

Fatigue crack propagation accelerated by mercury immersion

Japan Atomic Energy Agency

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Motivation and purpose

Bending fatigue test in mercury

with large indent *Briefly explain the previous experiment*

with notch *To investigate the fatigue crack propagation*

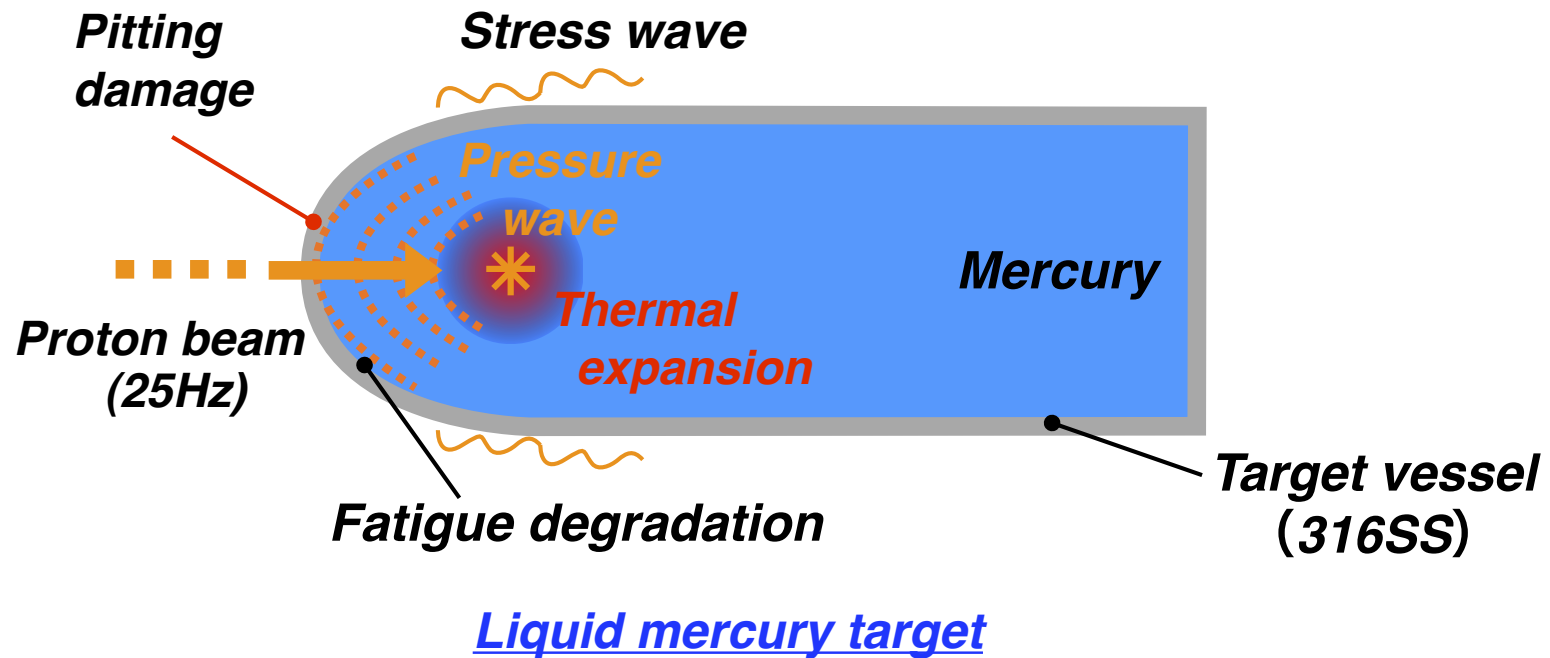
Fatigue crack propagation

Crack length estimated by FRASTA method with O.D. measurement
(FRActure Surface Topography Analysis)

Crack growth rate VS. Stress intensity factor

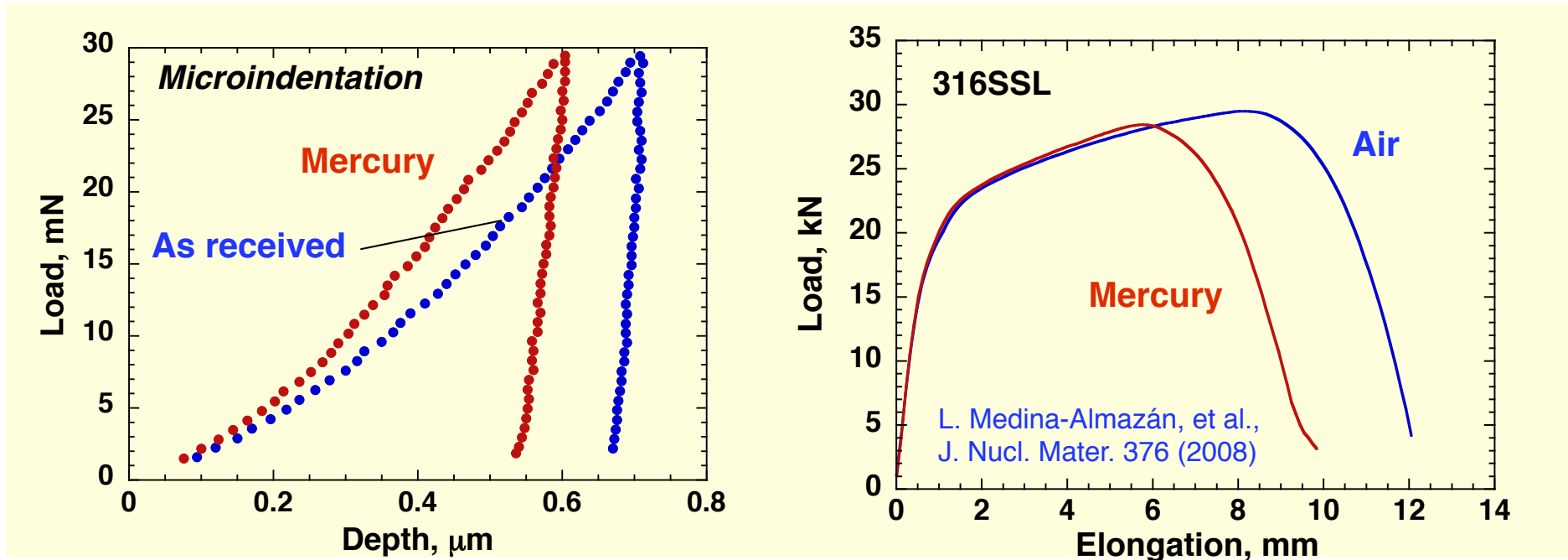
Summary

Motivation



- Mercury target vessel is exposed to severe environments
Radiation damage, Pressure wave, Cavitation damage, Repeated stress
Remarkably decreases the structural integrity of the target vessel
- To improve the structural integrity;
Surface modification, Microbubble injection into the mercury
- **Liquid Metal Embrittlement (LME)** may decrease the structural integrity

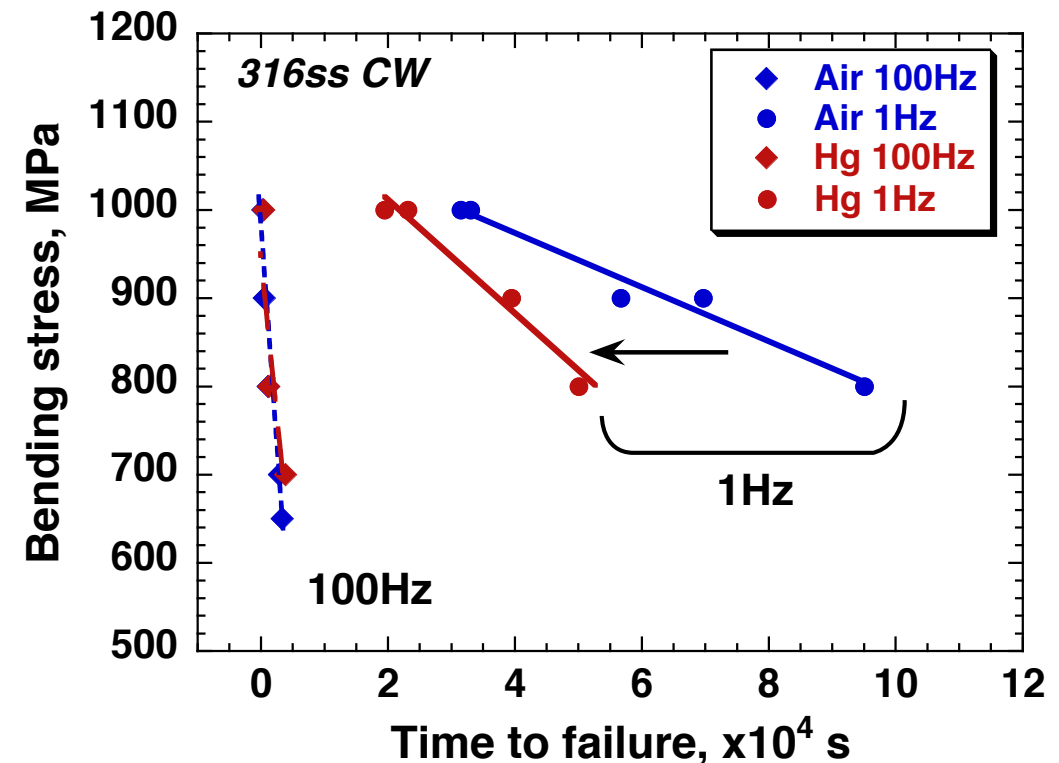
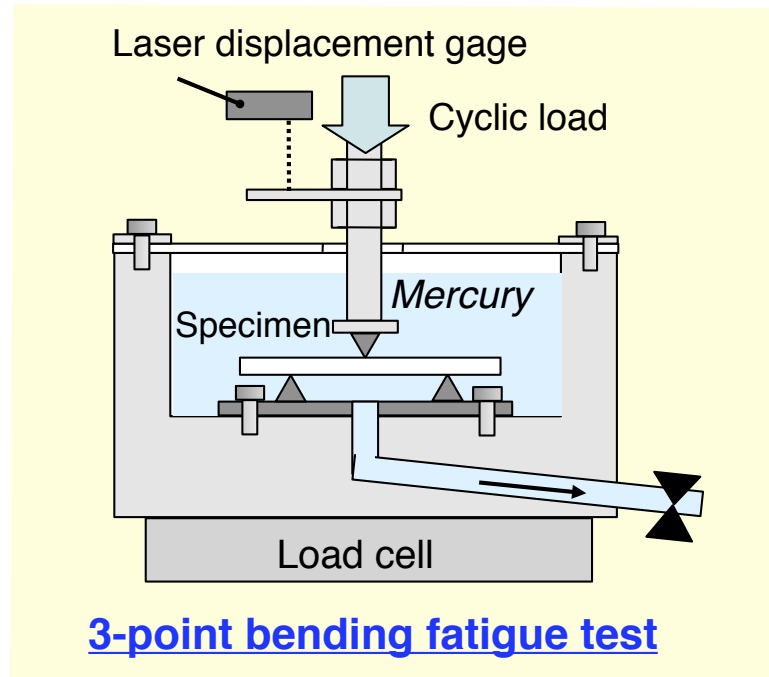
LME between mercury and 316SS



