

**10th International Workshop on
Spallation Materials Technology**
Oct.18-22, 2010, Beijing, China

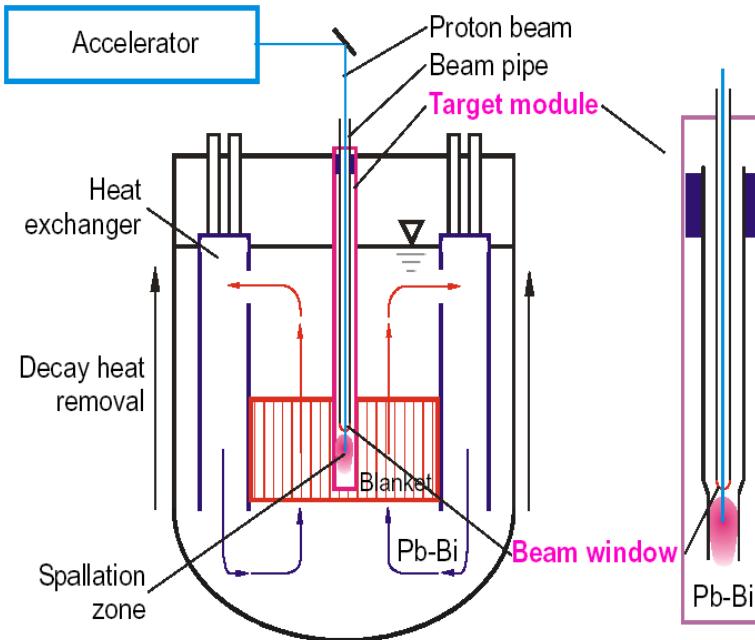
**Embrittlement Effects of LBE
on Ferritic/Martensitic Steels
After Irradiation in SINQ Targets**

B. Long^{1,2}, W.Gao², Y.Dai²

- 1. China Institute of Atomic Energy, Beijing 102413, China***
- 2. Paul Scherrer Institute, 5232 Villigen PSI, Switzerland***

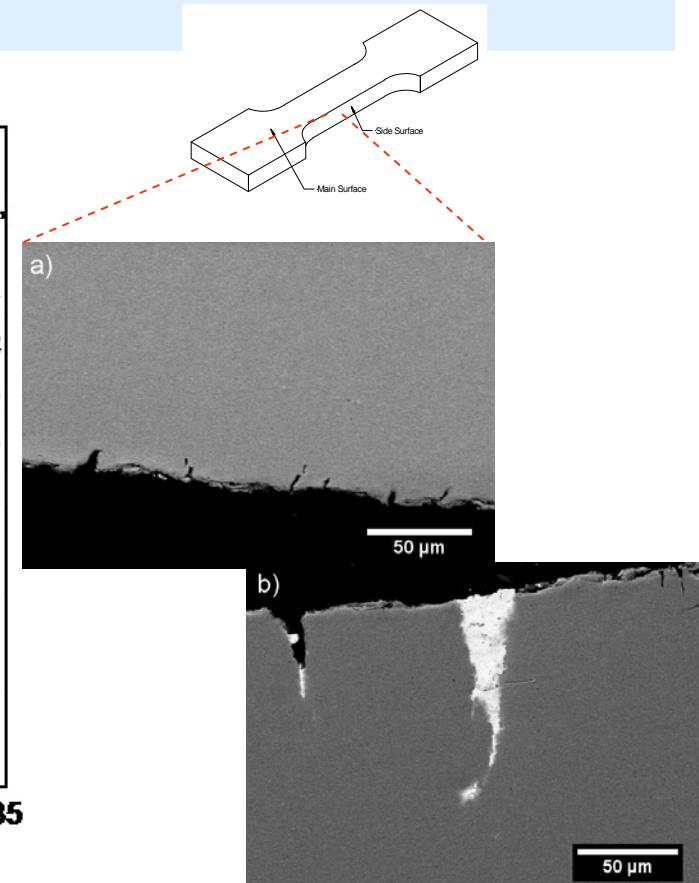
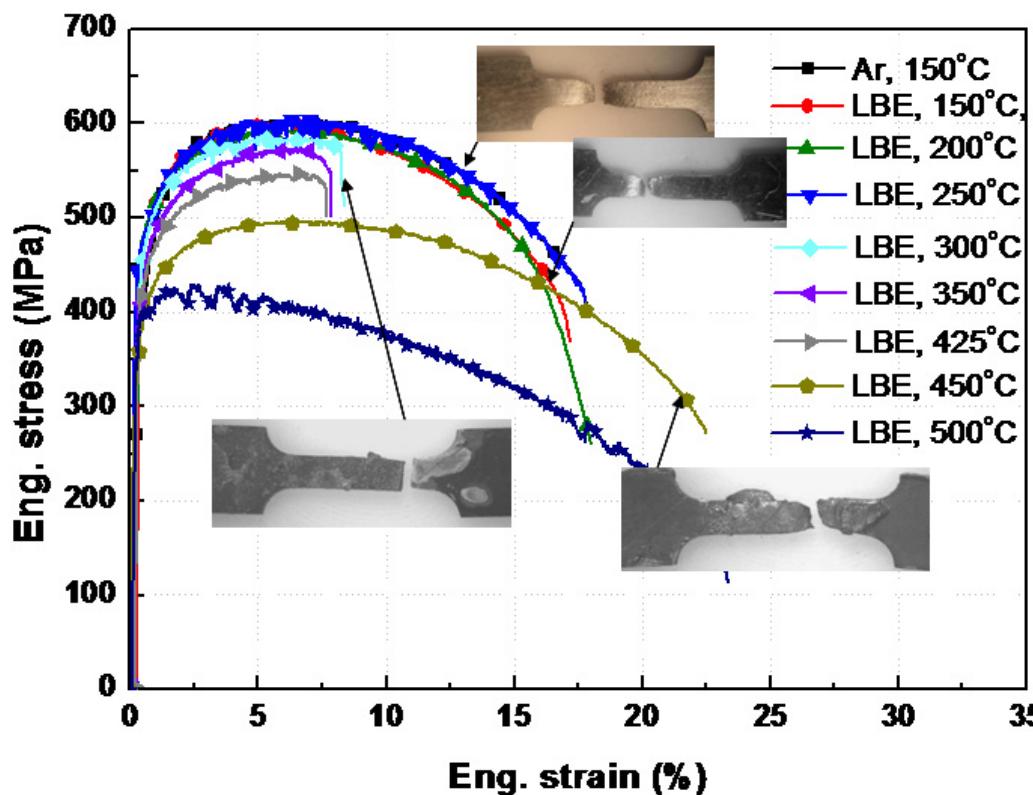
Introduction

- LBE (lead-bismuth eutectic) is selected as target and coolant material for the targets of the spallation sources and the accelerator driven system (ADS) -for example MEGAPIE;
- The T91 FM (ferritic/martensitic) steel is the main candidate structural material



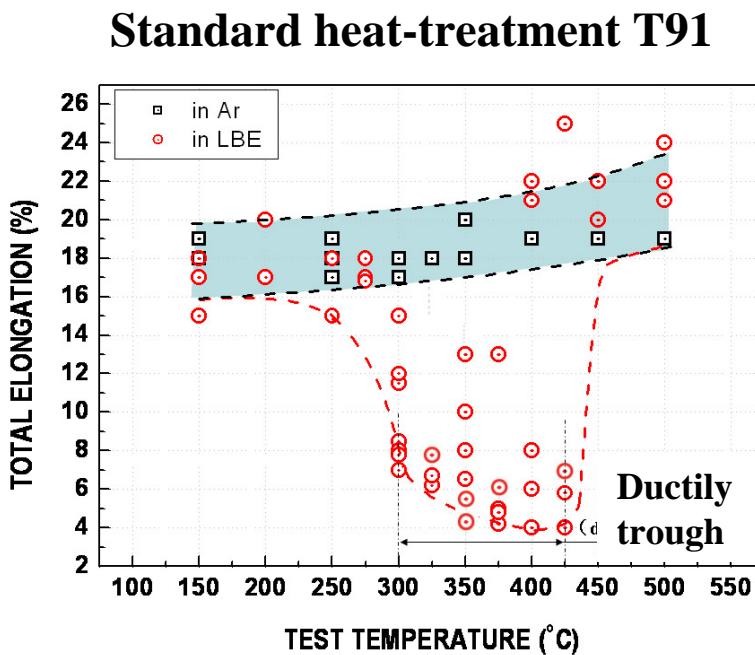
Introduction

- Our previous studies demonstrated that
 - a) The steel could sensitive to the LBE embrittlement effects when there were cracks or flows on the surfaces of specimens;

