Two-phase flow model for energetic proton beam induced pressure waves in mercury target systems in the planned European Spallation Source

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- The idea of a thermo-hydraulical model, gentle introduction into shock-waves (ideal gas) a general thermo-hydraulics model (for water) Equation of states for Hg, proton – Hg interaction the model for ESS and some results
- Summary and Outlook

Gentle introduction on shock waves, two-phase flow

Def: a surface of discontinuity propagating in a gas at which density and velocity experience abrupt changes we call it a shock wave



Gentle introduction on shock waves, two-phase flow

the measurable physical quantities change in time non-continously, (non-continous solutions for partial differential equations)

in a real shock wave physical quantities grow up in approx. 2-4 free mean path of a particle

(10^-2 mm at normal p, T, quick phenomena no time for diffusion, heat exchange)

the given equations have differents wave solutions with different wave propagation velocities

Jacobian matrix:

$$\underline{C} = \begin{bmatrix} 0 & 1 & 0 \\ (\gamma - 3)v^2 / 2 & (3 - \gamma)v & \gamma - 1 \\ (\gamma - 1)v^3 / 2 - vh & h - (\gamma - 1)v^2 & \gamma v \end{bmatrix}$$

Diagonalized:

$$\underline{C} = \underline{L} \cdot \underline{\Lambda} \cdot \underline{L}^{-1} \qquad \begin{pmatrix} c^2 = \underline{\gamma} \underline{p} \\ \rho \end{pmatrix} \qquad h = e + p/\rho$$
Eigenvalues:

$$\underline{\Lambda} = \begin{bmatrix} v + c & 0 & 0 \\ 0 & v - c & 0 \\ 0 & 0 & v \end{bmatrix} \qquad \text{Eigenvectors} \begin{bmatrix} 1 & 1 & 1 \\ v + c & v - c & v \\ h + cv & h - cv & v^2/2 \end{bmatrix}$$
characteristic-upwind schemes 8



Gentle introduction on shock waves, two-phase flow

1D single phase flow can be generalised for 2 phases, → averaging over the volume (void fraction,)

Different models, with diferent number of equ.s

from 3 up to 7 equation models are available, with different physical backgrounds

$$\vec{\psi} = (\rho_m, v_m, p_m)$$

$$\vec{\psi} = (\rho_m, \rho_g, \rho_m v_m, \rho_m u_m)$$

$$\vec{\psi} = (\rho_g, \rho_f, \rho_m v_m, \rho_f u_f, \rho_g u_g)$$

$$\vec{\psi} = (\rho_g, \rho_f, \rho_g v_g, \rho_f v_f, \rho_g u_g, \rho_f u_f)$$
we use this one, well tested,
single pressure for both phase phases

$$\vec{\psi} = (\rho_g, \rho_f, \rho_g v_g, \rho_f v_f, \rho_g u_g, \rho_f u_f, 7^{th} \text{ variable})$$
could be a two pressure model

210

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Introduction of the WAHA model

- 1Dim surface averaged, 6 equation model
- mass, momentum, energy balance equ. for both phases $\frac{\partial \vec{\psi}}{\partial \vec{\psi}} + C \frac{\partial \vec{\psi}}{\partial \vec{\psi}} =$

$$\psi + \underline{C} \frac{\partial \vec{\psi}}{\partial x} = \vec{S}$$
 $\vec{\psi} = (p, \alpha, v_f, v_g, u_f, u_g)$

- Single pressure model
- Relap5 based Model, with different numerics, for quick processes

дt

- 6 Equ. Model Widely used in the nuclear industry
- Realistic water-steam table, correlations for both phases
- Simplified Flow Maps
- Source Code available Fortran 90 J. Comp. Phys. 136, 503 (1997)

Idea of the numerical method

Hyperbolic partial dif. equ. systems

_non-continous solutions

(jump initial condition is conserved in time) Special numerical method is needed

$$\frac{\partial \vec{\psi}}{\partial t} + \underbrace{\underline{C}}_{i} \frac{\partial \vec{\psi}}{\partial x} = \vec{S}$$

(example: ideal gas shock wave)

Pure 1st order method smears discontinuity Pure 2nd order creates unphysical oscillations Mixed method gives physicaly correct answer (flux limiters)



Flow maps, correlations

two-phase flows have very complex flow mapsthese are the main uncertanities in the theory

we use simplified flow maps

stratified, bubbly, droplet flow with different correlations

Heat-mass, energy, impulse transfer between phases

Wall friction steady state/dynamical

Interphase friction

All can be swtiched on/off for different regimes For steam induced water hammer all correlations are needed