- LME occurs in the specific combination between the solid and liquid metals
- Sub surface layer hardened after mercury immersion
- Static elongation decreased by mercury immersion
- Degradation of low cycle fatigue strength was reported.

Strizak, et al, J.Nucl. Mater. 343 (2005), Futakawa, et al., J.Nucl. Mater. 356 (2006).

Fatigue strength in mercury

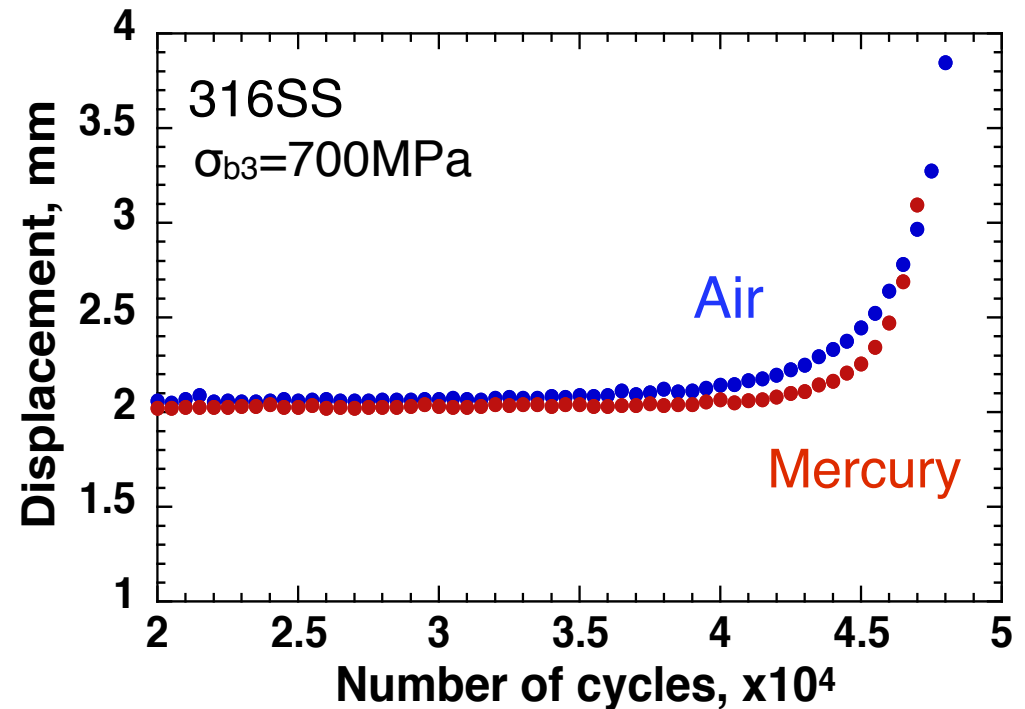
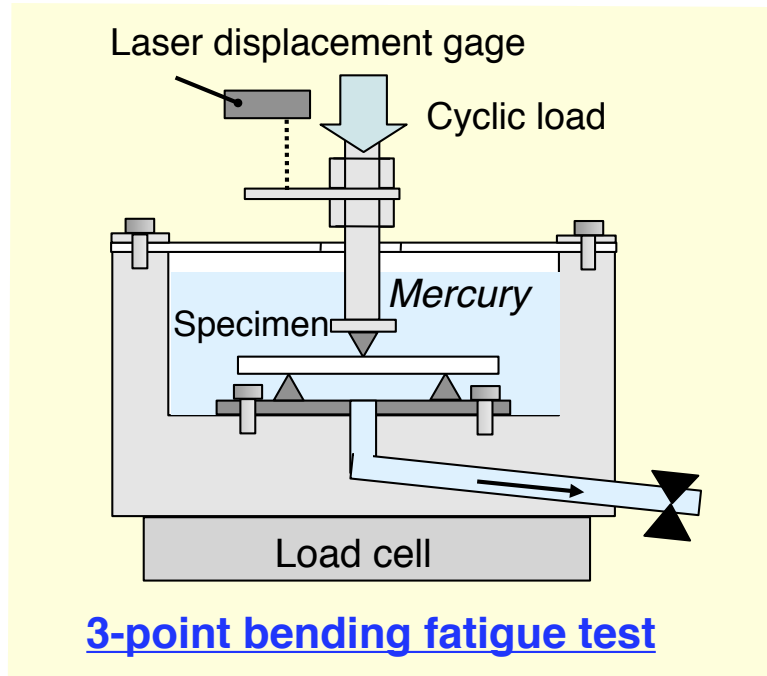


- Fatigue strength in mercury decreased depending on the time
- Displacement just before failure was slightly accelerated by mercury
- Detailed information on fatigue crack propagation was not obtained (the specimen was fully-immersed in mercury)