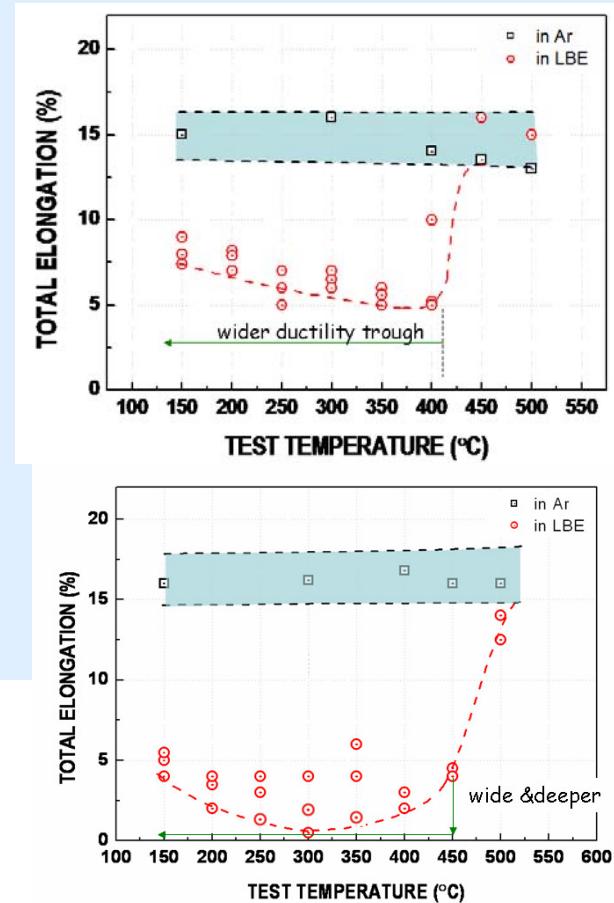


Introduction

- Our previous studies demonstrated that
- b) The LBE embrittlement effects can be strongly enhanced by the hardening of the steels



B. Long, Y. Dai, J. Nucl. Mater., 376 (2008) 341-345



Materials

Heat treatment: to simulate radiation hardening

- ➡ HT760 (T91): normalized at 1040°C for 1h, tempered at 760°C for 2h
Microhardness HV0.05 = 220 :standard metallurgical state
- ➡ HT600 (T91): normalized at 1040°C for 1h, tempered at 600°C for 2h
Microhardness HV0.05 = 350
- ➡ HT500 (T91): normalized at 1040°C for 1h, tempered at 500°C for 2h
Microhardness HV0.05 = 450

Material	Cr	Ni	Mn	Mo	Ti	V	Si	P	Nb	W	Ta	C
T91 ¹	8.76	0.10	0.60	0.86	-	0.19	0.32	0.019	0.07	---	----	0.09
F82H	7.65	0.02	0.10	0.003	0.004	0.19	0.07	0.003	0.002	1.98	0.03	0.09

1. Heat-A387, from INDUSTEEL for MEGAPIE project

Materials and specimens

Specimen for irradiation



specimens



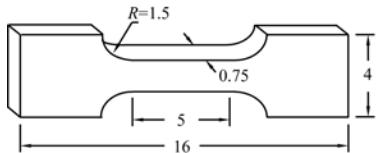
For tensile test



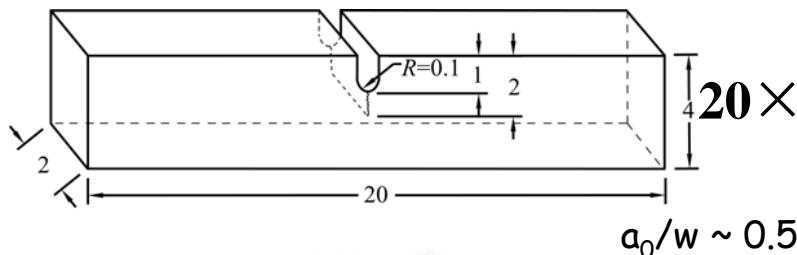
For 3-p bending test



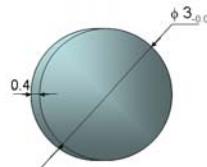
For TEM and small punch



$16 \times 4 \times 0.75 \text{ mm}$ with a gauge section of $5 \times 1.5 \times 0.75 \text{ mm}$

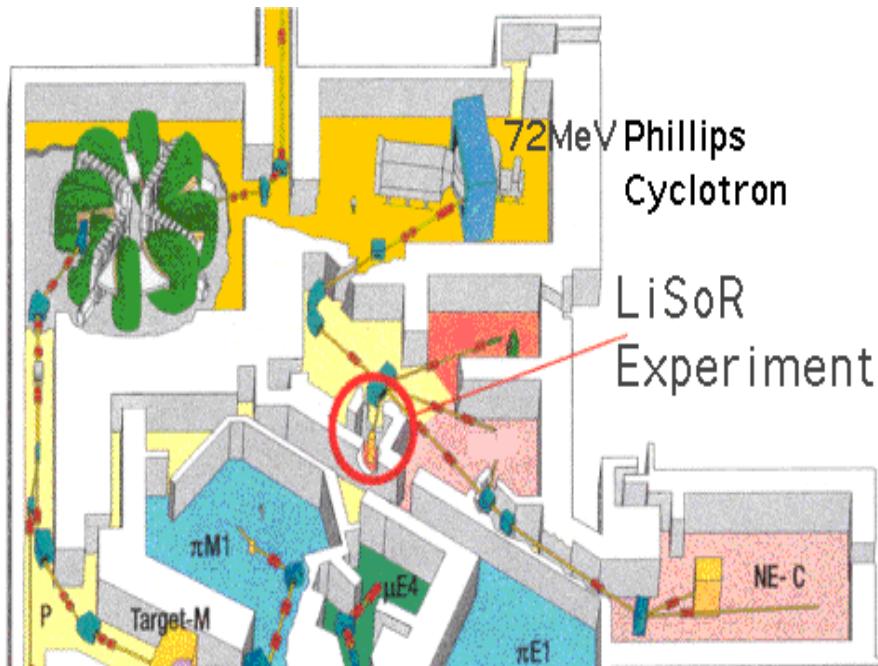


$20 \times 4 \times 2 \text{ mm}$ and with a notch of 1 mm in depth

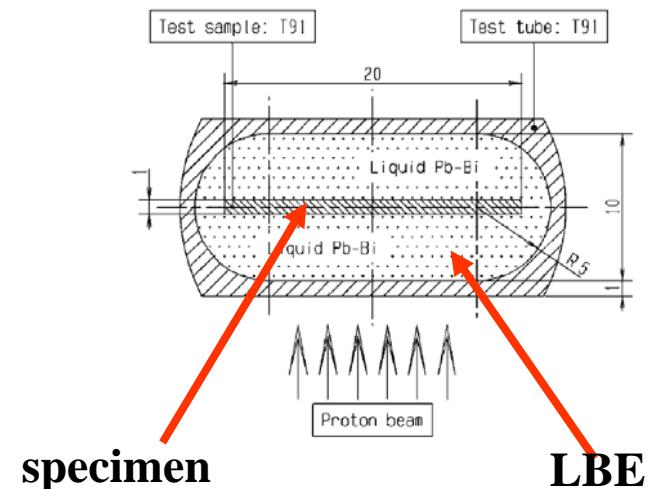


disc with $\phi 3$ and 0.4mm thickness

LiSoR loop



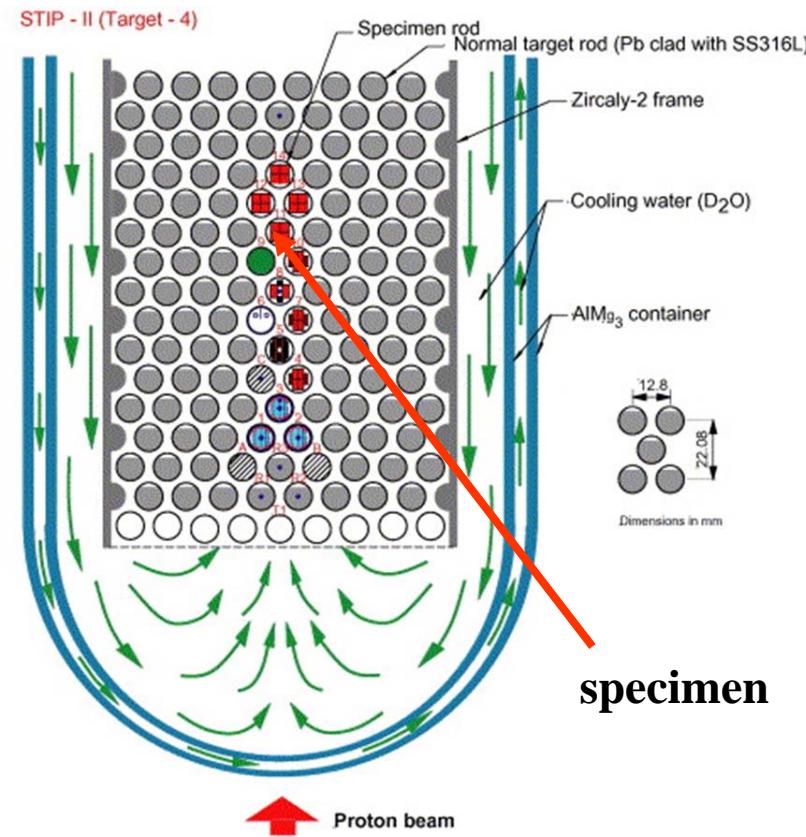
from PSI website



Irradiation parameters:

- Beam energy: 72 MeV
- Inlet LBE temperature: 300°C
- Irradiation temperature: 325 – 525 °C
- Irradiation dose: max. 0.48 dpa (displacement per atom)
- Oxygen concentration in LBE: saturated

