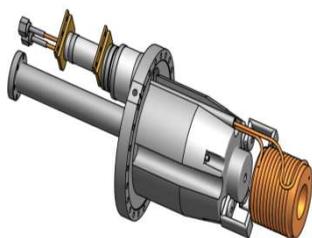




Positron Source

• FLUX concentrator

- It produces a pulsed magnetic field of 6 T to 0.5 T
- The maximum output value of the solid-state pulsed power generator is 15 kA / 15 kV / 5 μ s



The mechanical design of FLUX concentrator



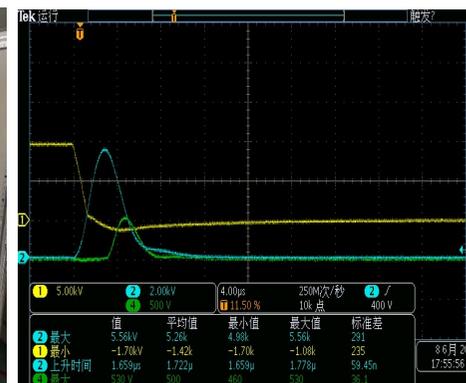
The finished FLUX concentrator



The test bench of the FLUX concentrator



solid-state pulsed power generator



The output of 10kA measurement

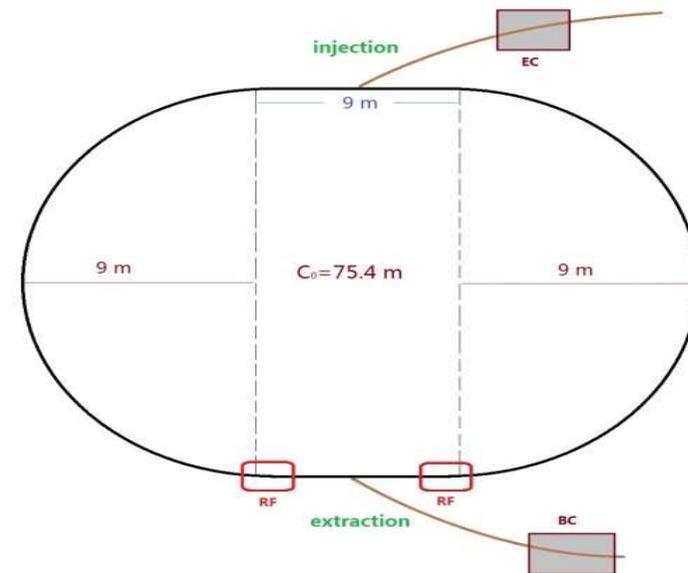
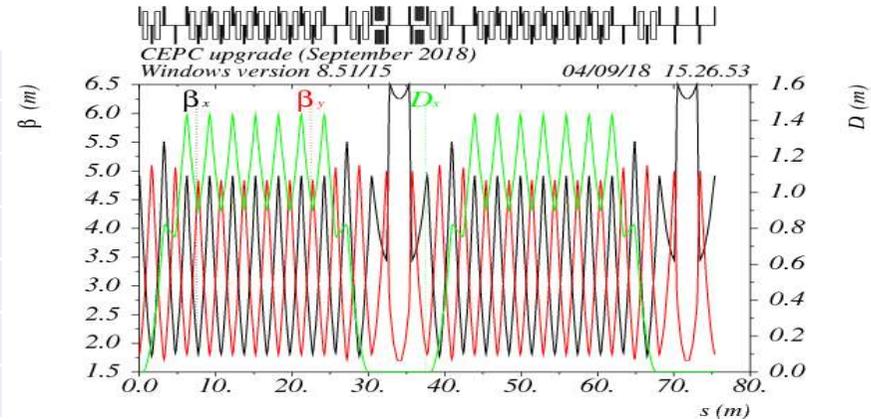


Damping Ring RF cavity

• Damping ring

DR V2.0	Unit	Value
Energy	GeV	1.1
Circumference	m	75.4
Storage time	ms	20
Bending radius	M	3.565
Dipole strength B_0	T	1.03
U_0	keV	36.3
Damping time x/y/z	ms	15.2/15.2/7.6
δ_0	%	0.05
ϵ_0	mm.mrad	376.7
$\sigma_{z, inj}$	mm	5.0
Nature σ_z	mm	7.5
ϵ_{inj}	mm.mrad	2500
$\epsilon_{ext x/y}$	mm.mrad	530/180
$\delta_{inj} / \delta_{ext}$	%	0.2/0.05
Energy acceptance by RF	%	1.0
f_{RF}	MHz	650
V_{RF}	MV	2.0