Purpose in this work

Evaluation of the effect of mercury on fatigue crack propagation

Fatigue strength in mercury

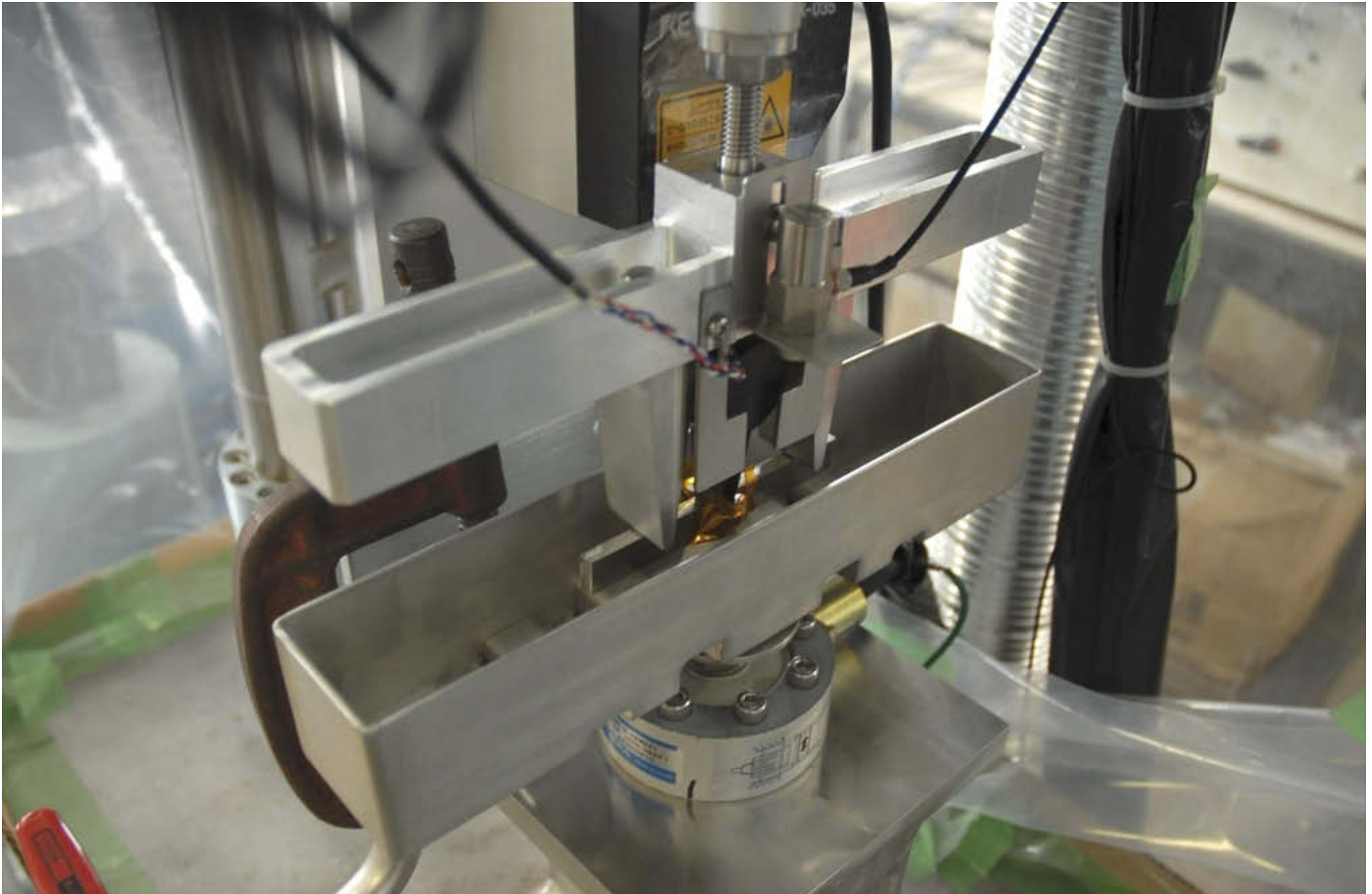


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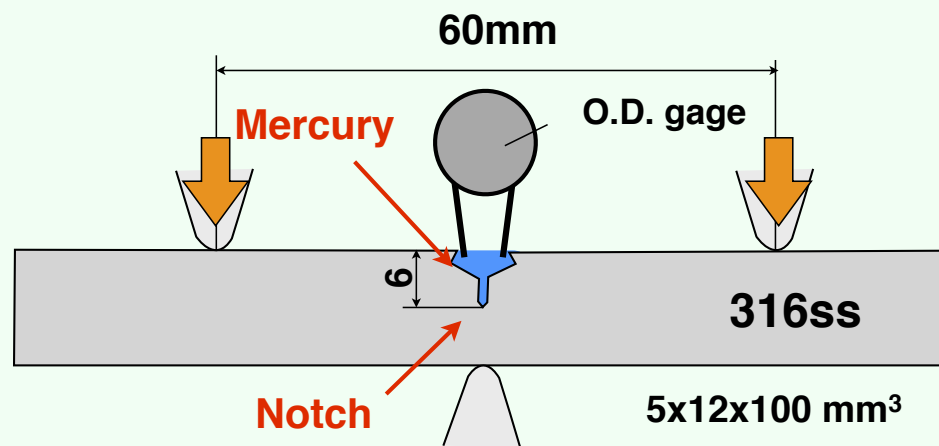
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V-notch fatigue test



V-notch fatigue test

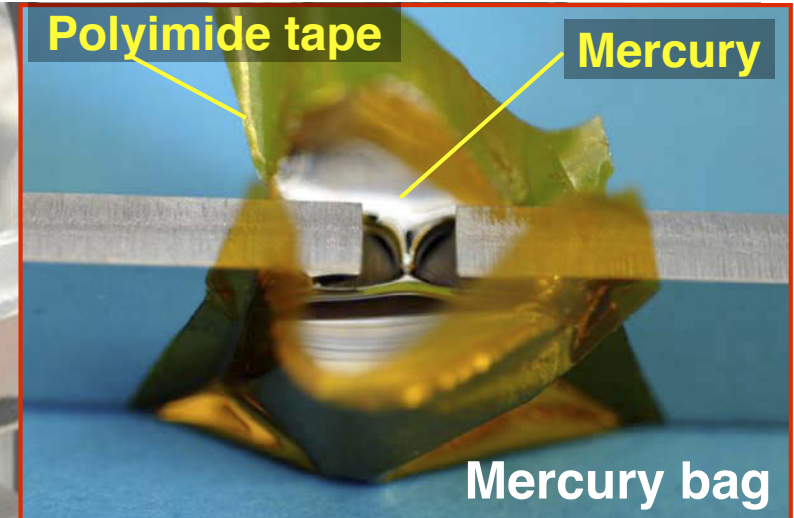


3-point bending fatigue test with V-notch

Specimen: 316ss (5x12x100mm)
Load control: Sine wave
Stress ratio: Max./Min.=0.1

Frequency: 1 Hz --Mercury effects depends on testing time
Based on the previous experiment

- Prepared V-notch (6mm in depth) to limit the failure point and partly immerse in mercury
- Filled mercury (2cc) in mercury bag for mercury condition
- Measured opening distance of the notch to estimate the crack length