Irradiations at SINQ (STIPs)

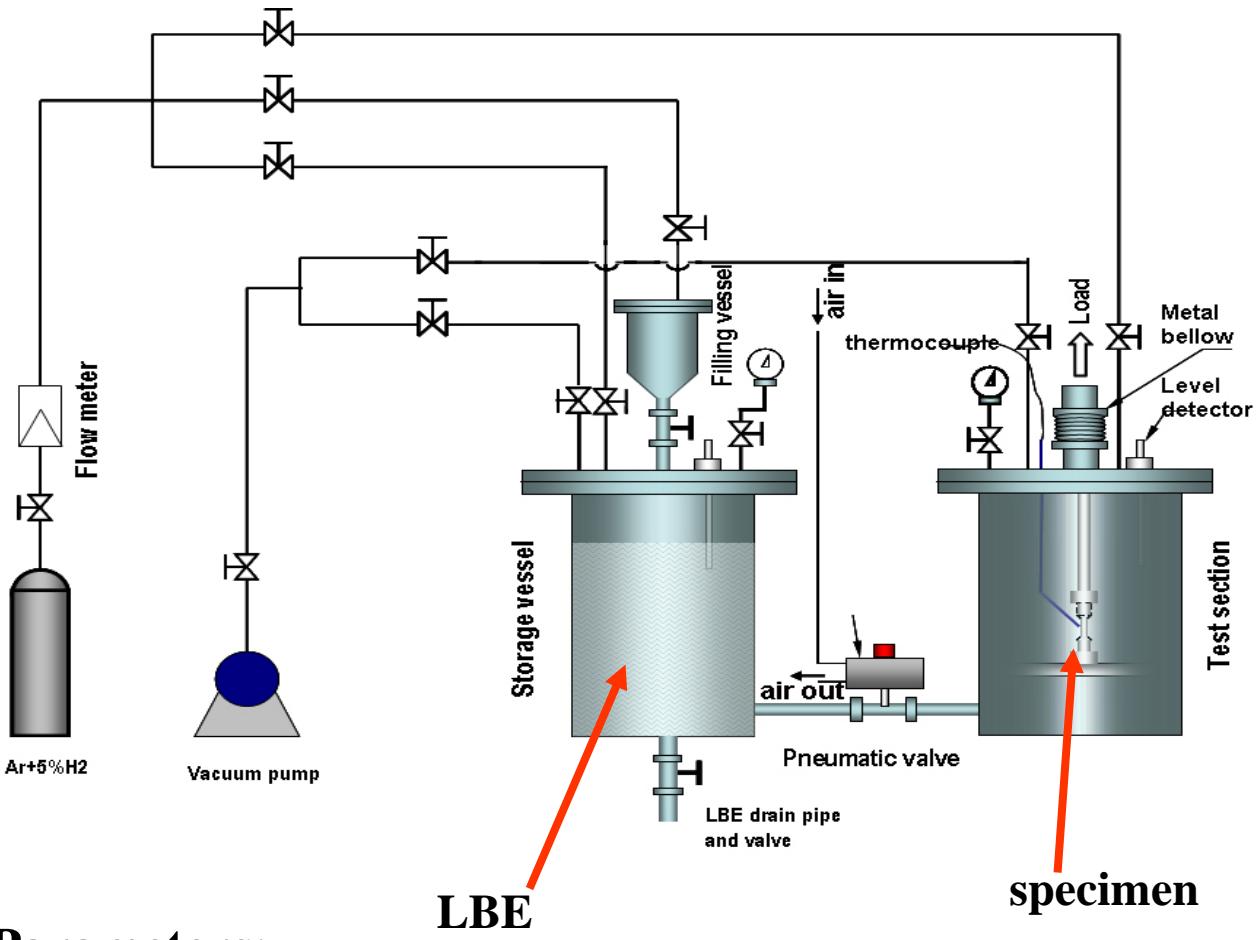


STIP program is aiming at studying radiation damage in structural materials under a mixed spectrum of high-energy protons plus spallation neutrons.

Irradiation parameters:

- beam energy: ~ 570MeV
- irradiation temperature: 100 – 500 °C
- irradiation dose: max. 20 dpa
- He concentration: max. 1790 appm

LME test facility

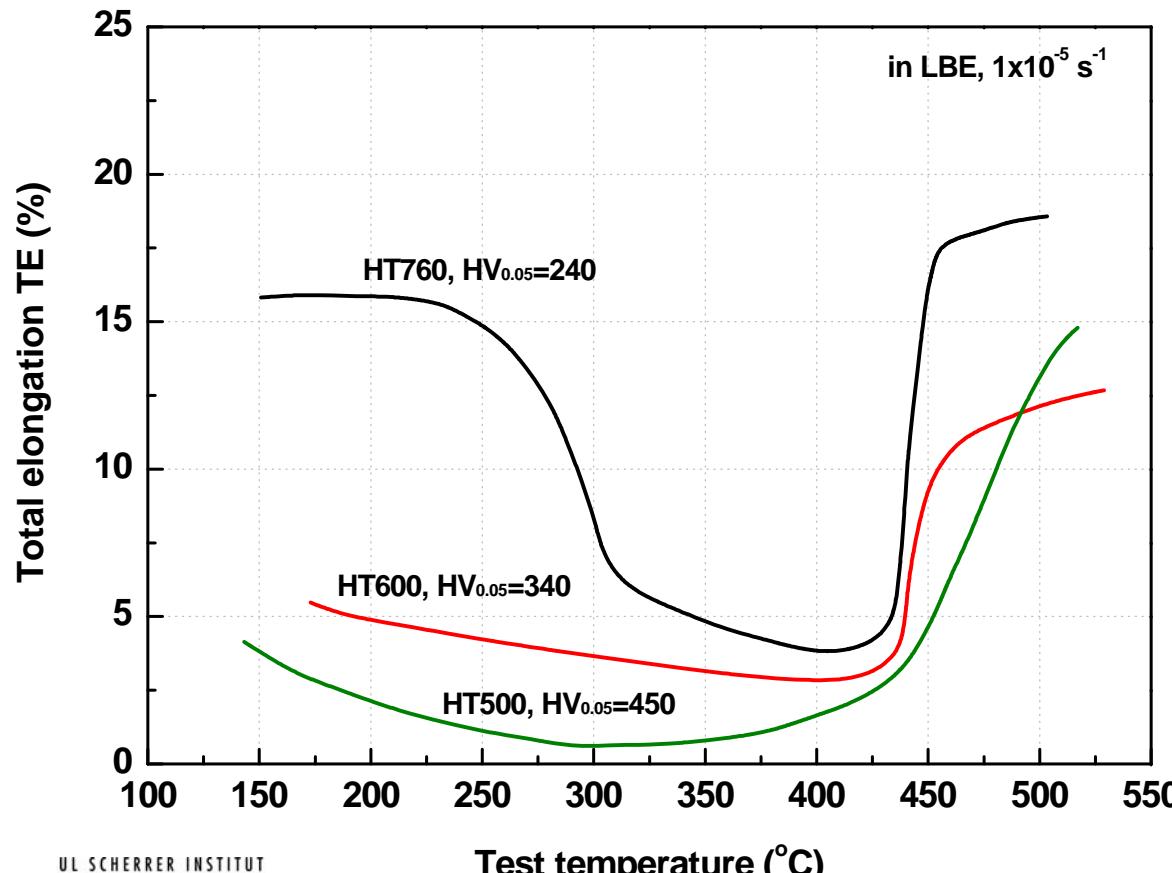


Parameters:

- test temperature: **150 to 500 °C**
- oxygen concentration in LBE: **1×10^{-6} wt.%**