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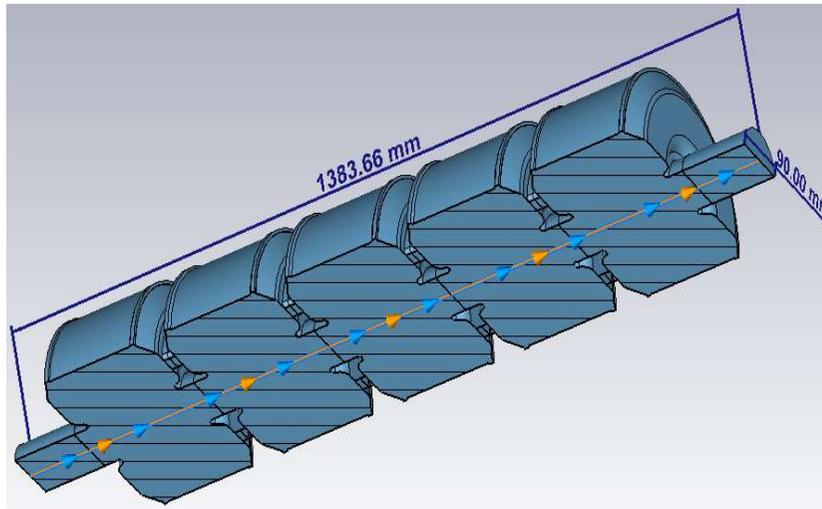


Damping Ring RF cavity

- HOM longitudinal impedance & threshold

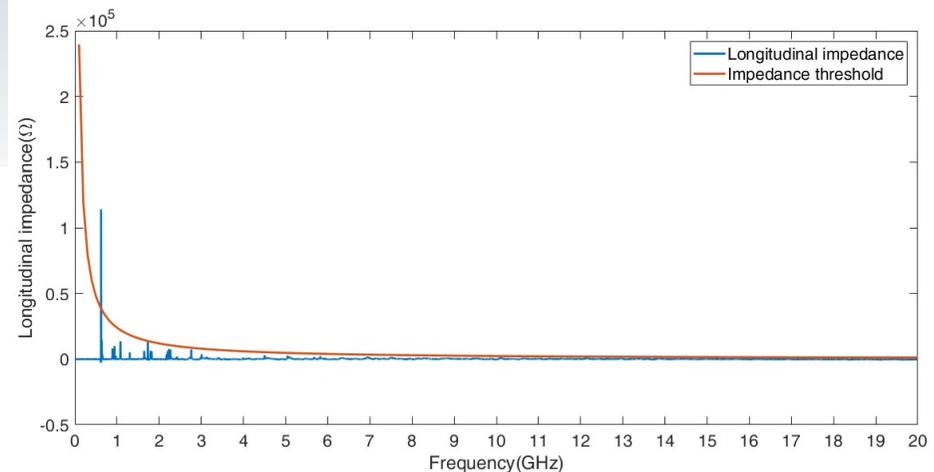
Y.D. Liu

- The cavity diameter is 90 mm



$k=4.12\text{V/pC}$
 $P=51.8\text{w}\&10\text{mA}$

Beta tune	3.84
Bunch length	5mm
Bunch number	2
Synchtron tune	0.062
Beam current	10mA



Longitudinal loss factor and power(σ_z & 5mm)