S-N curves

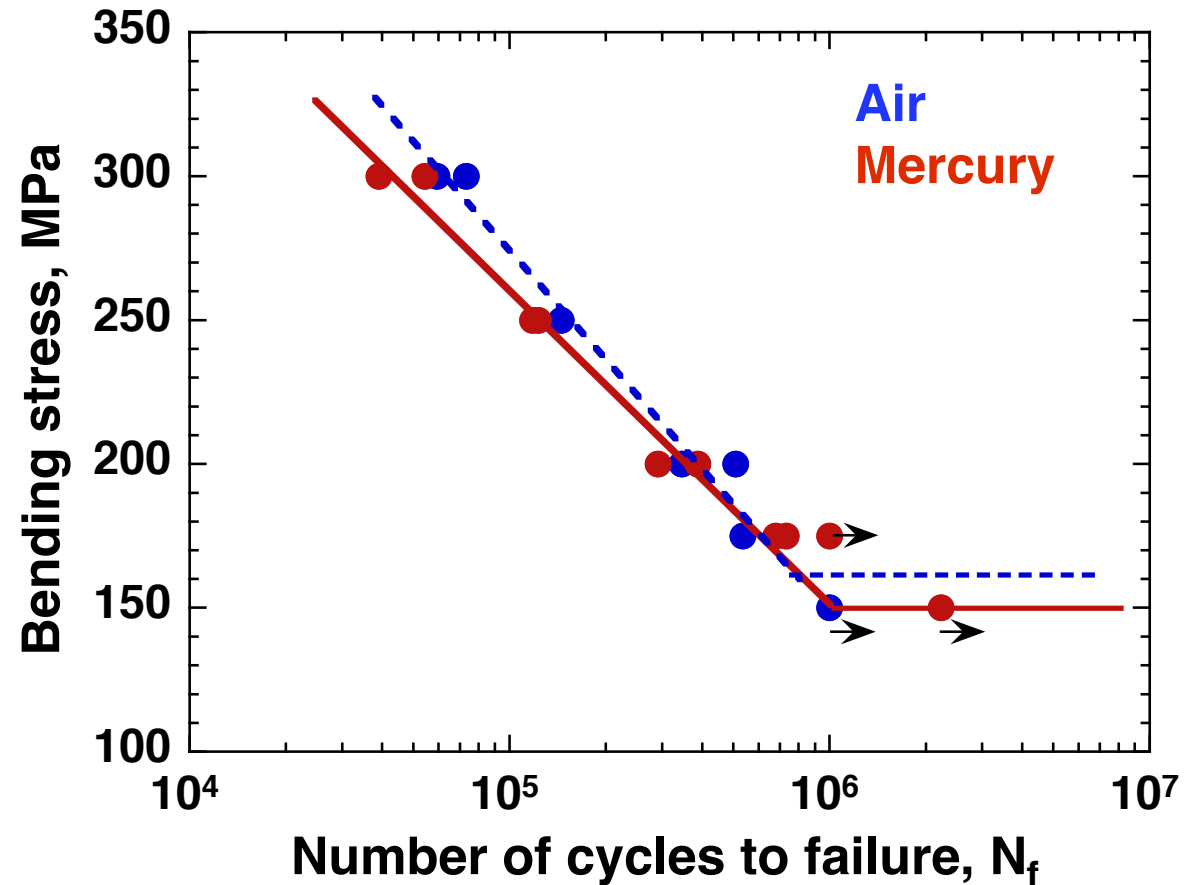
Bending stress

$$\sigma_{b3} = \frac{3PL}{2bd^2}$$

P: Max. load

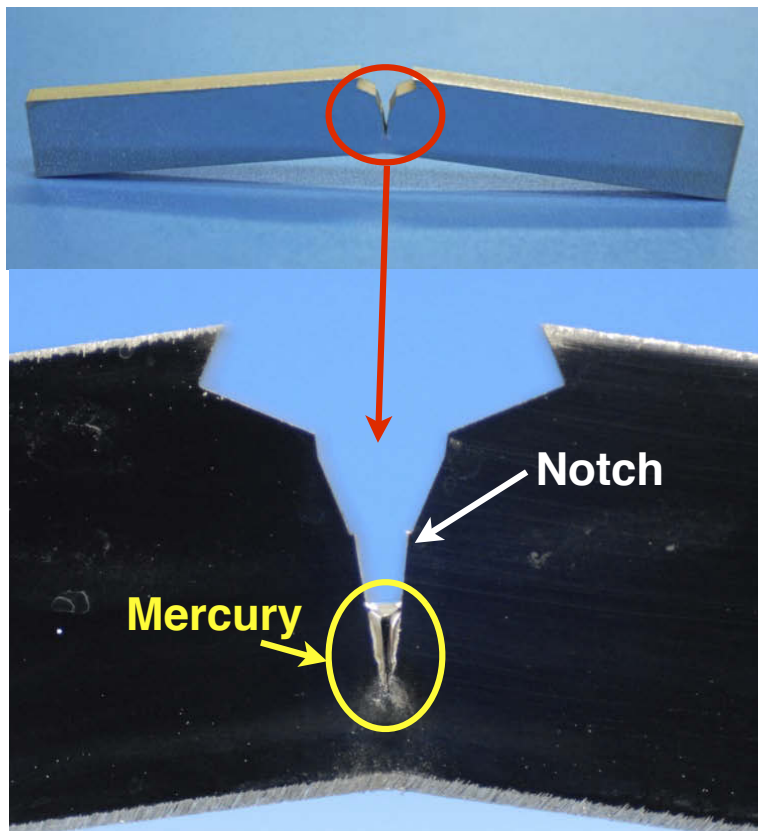
L: Span

b,d: Width and thickness

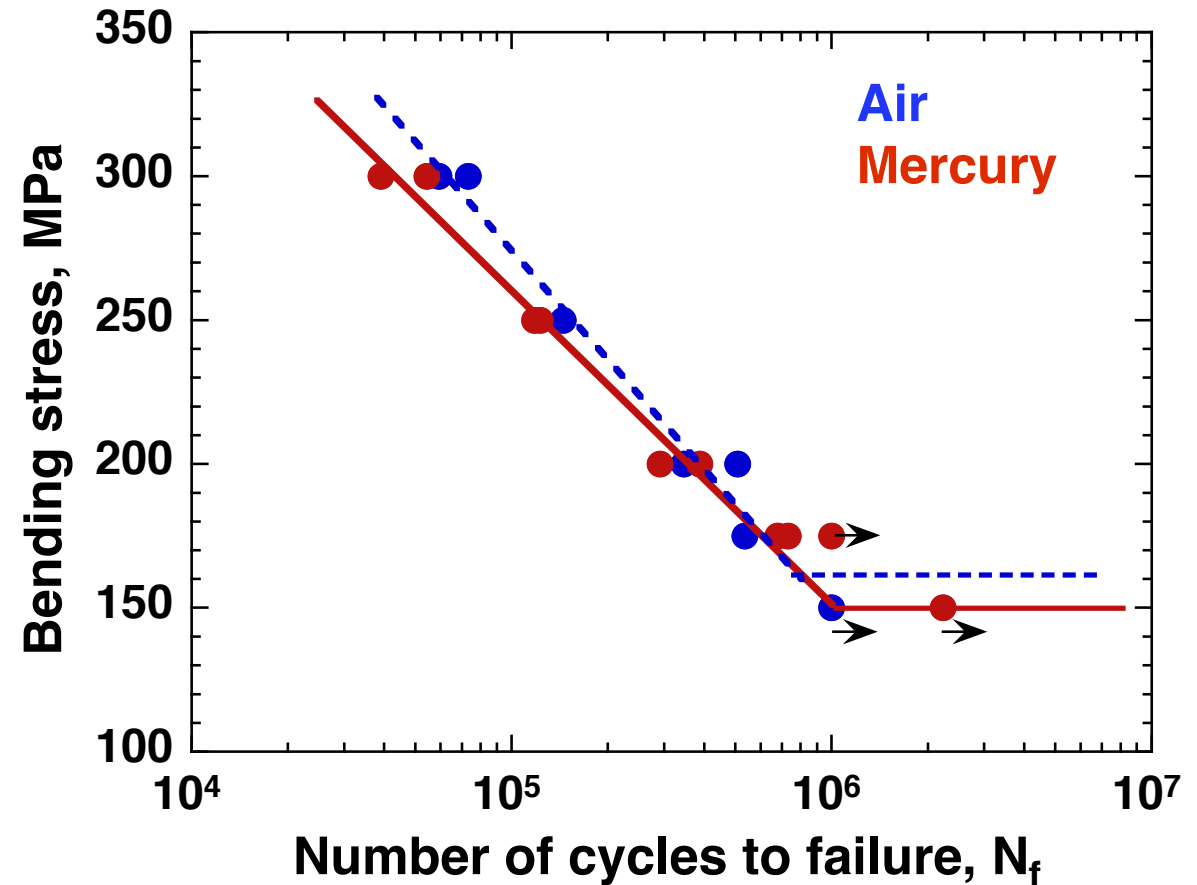


- Crack tip completely-wet from mercury
- N_f in high-stress imposed area was decreased by mercury
- N_f in low stress imposed area was increased by mercury