Comparison of SSRT tests results on HT760, HT600 and HT500

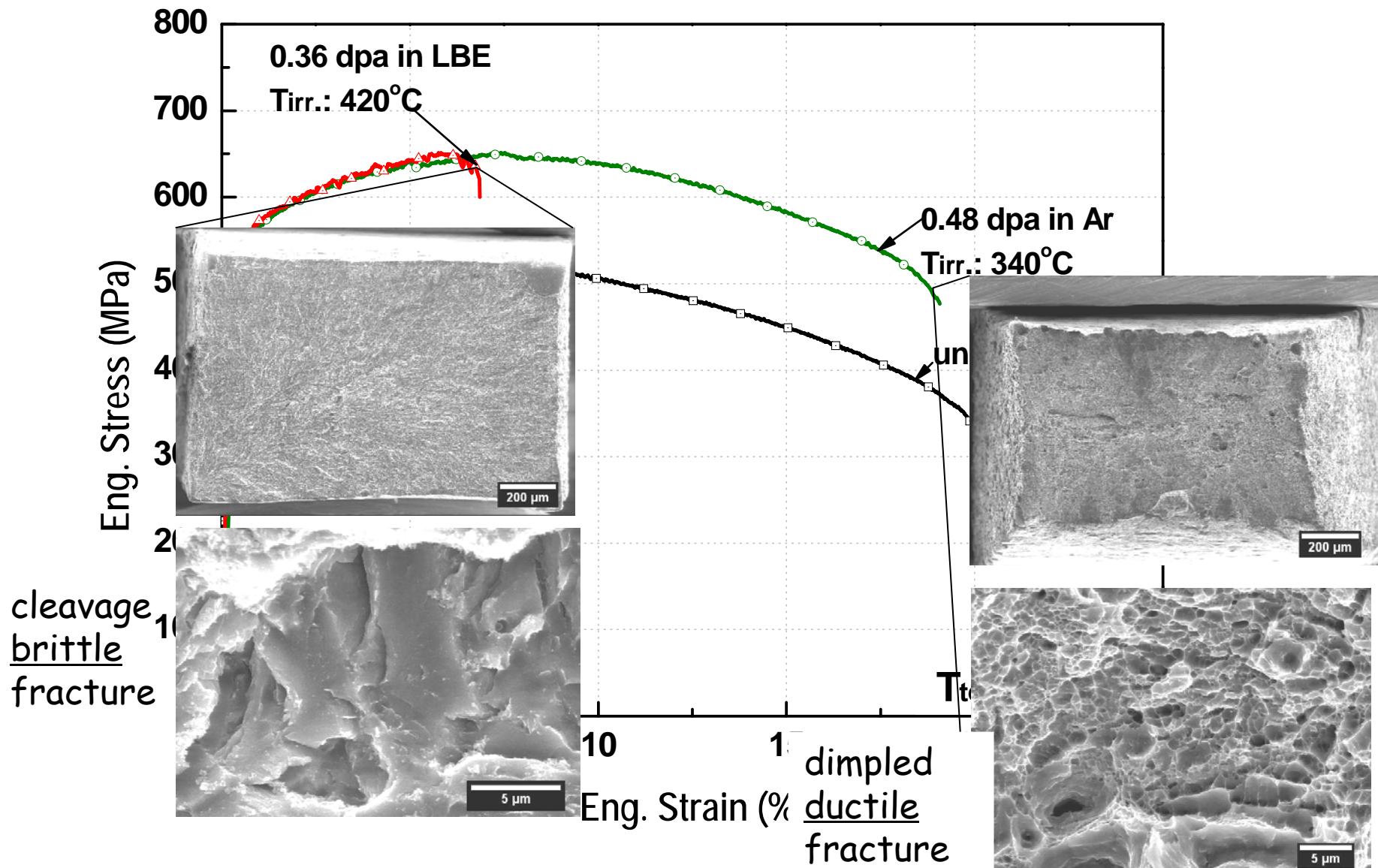
- ▲ The “ductility trough” of HT760 is 300-425°C
- ▲ The “ductility troughs” of HT600 and HT500 cover a wider temperature range
- ▲ LBE embrittlement effects on tensile properties of FM steels can be strongly enhanced by the hardening of the steels (**high strength → high risk to LME**)



SSRT on irradiated T91

(LiSoR-3 and -4)

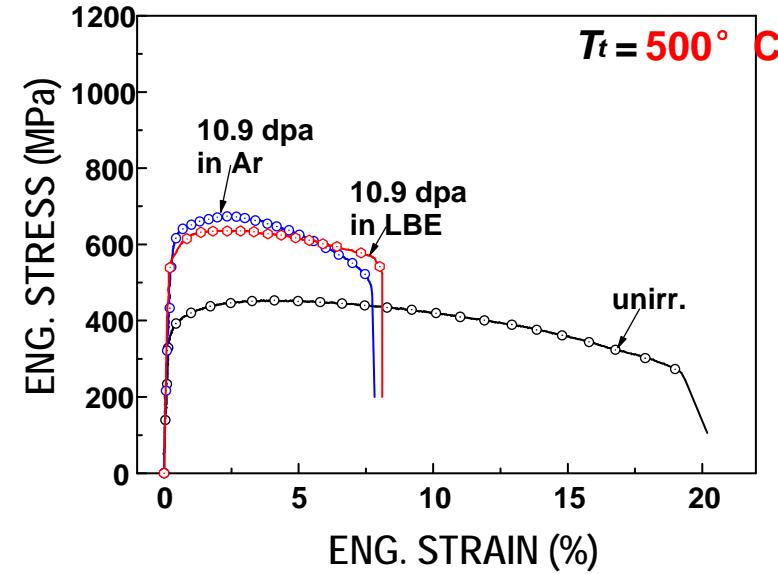
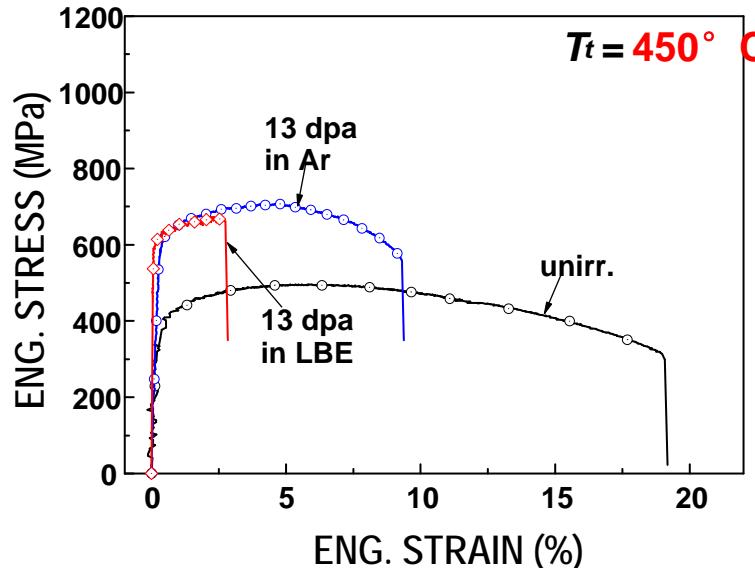
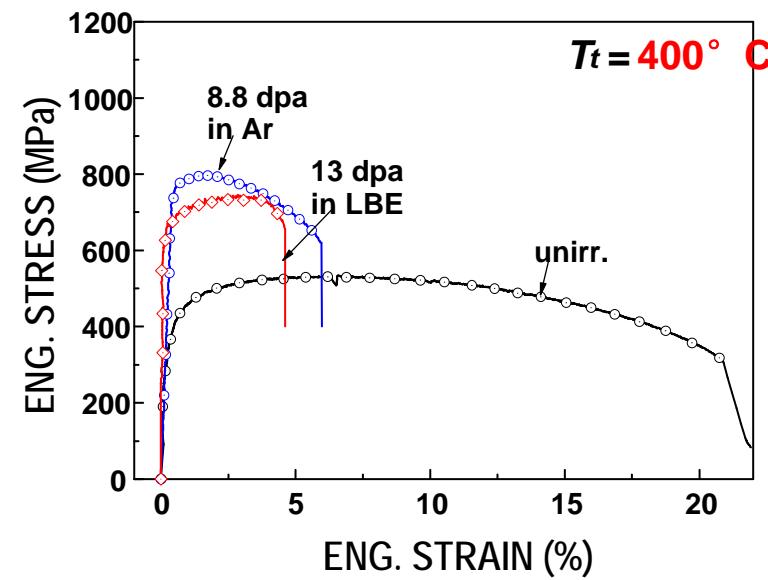
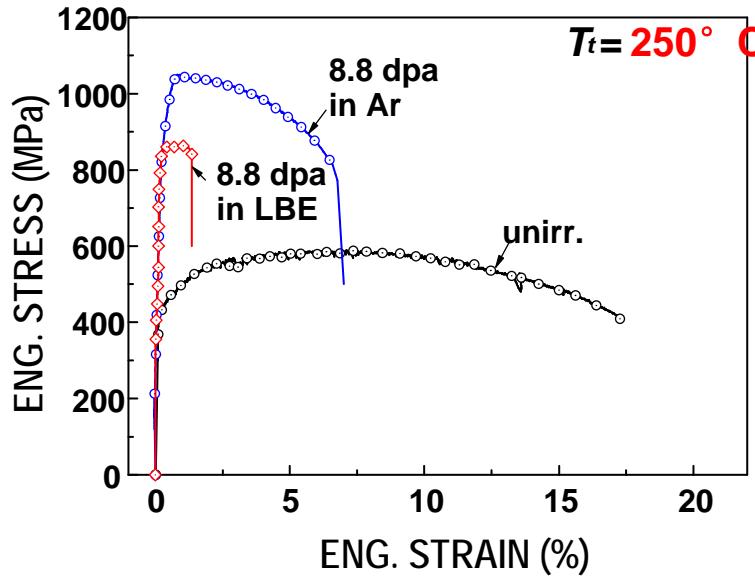
▲ In Ar: irradiation-induced hardening; In LBE: LBE-induced embrittlement



Irradiated T91

(STIP-3)