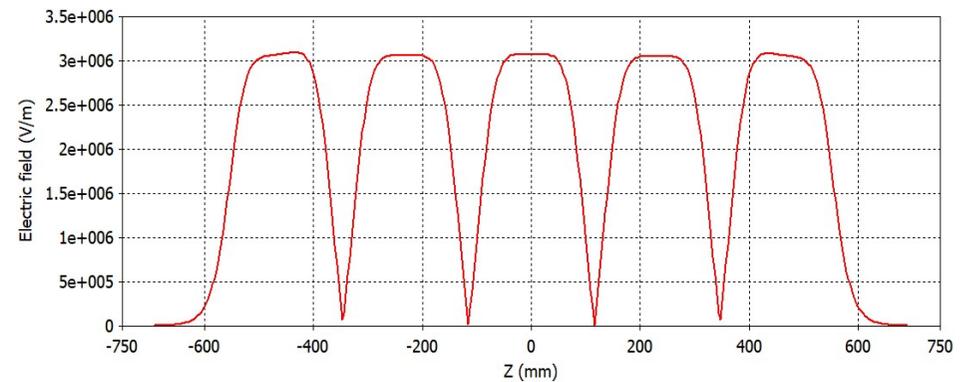
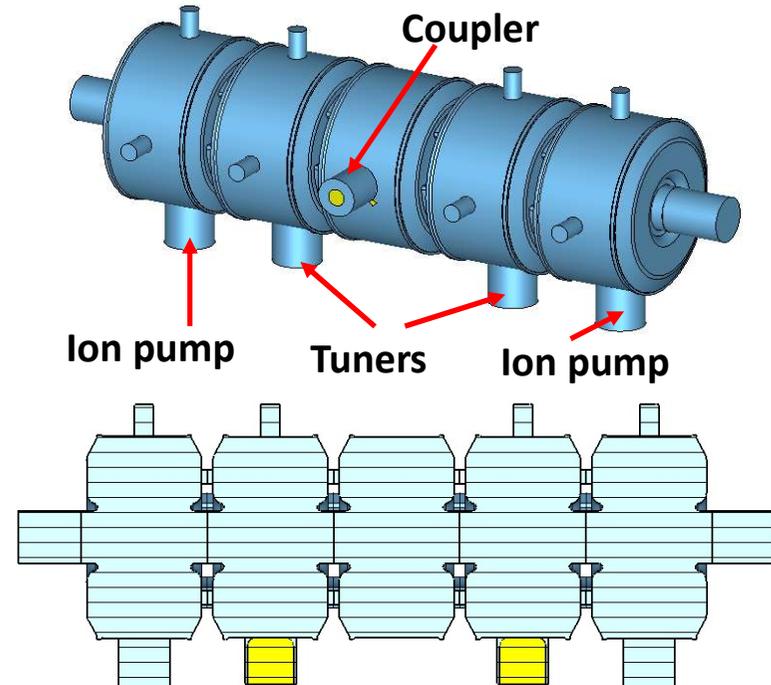


Damping Ring RF cavity

- Cavity design

- Fundamental mode: TM_{010}
- Parameters at field balancing

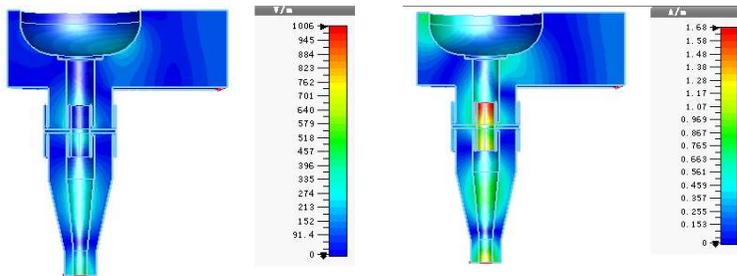
	Unit	Value
Beam tube aperture	mm	90
Cell length	mm	5*230.61
π -mode frequency	MHz	650.0
Q_0		32000
Shunt impedance	M Ω	16
$R/(Q*I)$	Ω/m	430
Accelerating voltage	MV	1.0 (1.2)
Accelerating gradient	MV/m	0.87 (1.04)
Dissipated cavity power (20% margin)	kW	38 (54)