S-N curves

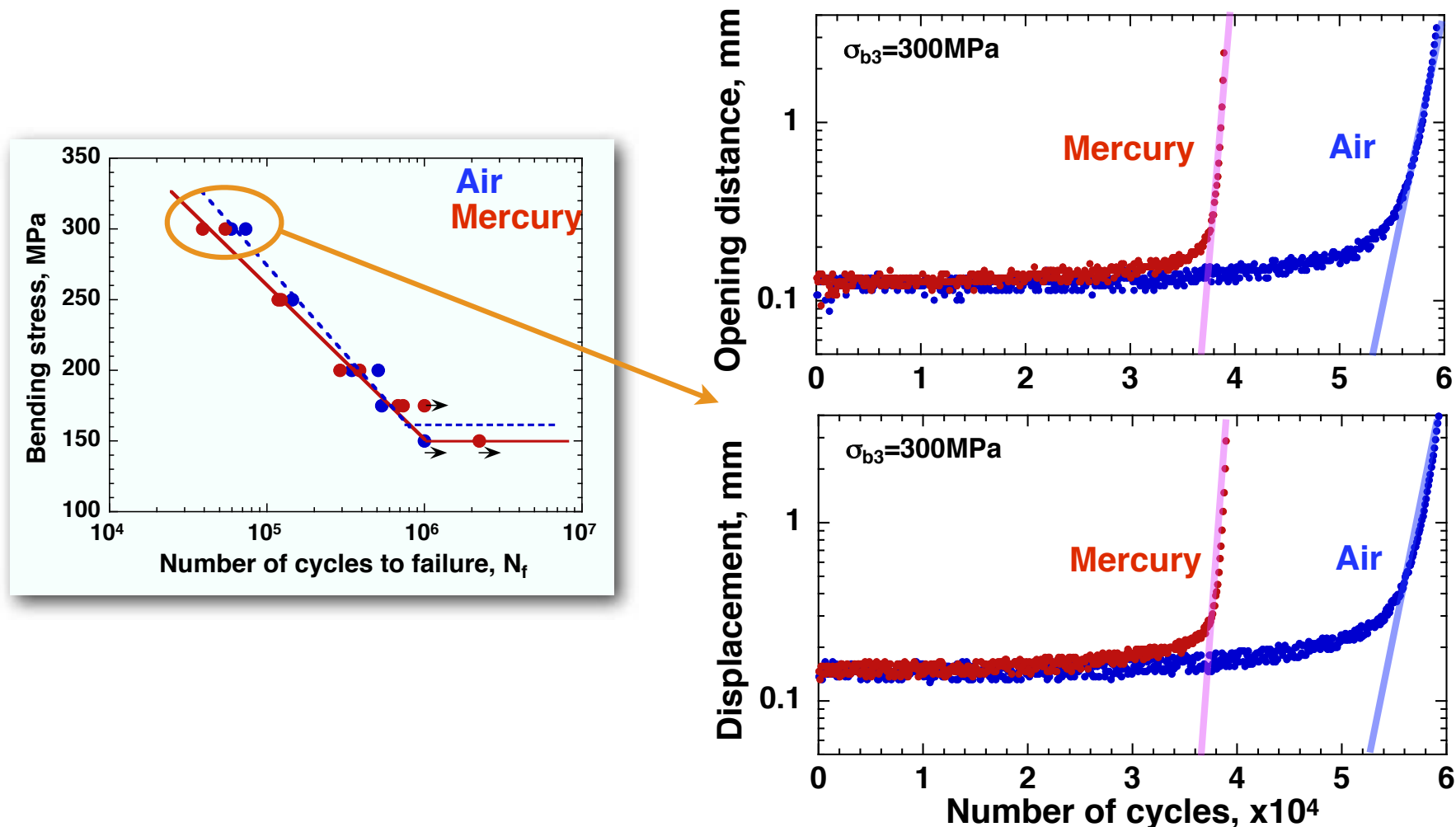


Crack tip after failure



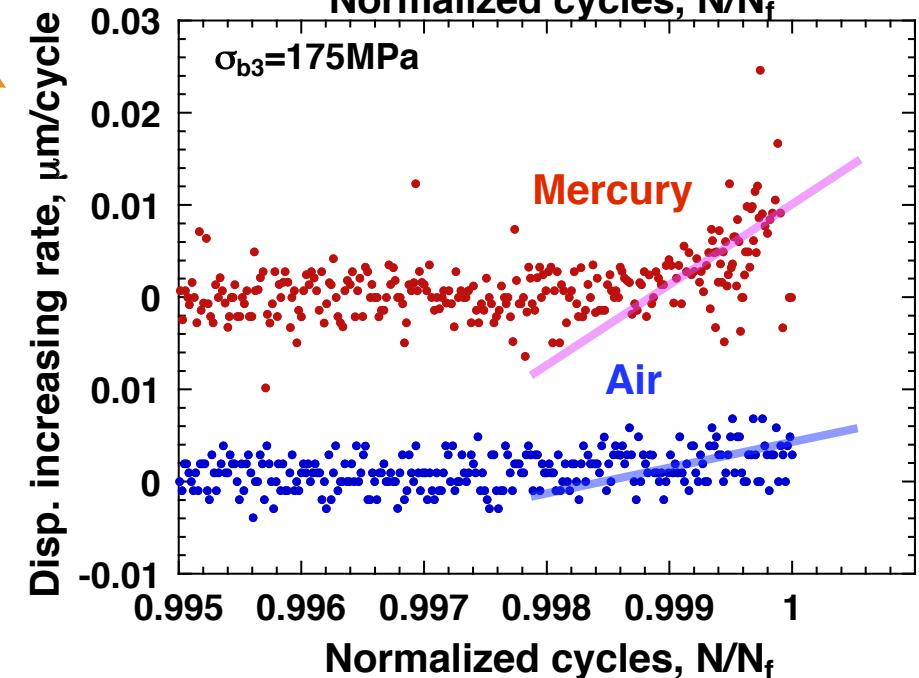
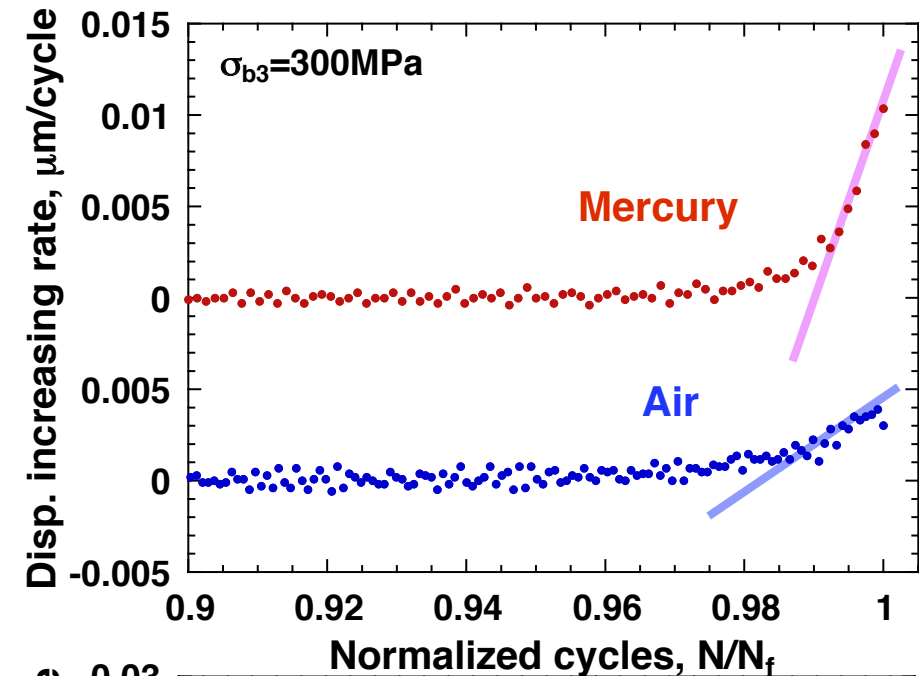
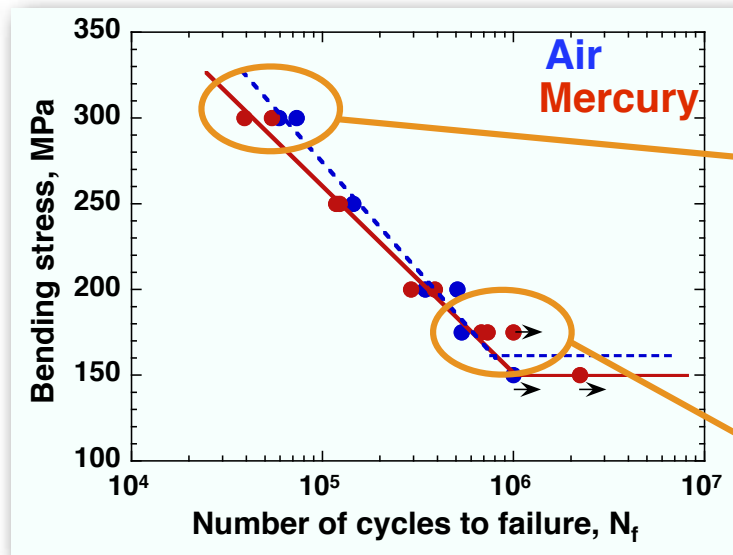
- Crack tip completely-wet from mercury
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Opening distance



- Confirmed an adequate correlation between the opening distance and the crosshead displacement
- Opening distance for mercury case at just before failure was sharply increased compared with the air case.

Increasing rate of the displacement



- Increasing rate of the displacement accelerates by mercury immersion regardless of the imposed stress

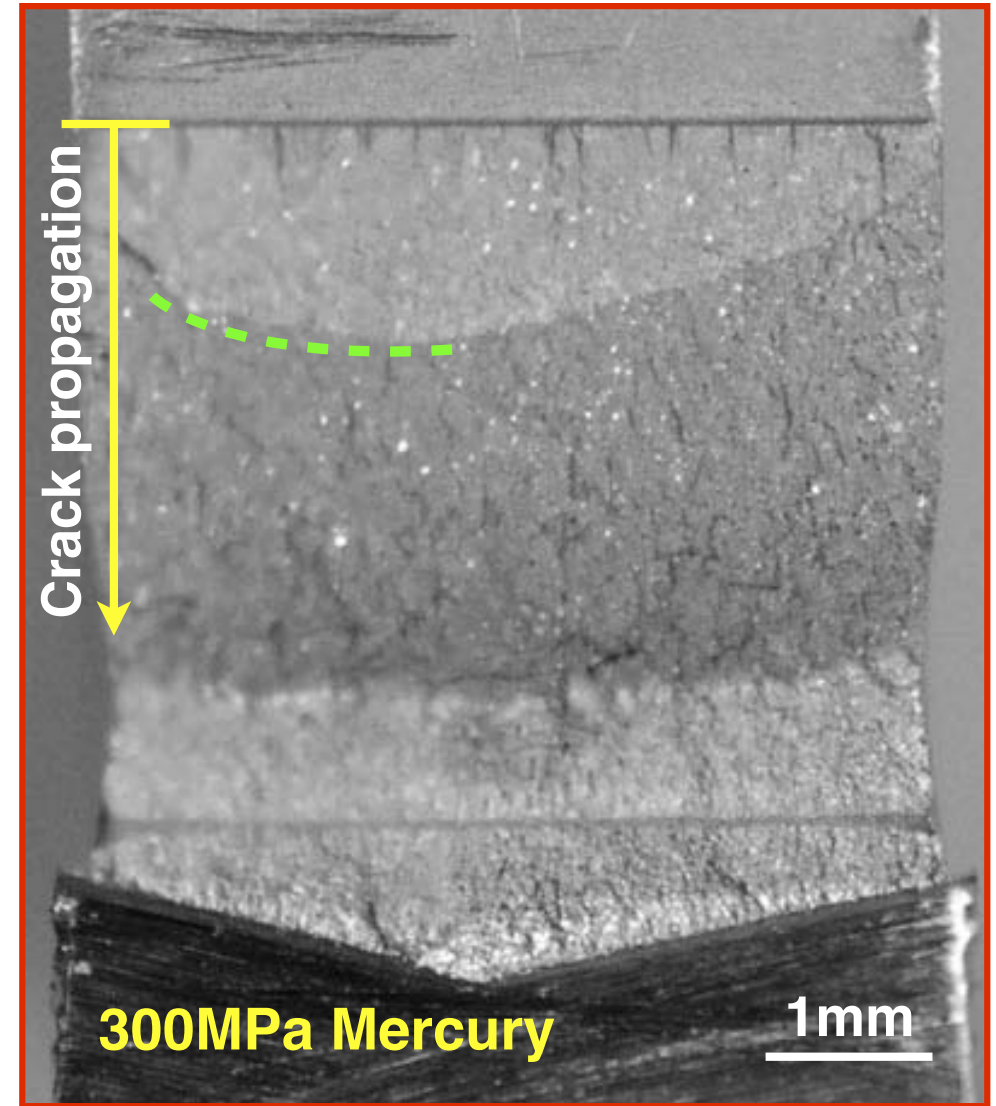
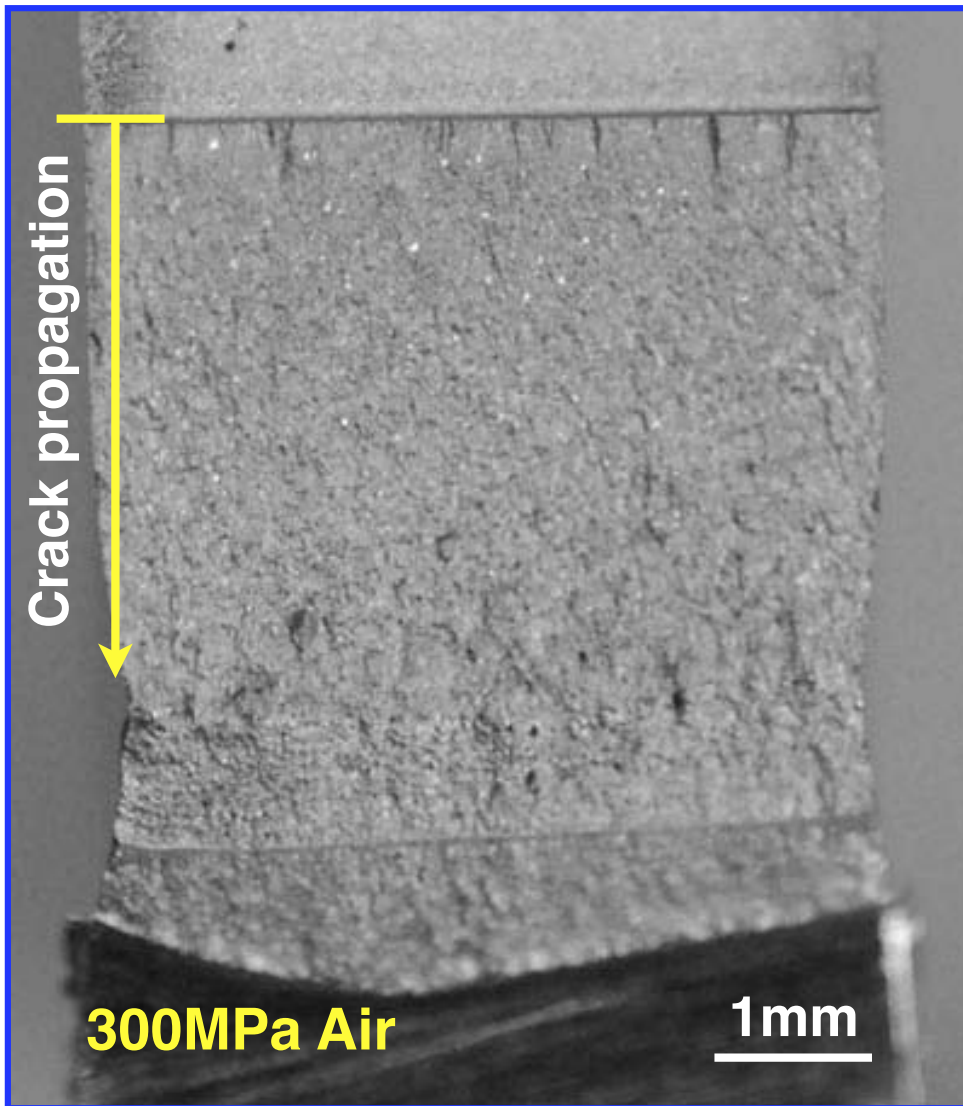
Effect of mercury on fatigue...