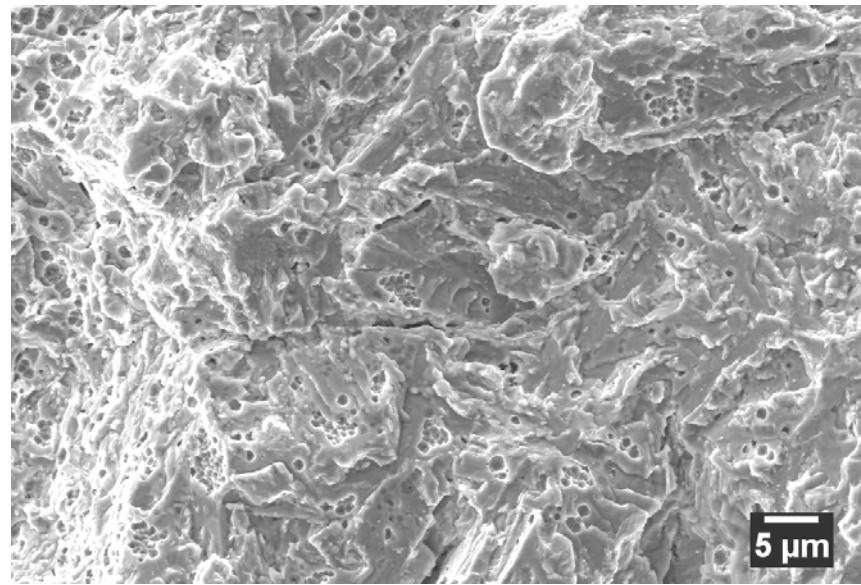
▲ LBE-induced embrittlement occurs in the temperature range of 250-450°C



Irradiated T91

(STIP-3)

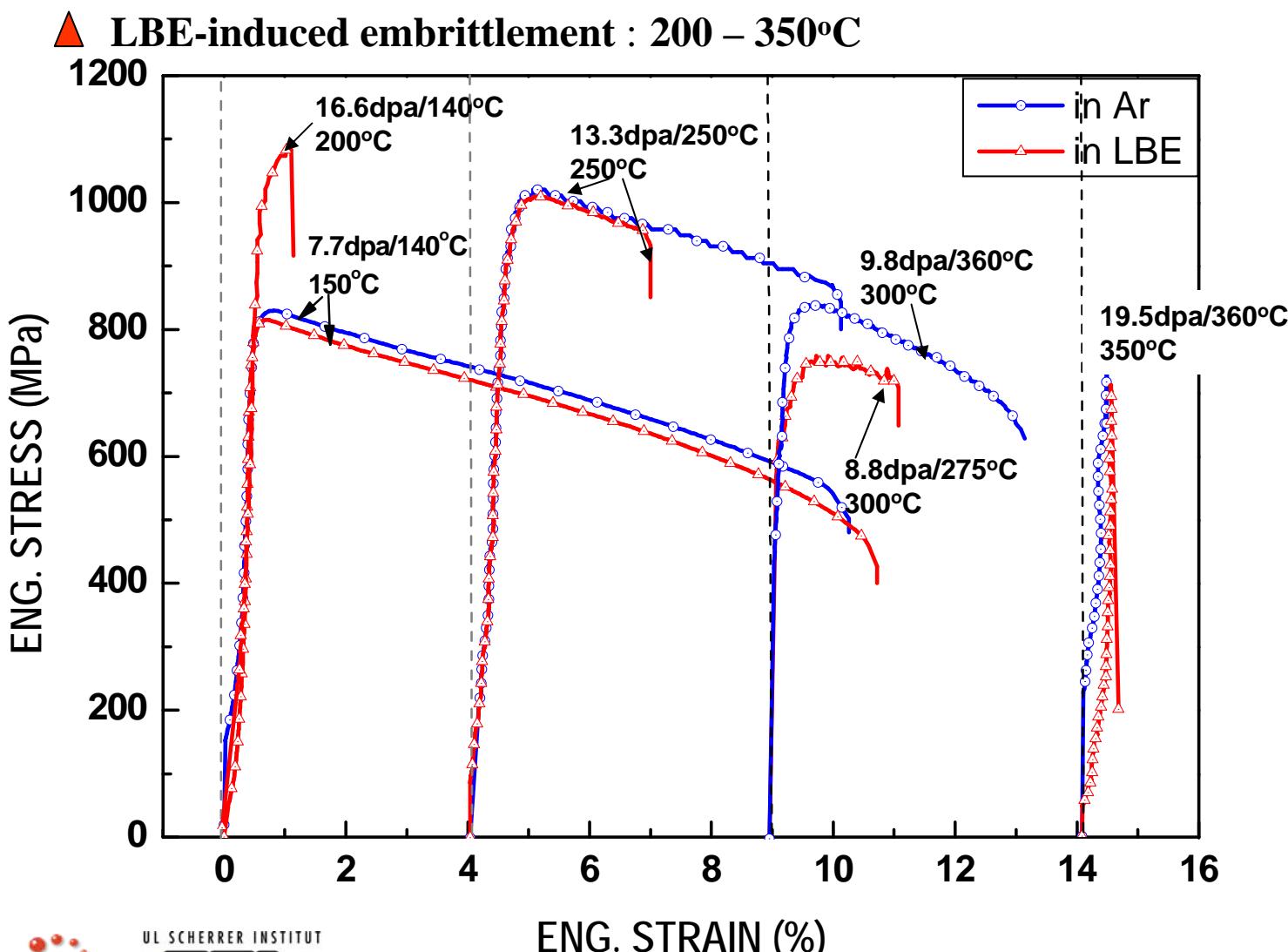
13.0 dpa/451°C in LBE at 450°C



cleavage brittle fracture

SSRT on irradiated F82H

(STIP-2 and -3)

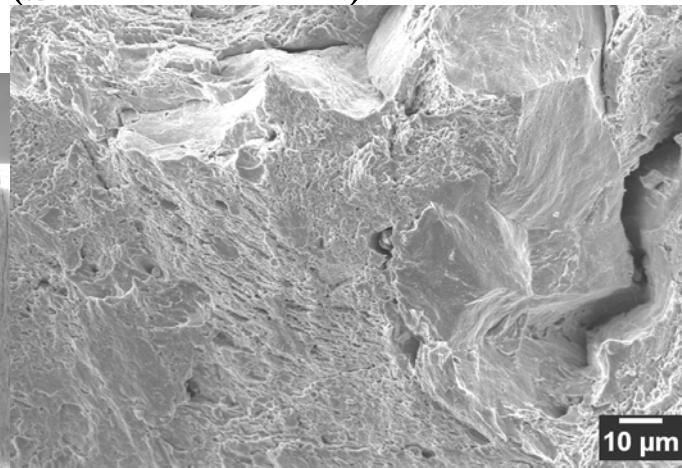
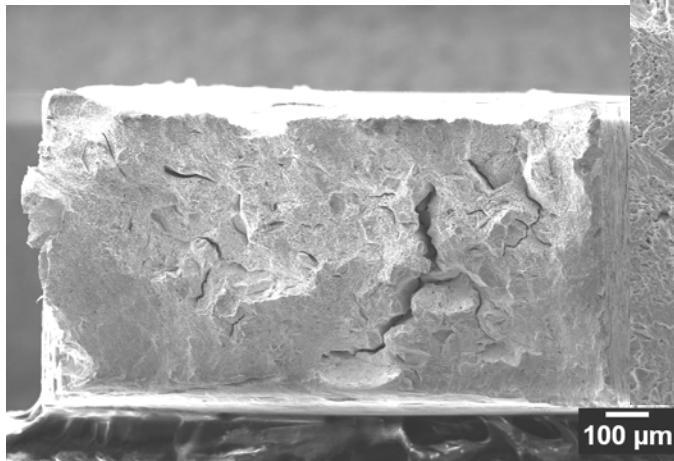


Irradiated F82H

(STIP-2 and -3)

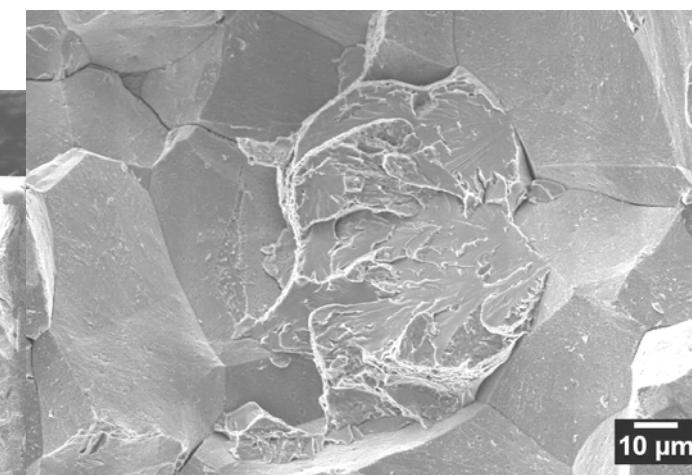
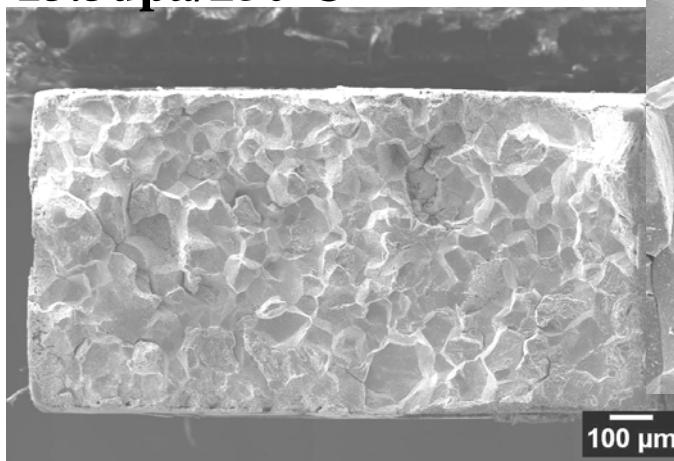
in Ar at 250°C