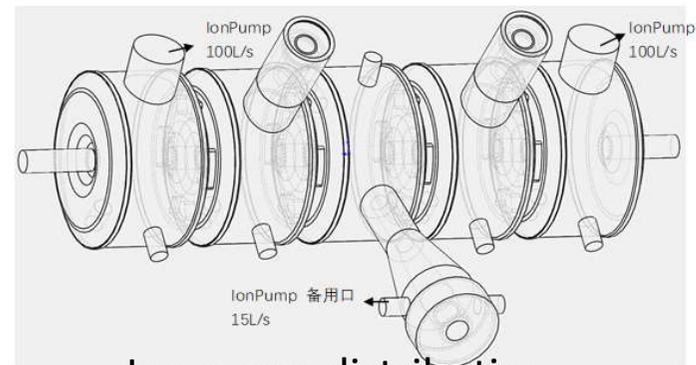


Damping Ring RF cavity

- Input coupler, doorknob and tuner
 - The diameters of neck tubes of tuner and vacuum ports are 94mm
- Vacuum
 - 2 pump ports near the ceramic of coupler and 1 pump port for each tuner with flanges CF35 are considered
 - The inner diameters of these pump ports are 38mm



Electromagnetic field distribution



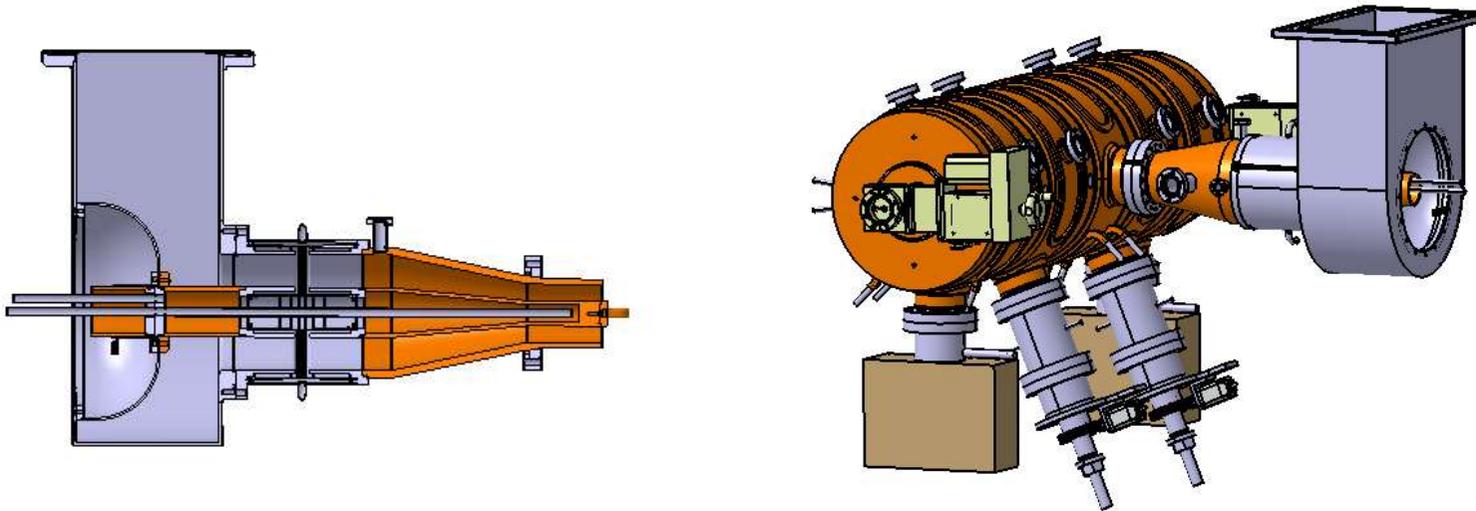
Ion pump distribution



Damping Ring RF cavity

- Mechanical design

- The preliminary design has finished
- Multiple iteration with the physical design of the DR, RF design and mechanical design is needed