✓ **Strength**

✓ **Displacement change**

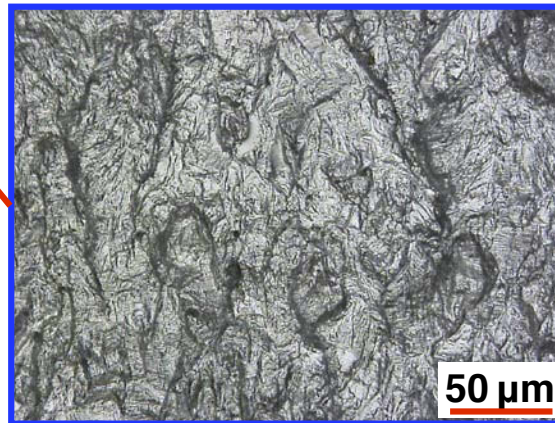
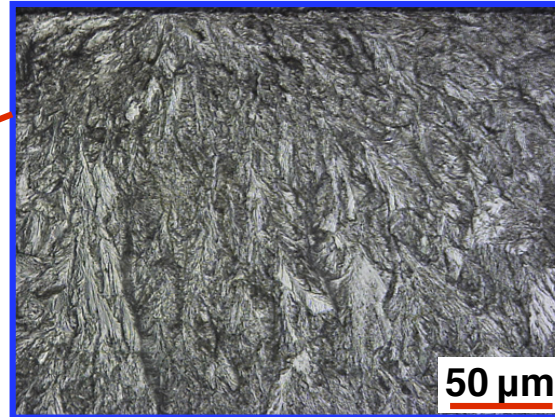
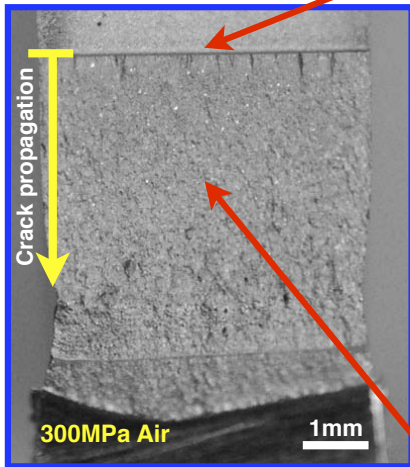
➡ **Crack propagation**

Fracture surface observation

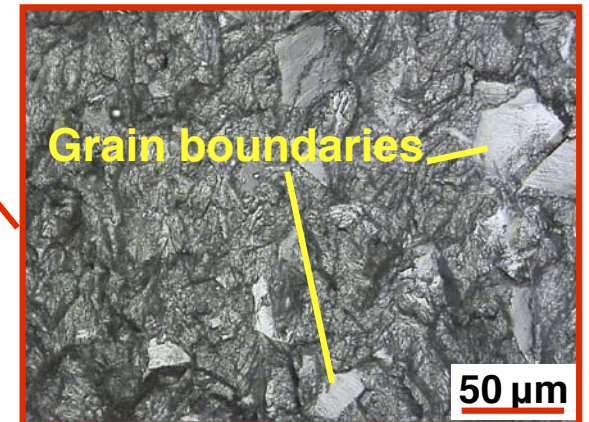
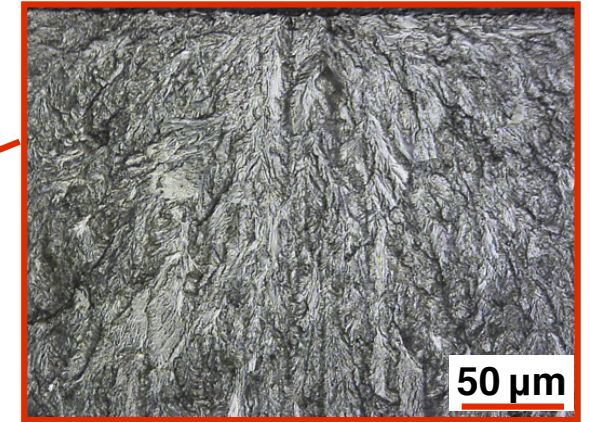
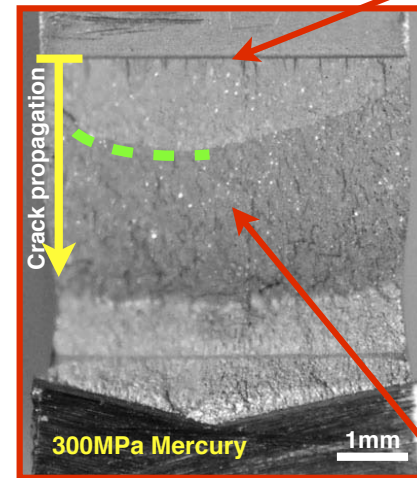


Fracture surface observation

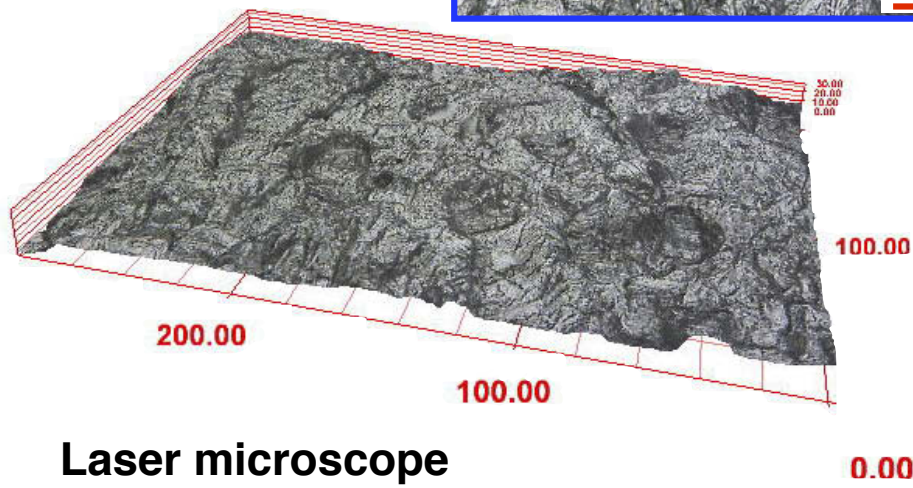
300MPa Air



300MPa Mercury



Brittle failure

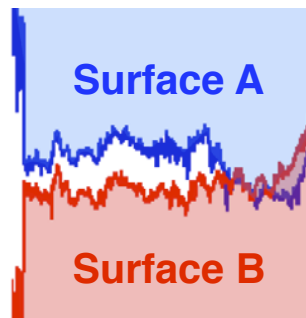


FRASTA method

FRASTA: FRActure Surface Topography Analysis

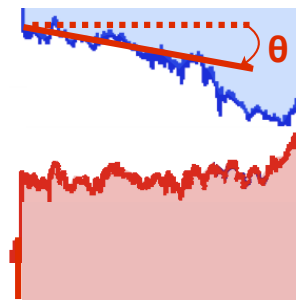
- Overlay a couple of 3D image to simulate fracture process
- Estimate the crack propagation under invisible condition