13.3dpa/250°C



mixed
ductile &
brittle
fracture

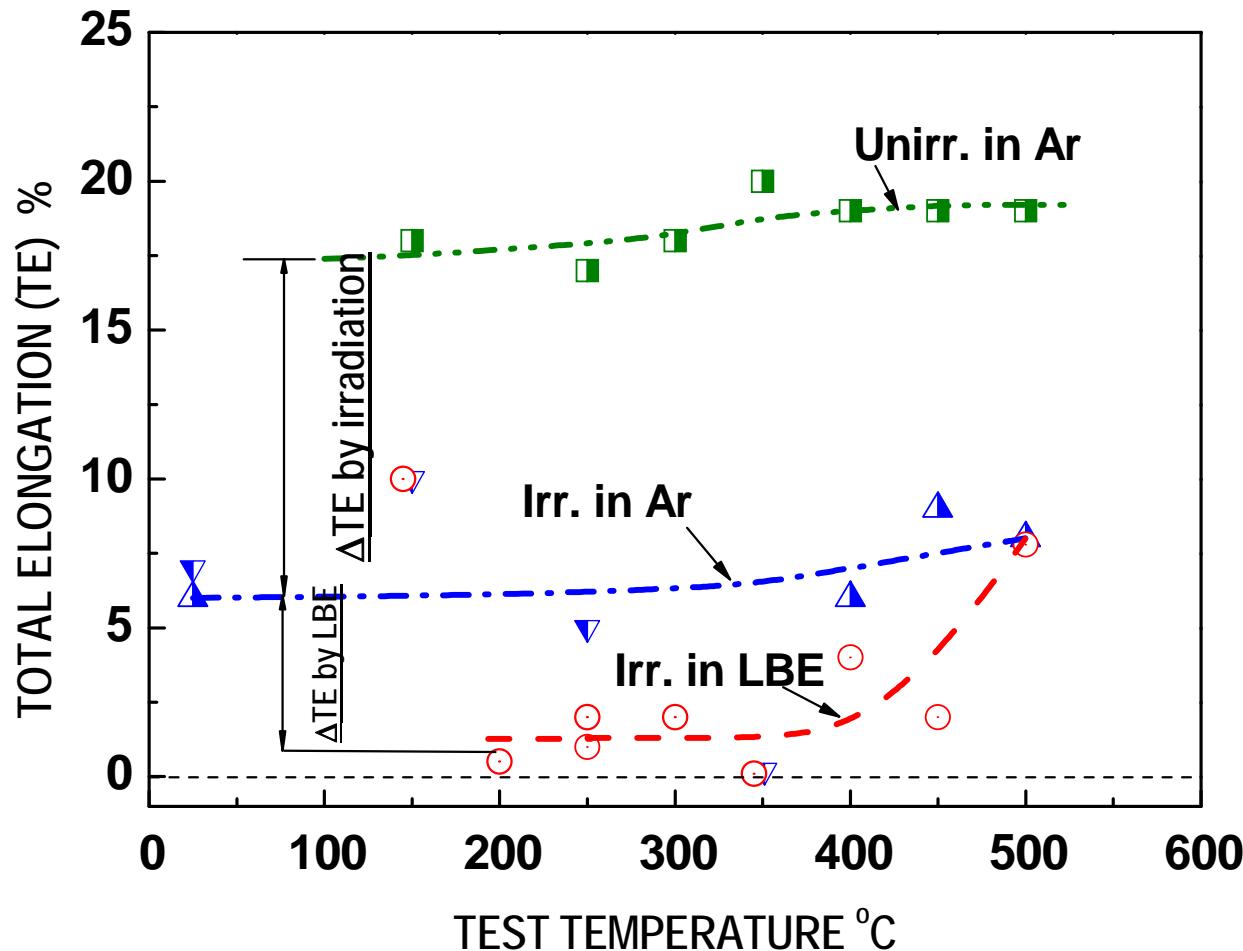
13.3dpa/250°C



cleavage &
intergranular
brittle
fracture

Comparison of SSRT tests results on irradiated specimens

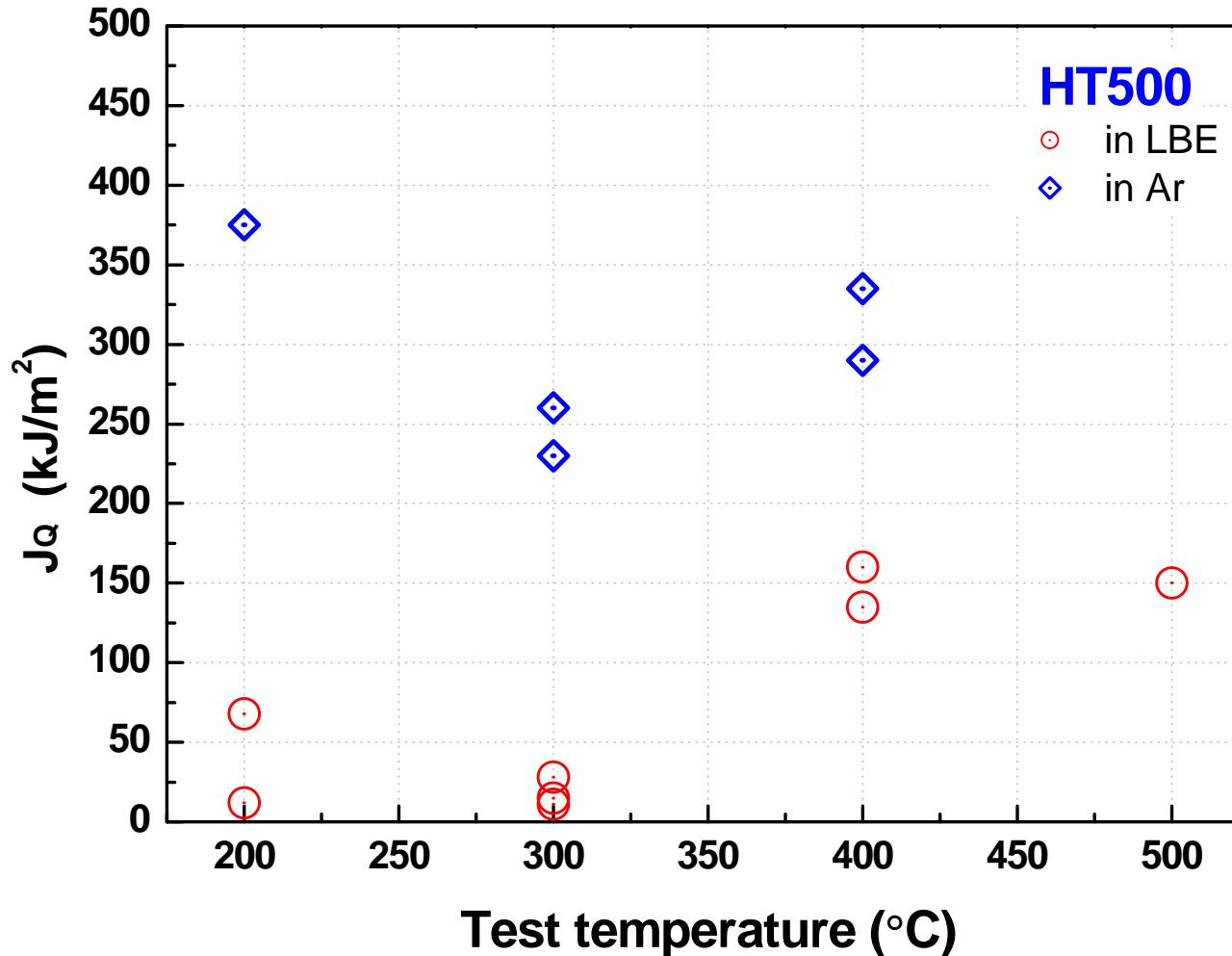
- ▲ Irradiated specimens suffer a drastic loss of ductility due to irradiation-induced embrittlement effect
- ▲ Most irradiated specimens tested in LBE undergo a further reduction in ductility



3P bending tests on HT500

(tempering at 500°C)

- ▲ Fracture toughness is strongly reduced in LBE environment:
only about 12 kJ/m² at T = 300°C