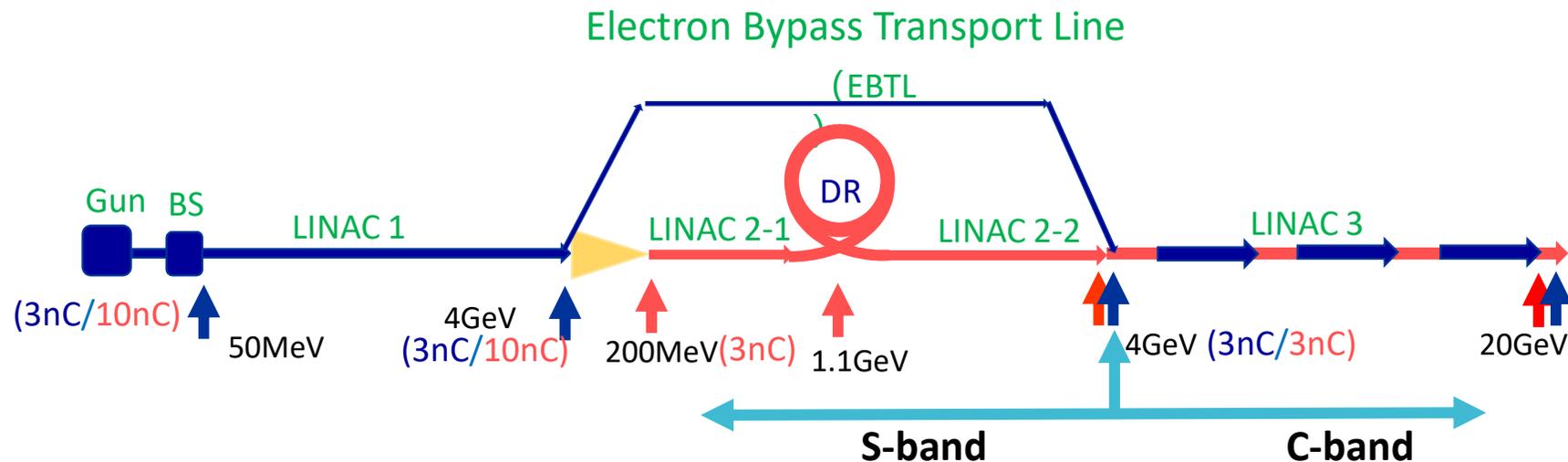
Linac alternative

- Linac design must match booster requirement
- As long as the booster requirement changes, the linac must give the corresponding design
 - High luminosity scheme at Higgs energy
 - ◆ The linac beam emittance 40nm (CDR) → 10 nm
 - Full injection for Z(2T_39MW)



Linac alternative

- 20 GeV linac
 - Reduce the difficulty of the Booster design
 - Reduce the technical risk of low magnetic field magnets of the Booster
- S-band+C-band RF system
 - C-band start energy: 4GeV





Linac alternative

- 20 GeV linac (S-band + C-band)
 - The gradient of C-band structure is 45 MV/m
 - The total length is 1.4 km, 200 m longer than the baseline design

The main parameters of the linac exit

Parameter	Unit	S-band	C-band
Frequency	MHz	2860	5720
Length	m	3.1	1.8
Cavity mode		$2\pi/3$	$3\pi/4$
Aperture diameter (mm)	mm	20~24	11.8~16
Gradient	MV/m	21	45

Parameter	Symbol	Unit	Baseline	Alternative
e^-/e^+ beam energy	E_{e^-}/E_{e^+}	GeV	10	20
Repetition rate	f_{rep}	Hz	100	100
Bunches/pulse			1	1
e^-/e^+ bunch population	N_{e^-}/N_{e^+}		$>9.4 \times 10^9$	$>9.4 \times 10^9$
			nC	$>1.5 (3)$
Energy spread (e^-/e^+)	σ_E		$<2 \times 10^{-3}$	$<2 \times 10^{-3}$
Emittance (e^-/e^+) Req.	ϵ_r	nm	< 40	< 20
Length	L	m	1200	1400

The main parameters of the C-band structure



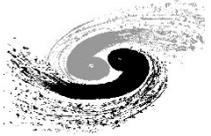
Linac alternative

- Full injection for Z(2T_39MW)
 - Two bunches/pulse
 - ◆ Preliminary evaluation
 - Physics design/control system/instrumentation
 - Repetition: 200 Hz
 - ◆ RF Power source: no mature product
 - Modulator: The price increased by 1 times
 - Klystron: The price increased by 1.5 times
 - ◆ RF system (The average power increase 1 times)
 - Load
 - Water cooling



Summary

- The linac baseline design is a 10 GeV S-band accelerator
- The key components of the linac baseline are being developed. The accelerating structure, the spherical pulse compressor, The FLUX concentrator and damping ring RF cavity
- According to the change of the booster requirement, the linac has made the corresponding considerations



Thank you for your attention!