Fracture surface measurement

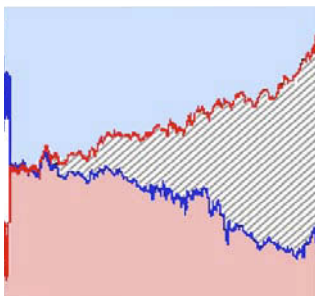


Assign slope

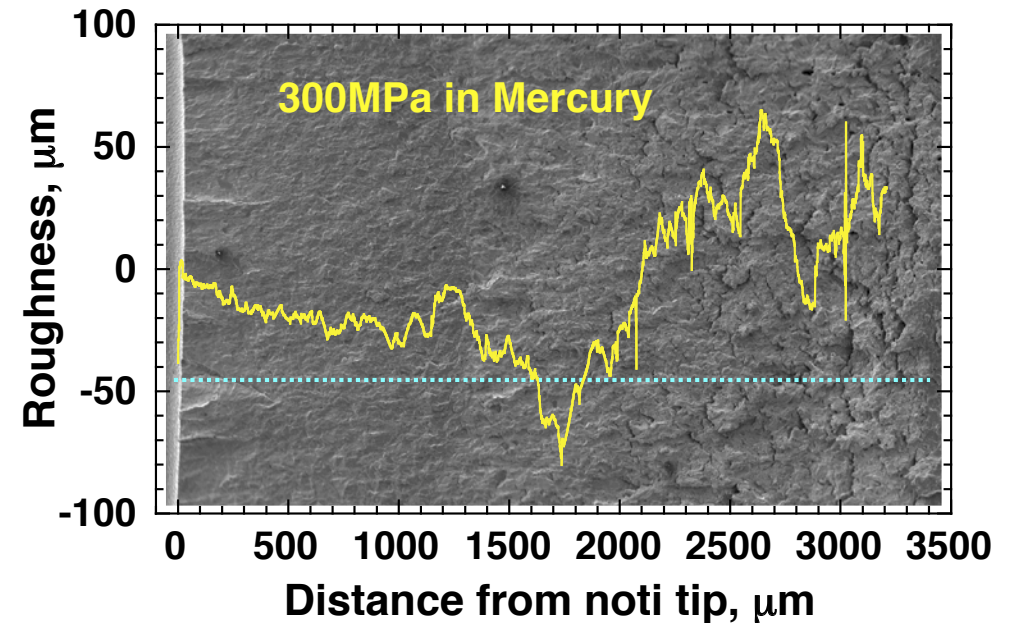
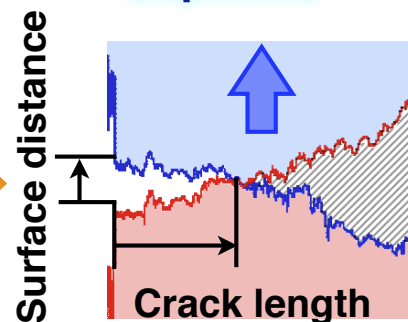
Correct elastic deformation



Overlay



Separate

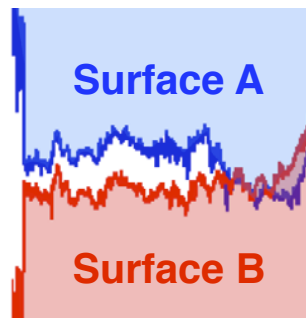


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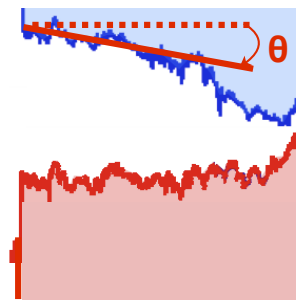
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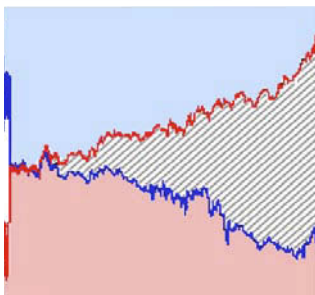


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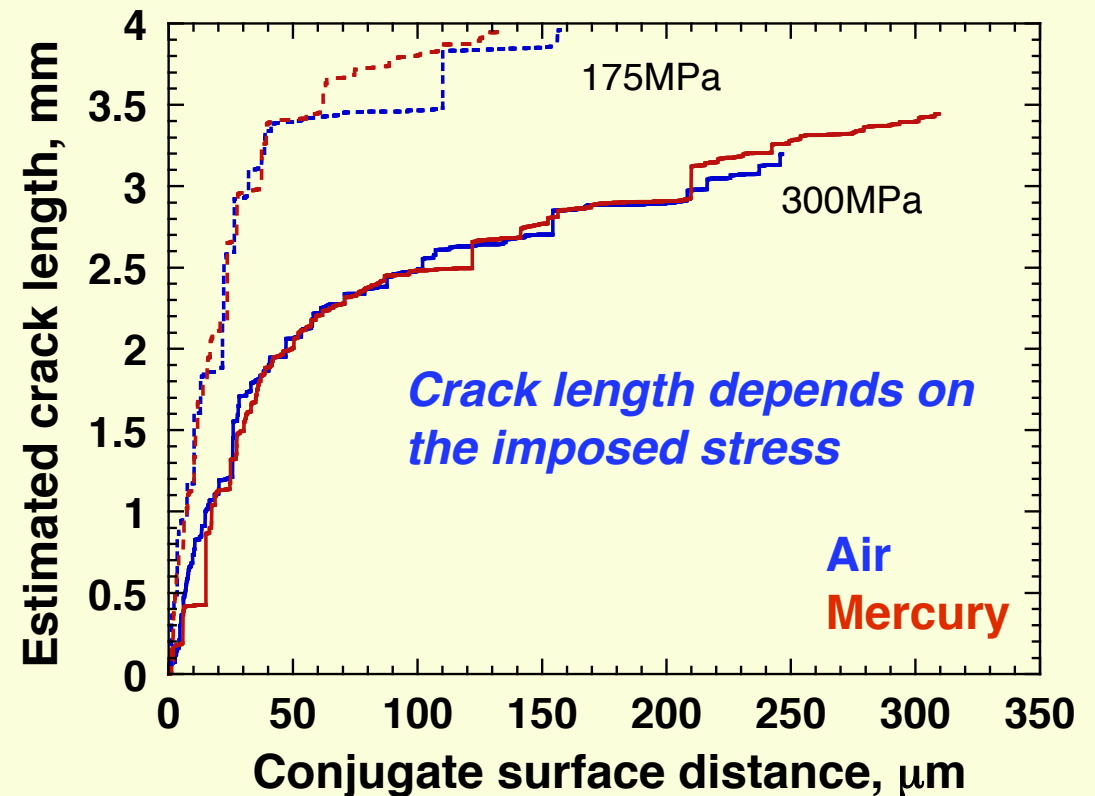
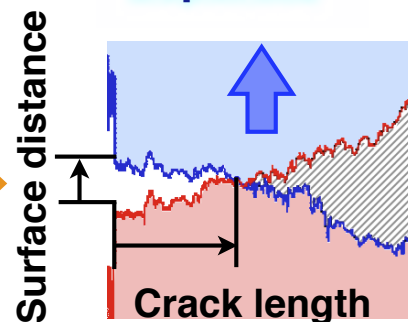
Correct elastic deformation