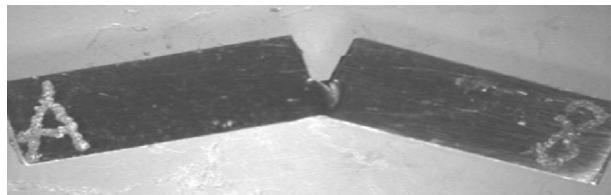


HT500

(tempering at 500°C)

in Ar

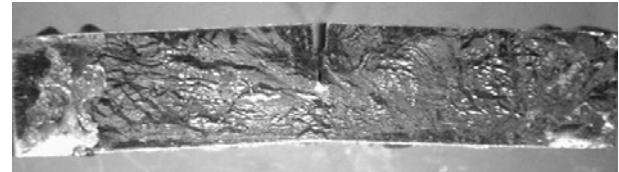
300° C



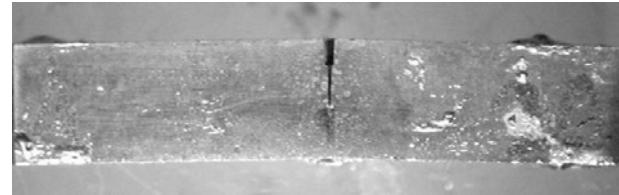
a large bending deformation

in LBE

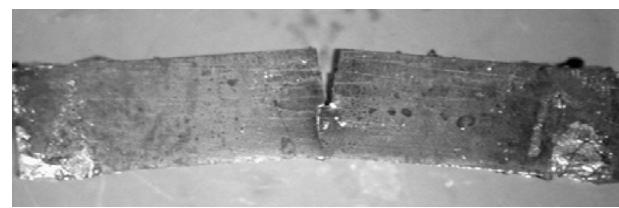
200° C



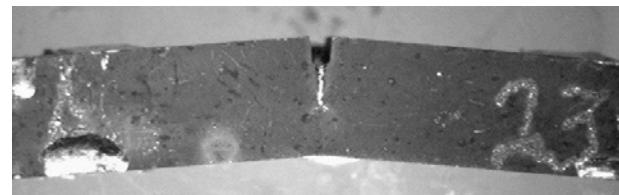
300° C



400° C



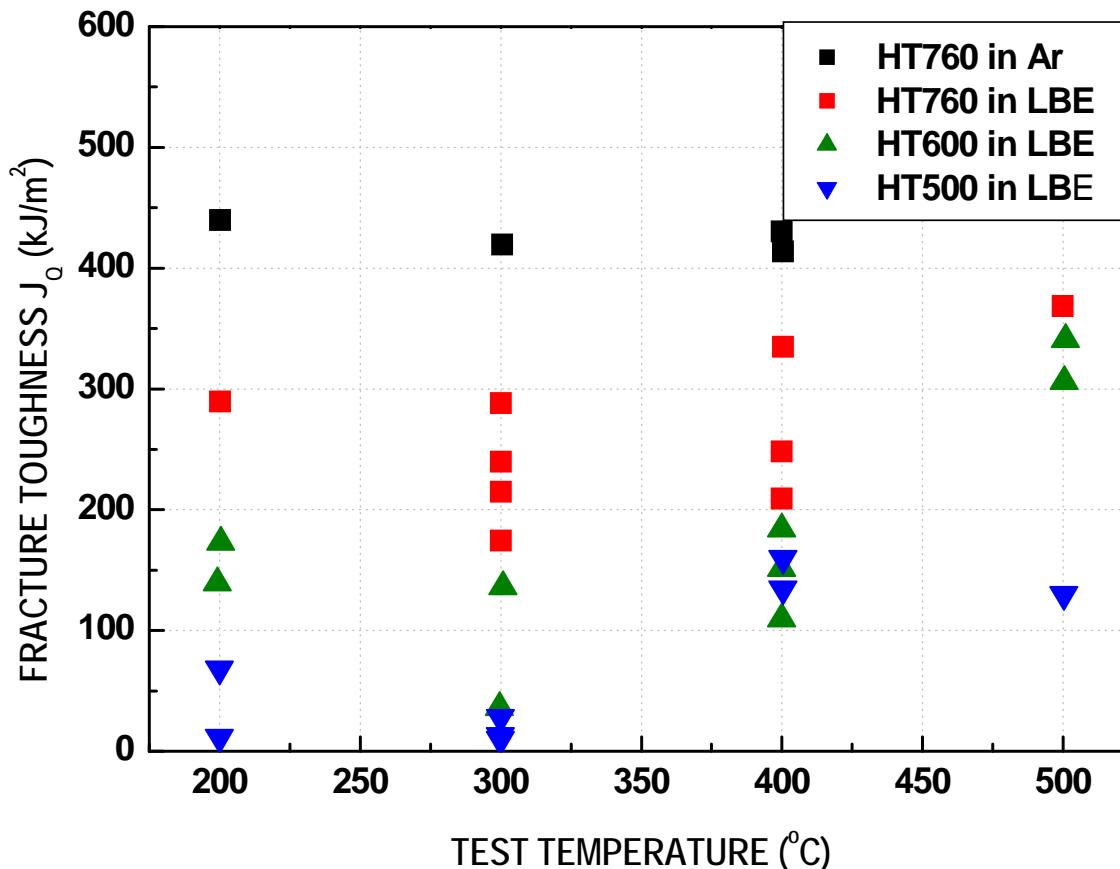
500° C



a slight bending deformation

Comparison of 3-p bending tests results on HT760, HT600 and HT500

- ▲ HT760: fracture toughness is reduced in LBE as compared to Ar
- ▲ HT600 and HT500: fracture toughness is further reduced in LBE
- ▲ LBE embrittlement effects on fracture toughness of FM steels can be strongly enhanced by the hardening of the steels (**higher strength → higher risk to LME**)

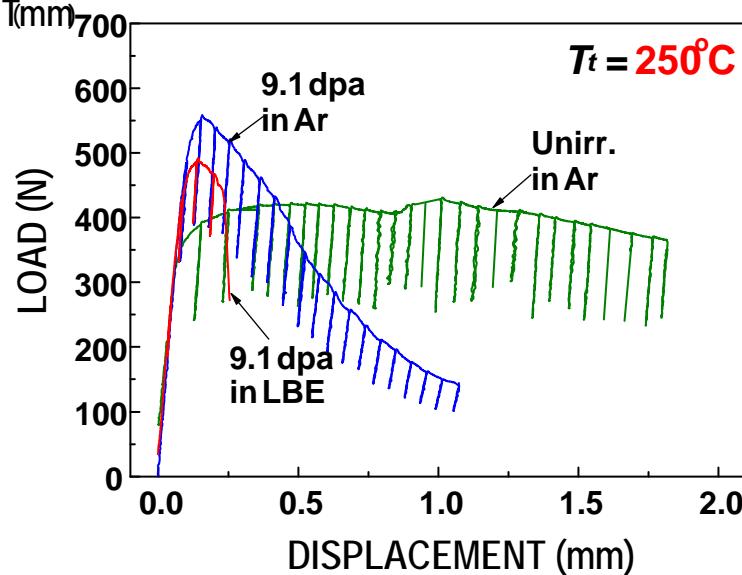
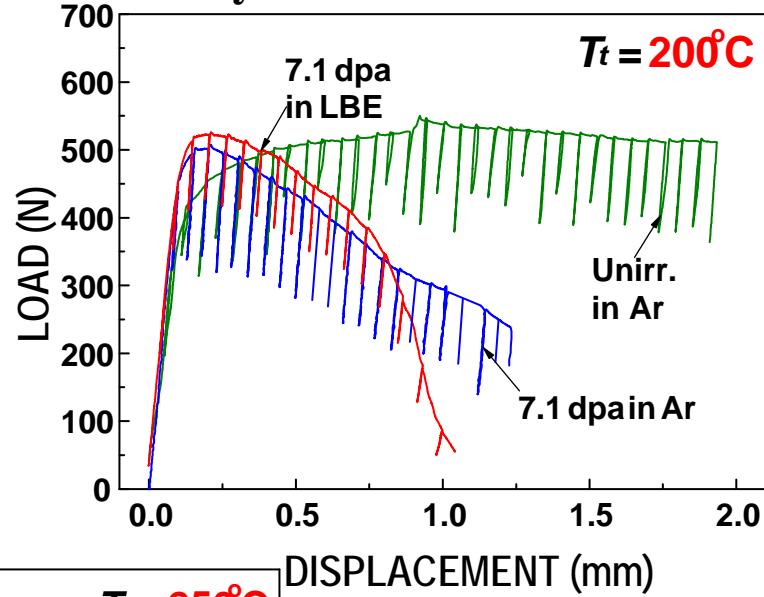
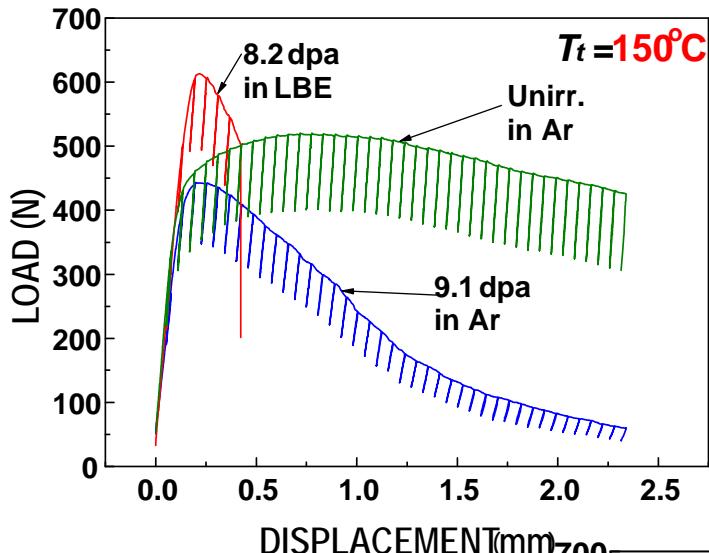


3-p bending test on irradiated T91

(STIP-1 and -3)