Our former aim/experience with WAHA

study of the steam condensation induced water hammer phenomena,

the most complex two-phase flow phenomena

(experimental setup and the model scheme in numerical simulation)





Tube volume 12 litre

The physical mechanism for steam condensation induced water hammer (some figures, poore man's animation)



Analysis of the pressure peaks

(all the correlations and all know-hows are needed)

I.F. Barna et al. Nucl. Eng. and Des. 240, 146, (2010)



Idea, use the modified 6equ. model for proton – Hg interaction

- Basicaly two new points
- Not water but mercury (new & complete liquid- steam table), equation of state (EOS) (Subbotin correlation, surface tension, heat conduction, viscosity is known)
- Periodic driving from absorbed proton pulses, a new source term in both energy equations

How to create a steam table for Hg

For standard 2 phase-flow calculation a 6-fold table is needed: T T (K), ρ (Pa), ρ _vap (kg/m^3), u_vap (J/kg), ρ _liq (kg/m^3), u_liq (J/kg)



Our Van-der Waals fit for vapour-liquid coexistence and vapour pressure

N. B. Vargaftik, Y. K. Vinogradov, and V. S. Yargin, Handbook of Physical Properties of Liquid and Gases, 3rd ed. Begell House, New York, 1996.

Proton beam–Hg target interaction



The new source terms

 We consider proton beam-Hg interaction as a periodic sudden heat shock in the energy equation of the liquid and gas phase

$$\frac{\partial \vec{\psi}}{\partial t} + \underbrace{\underline{C}}_{=} \frac{\partial \vec{\psi}}{\partial x} = \vec{S}$$

$$\frac{\partial A(l-\alpha)\rho_{f}u_{f}}{\partial t} + \frac{\partial A(l-\alpha)\rho_{f}u_{f}v_{f}}{\partial x} - p\frac{\partial A\alpha}{\partial t} + p\frac{\partial A(l-\alpha)v_{f}}{\partial x} = A\left(Q_{if} - \Gamma_{g}h_{f}^{*} + v_{f}F_{f,wall}\right) + E_{f,pulse}(x,t)$$

$$\frac{\partial A\alpha}{\partial t}\rho_{g}u_{g}}{\partial t} + \frac{\partial A\alpha}{\partial x}\rho_{g}u_{g}v_{g}}{\partial x} + p\frac{\partial A\alpha}{\partial t} + p\frac{\partial A\alpha}{\partial x}v_{g}}{\partial x} = A\left(Q_{ig} + \Gamma_{g}h_{g}^{*} + v_{g}F_{g,wall}\right) + E_{g,pulse}(x,t)$$

$$E_{g,pulse}(x,t) = \frac{\rho_g \alpha}{\rho_m} E_0 \sin^2 \left[\frac{\Pi t}{\tau}\right] (1 - (x/x_s)^2)$$
$$E_{f,pulse}(x,t) = \frac{\rho_f (1 - \alpha)}{\rho_m} E_0 \sin^2 \left[\frac{\Pi t}{\tau}\right] (1 - (x/x_s)^2)$$

continuity, momentum equations will not be changed

The ESS-SNS-JSNS Hg Target Concepts





ESS (5 MW), SNS (2 MW) and JSNS (1 MW) use liquid mercury targets enclosed in steel shells, albeit with different internal flow distributions.



The scematic scheme of the target

No sophisticated 3D model, like Fluent, Ansys of CFX NO ENGINEERING But better phylscs for boiling-condensation, 2 phase flow



Our results till now



Total Length = 18 m Tube diameter = 15 cm $V_Hg = 4$ m/s $P_0 = 4.5$ bar $T_0 = 385$ K $T_max = 475$ K $P_max = 280$ bar

Only a single pulse is taken at t = 0 sec which is 2 ms long

E = 300 KJ/puls ESS Energy

If Hg begins to cavitate, calculation Breaks down, EOS must be more Accurate

Summary and Outlook

We gave a short/gentle introduction into shock waves/2phase flow ©

introduced the WAHA3 model, which is feasible to describe shock waves, quick transients in two phase-flows

presented a model which is **hopefully** a good choice to understand some new physics in proton-Hg system

further work is in progress to clear out the dark points and present reasonable results

I.F. Barna et al. Eur. Phys. J. B. 66 (2008) 419 Or: <u>arXiv:0805.3618v1</u> [cond-mat.other]

There are liquid-metal (eq. Li) or liquid helium cooled systems as well... (work for the next 20-30 years)



Questions, comments, remarks?...