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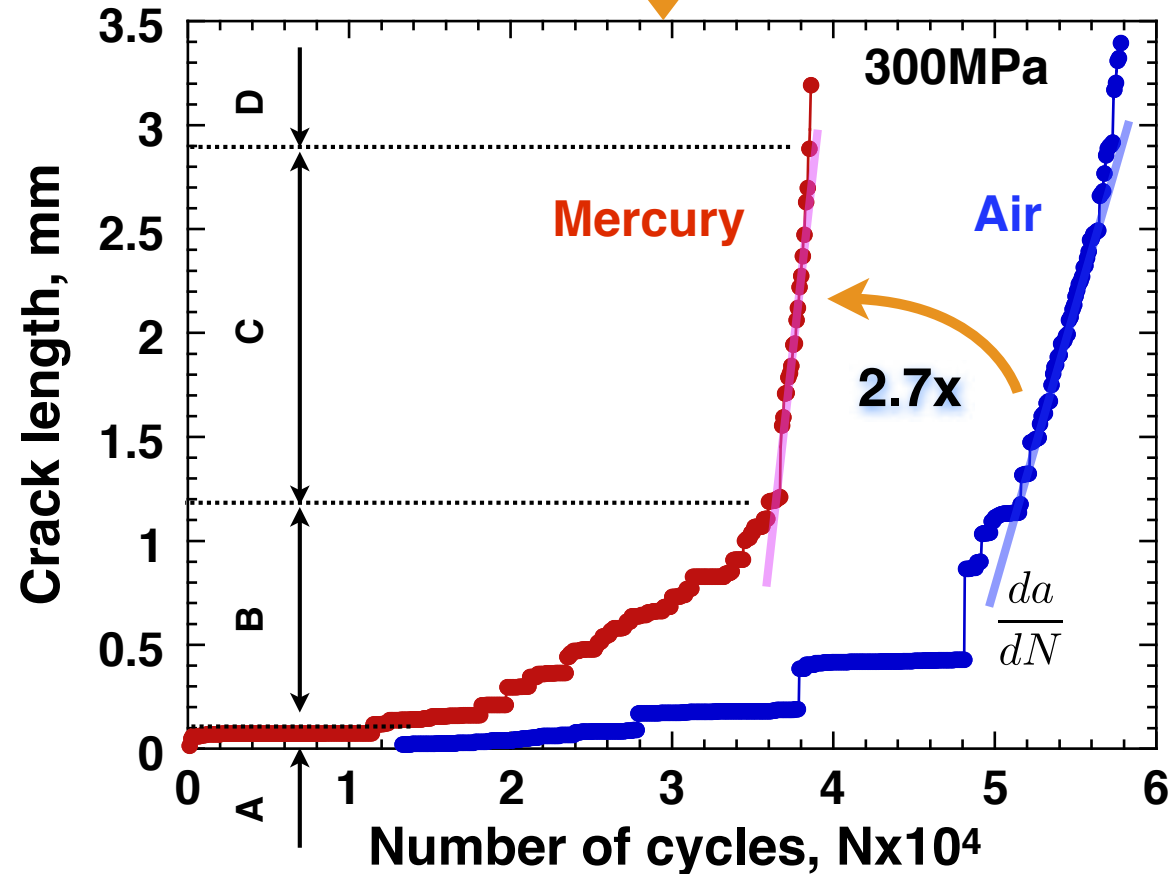
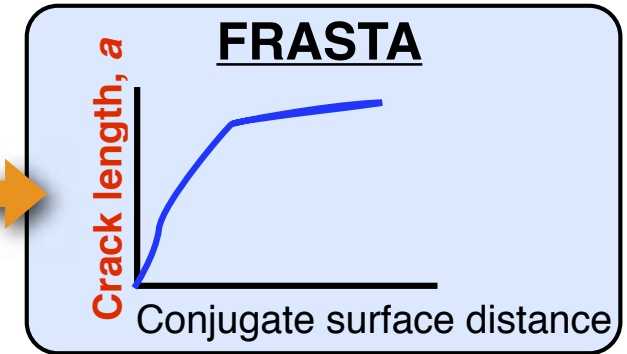
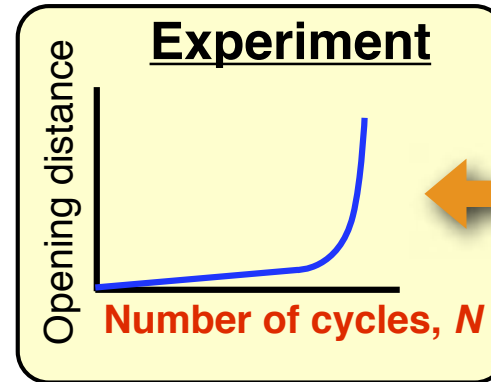
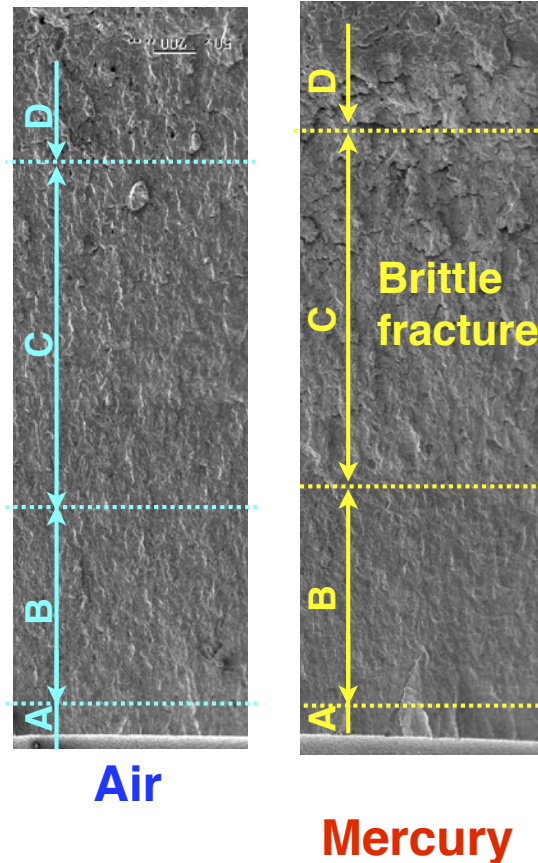
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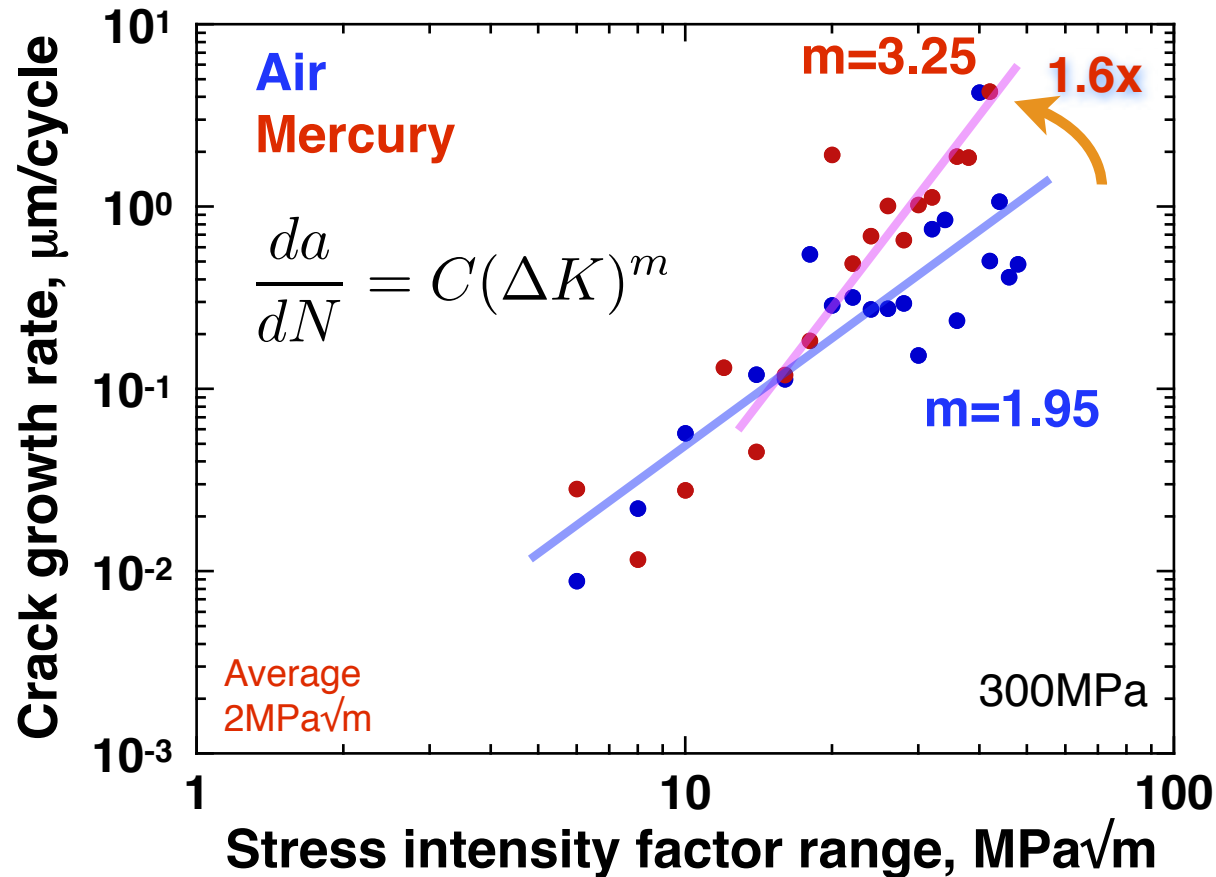
Crack propagation

Categorize 4 region

- A: Incubation*
- B: Gradually increase*
- C: Sharply increase*
- D: Final fracture*



Stress intensity factor range



Stress intensity factor range

$$\Delta K = \Delta \sigma \sqrt{\pi a} F(\xi)$$

For 3-point bending with notch

$$F(\xi) = 1.090 - 1.735\xi + 8.20\xi^2 - 14.18\xi^3 + 14.57\xi^4$$

$$\xi = a/W \quad \begin{array}{l} a: \text{crack length} \\ W: \text{width}(6\text{mm}) \end{array}$$

- Mercury effect was remarkably appeared at high- ΔK
- m value for mercury case was 1.6x larger than air case
- Crack propagation will be accelerated by mercury at high-stress imposed area and/or long crack length

Summary

Effect of mercury immersion on fatigue crack propagation was investigated through the fatigue test with notched specimen.

- **Fatigue strength was degraded by mercury immersion** at high stress imposed area.
- To investigate the crack propagation in mercury, FRActure Surface Topography Analysis with opening distance measurement was performed
- At the brittle failure region, crack propagation rate in mercury was 2.7x larger than that of in air.
- We suggested that the **fatigue crack propagation accelerates by mercury** immersion in the high-stress intensity factor range.