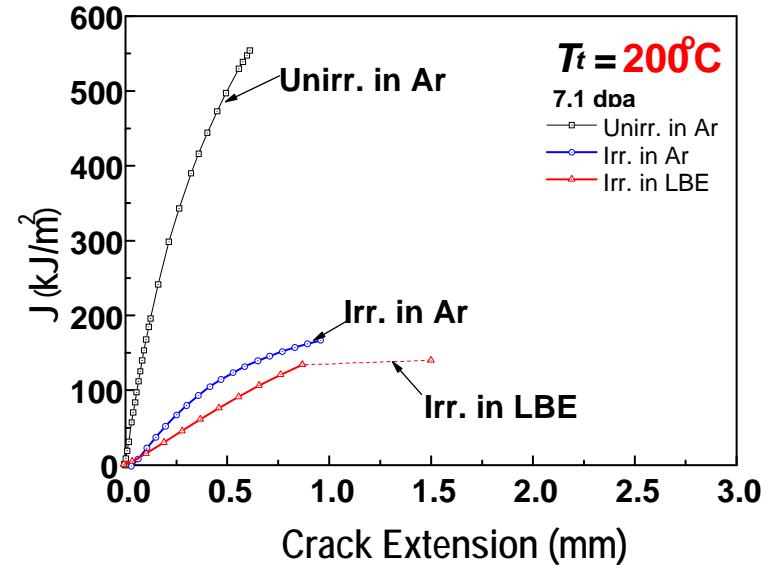
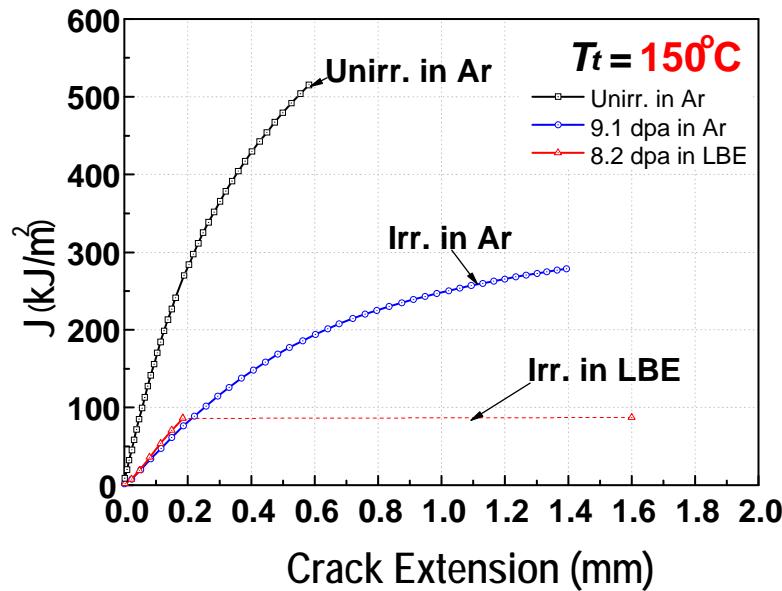
▲ Tested in Ar: irradiation induced embrittlement effect

▲ Tested in LBE: a further embrittlement effect by LBE is observed

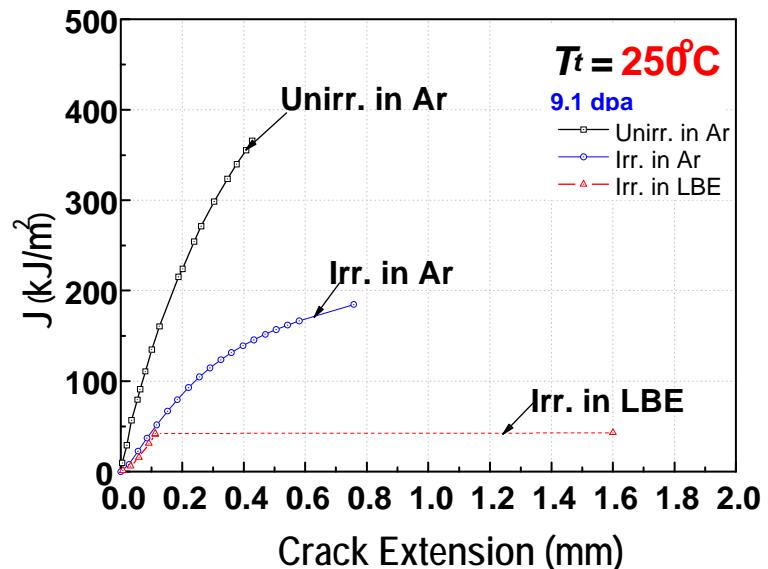


Irradiated T91 (STIP-1 and -3)

J-R curves

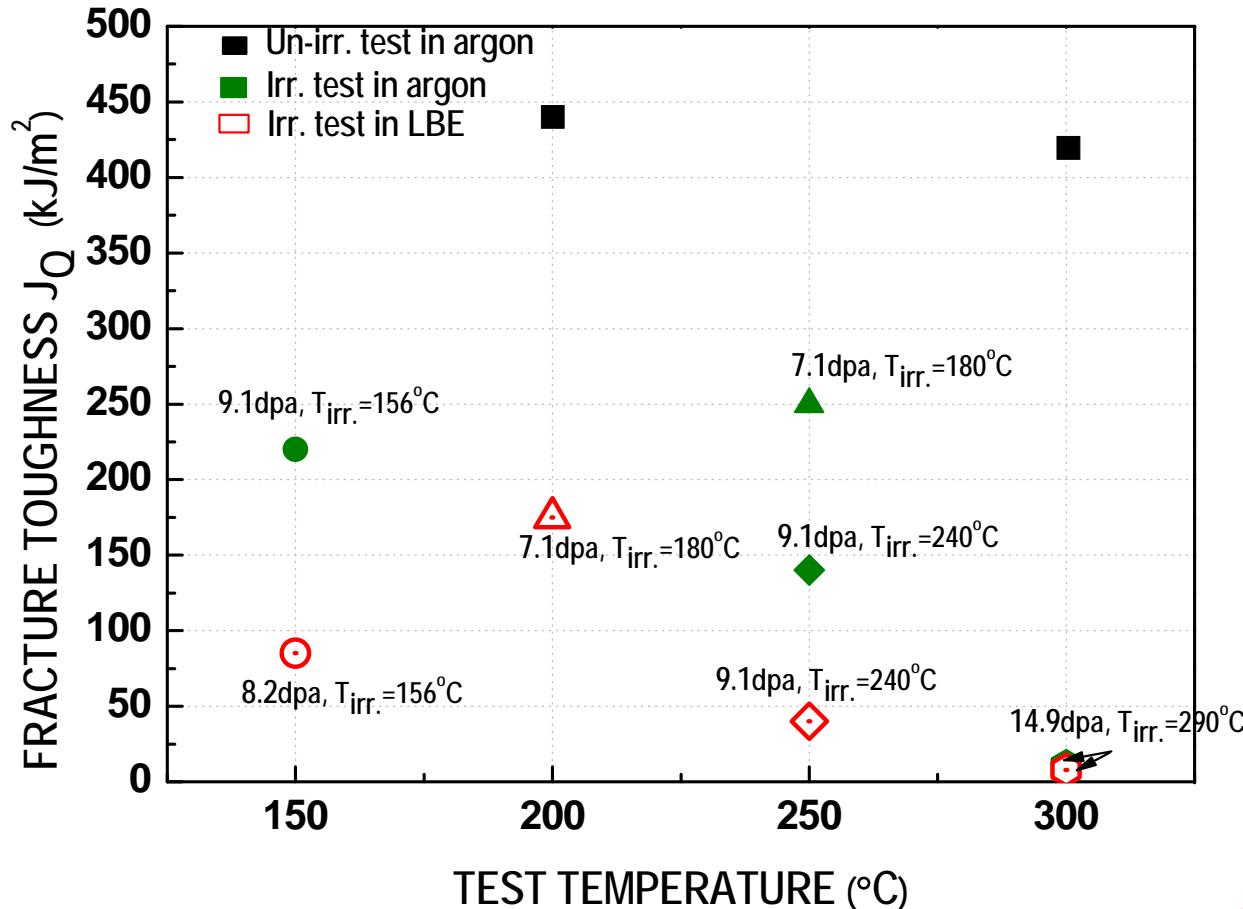


- ▲ J values of irradiated specimens are much lower than those of unirradiated ones
- ▲ J values are further reduced by LBE



Comparison of 3-p bending tests results on irradiated specimens

- ▲ The fracture toughness of irradiated specimens is reduced by irradiation-induced embrittlement
- ▲ The fracture toughness of irradiated specimens decreases further as a result from exposure to liquid LBE



Conclusions

- The ductility trough of the T91 FM steel in the standard heat treatment state is 300-425°C. For the first time, the ductility trough of the T91 steel in LBE is determined.
- The LBE embrittlement effects can be strongly enhanced by the hardening of the steels
- The combination of irradiation-induced embrittlement with LBE-induced embrittlement may give rise to unexpected premature failure. Therefore, it should deserve a great attention.

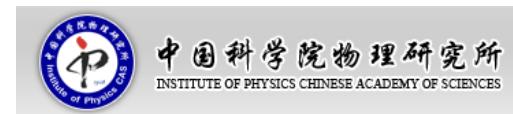
Acknowledgments

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Thank You for Your Attention



Proposed mechanism

