

# 光前夸克模型下 $P \rightarrow T$ 跃迁形状因子研究

学科、专业 : 物理学、粒子物理与原子核物理  
研究方向 : 粒子物理理论  
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# Outline

1 研究动机

2 理论框架

3 数值结果与分析

4 总结与展望

5 致谢

- 由重夸克到轻夸克跃迁引起的 $B$ 介子和 $D$ 介子的衰变过程在检验标准模型和寻找新物理等方面具有重要意义。

$B$ 介子到张量介子的跃迁过程可能存在轻子味普适性破缺。

与标量介子和矢量介子相比，张量介子的衰变具有更多的极化态。

Y. S. Amhis *et al.* [HFLAV], Eur. Phys. J. C **81**, no.3, 226 (2021);

- 在介子弱衰变的研究中，形状因子是必不可少的非微扰输入参数。

光前夸克模型为非微扰物理量的计算提供了一个概念上简单，唯象上可行的理论框架。

M. V. Terentev, Sov. J. Nucl. Phys. **24**, 106 (1976);

V. B. Berestetsky and M. V. Terentev, Sov. J. Nucl. Phys. **25**, 347-354 (1977);

W. Jaus, Phys. Rev. D **41**, 3394 (1990);

W. Jaus and D. Wyler, Phys. Rev. D **41**, 3405 (1990).

主要任务：

$$\mathcal{B} \equiv \langle T(\epsilon^{\mu\nu*}, p'') | \bar{q}_1''(k_1'') \Gamma q_1'(k_1') | P(p') \rangle, \quad \Gamma = \sigma_{\mu\nu}, \sigma_{\mu\nu}\gamma_5, \dots \quad (1)$$

标准光前夸克模型 (SLF QM) :

介子束缚态：

$$|M(p, L, J)\rangle = \sum_{h_1, h_2} \int \frac{d^3 k_1}{(2\pi)^3 2\sqrt{k_1^+}} \frac{d^3 k_2}{(2\pi)^3 2\sqrt{k_2^+}} (2\pi)^3 \delta^3(p - k_1 - k_2) \Psi_{LS}^{JJ_z}(k_1, h_1, k_2, h_2) |q_1(k_1, h_1)\rangle |\bar{q}_2(k_2, h_2)\rangle, \quad (2)$$

动量空间波函数  $\Psi_{LS}^{JJ_z}(k_1, h_1, k_2, h_2)$ :

$$\Psi_{LS}^{JJ_z}(k_1, h_1, k_2, h_2) = S_{h_1, h_2}(x, \mathbf{k}_\perp) \psi(x, \mathbf{k}_\perp) \quad (3)$$

自旋轨道波函数  $S_{h_1, h_2}(x, \mathbf{k}_\perp)$ : Phys. Rev. D 41, 3405 (1990); Phys. Rev. D 69, 074025 (2004);

$$S_{h_1, h_2} = \frac{\bar{u}(k_1, h_1)\Gamma' v(k_2, h_2)}{\sqrt{2}\hat{M}_0}, \quad (4)$$

其中,  $P$ 和 $T$ 介子的顶角算符 $\Gamma'$ :

$$\Gamma'_P = \gamma_5, \quad (5)$$

$$\Gamma'_T = -\frac{1}{2}\hat{\epsilon}^{\mu\nu}\left[\gamma_\mu - \frac{(k_1 - k_2)_\mu}{D_{T,LF}}\right](k_1 - k_2)_\nu, \quad D_{T,LF} = M_0 + m_1 + m_2, \quad (6)$$

径向波函数  $\psi(x, \mathbf{k}_\perp)$ :

$$\psi_s(x, \mathbf{k}_\perp) = 4\frac{\pi^{\frac{3}{4}}}{\beta^{\frac{3}{2}}}\sqrt{\frac{\partial k_z}{\partial x}} \exp\left[-\frac{k_z^2 + \mathbf{k}_\perp^2}{2\beta^2}\right], \quad (7)$$

$$\psi_p(x, \mathbf{k}_\perp) = \frac{\sqrt{2}}{\beta}\psi_s(x, \mathbf{k}_\perp), \quad (8)$$

矩阵元:

$$\begin{aligned} \mathcal{B}_{SLF} &= \sum_{h'_1, h''_1, h_2} \int \frac{dx d^2\mathbf{k}'_\perp}{(2\pi)^3 2x} \psi''^*(x, \mathbf{k}'_\perp) \psi'(x, \mathbf{k}'_\perp) S_{h''_1, h_2}^{''\dagger}(x, \mathbf{k}'_\perp) \\ &\quad C_{h''_1, h'_1}(x, \mathbf{k}'_\perp, \mathbf{k}''_\perp) S'_{h'_1, h_2}(x, \mathbf{k}'_\perp) \end{aligned} \quad (9)$$

## 协变光前夸克模型 (CLF QM) :

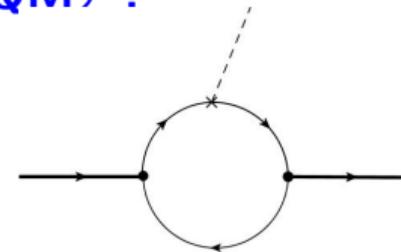


Figure: 矩阵元  $\mathcal{B}$  费曼图。

矩阵元:

$$\mathcal{B} = N_c \int \frac{d^4 k'_1}{(2\pi)^4} \frac{H_P H_T}{N'_1 N''_1 N_2} i \mathcal{S}_{\mathcal{B}} \cdot \epsilon^*, \quad (10)$$

内线费米子圈求迹部分  $\mathcal{S}_{\mathcal{B}}$ :

$$\mathcal{S}_{\mathcal{B}} = \text{Tr} \left[ \Gamma(k'_1 + m'_1) (i\Gamma_P) (-k_2 + m_2) (i\gamma^0 \Gamma_T^\dagger \gamma^0) (k''_1 + m''_1) \right], \quad (11)$$

顶角算符  $\Gamma_{P,T}$ :

$$i\Gamma_P = -i\gamma_5, \quad (12)$$

$$i\Gamma_T = i \frac{1}{2} \left[ \gamma_\mu - \frac{(k''_1 - k_2)_\mu}{D_{T,\text{con}}} \right] (k''_1 - k_2)_\nu, \quad D_{T,\text{con}} = M + m''_1 + m_2, \quad (13)$$

假设:  $H_{P,T}$  在  $k_1^-$  的复平面上是解析的。则, 在对  $k_1^-$  积分后,  $q_2$  在壳, 且有以下替换:

$$N_1'^{(\prime\prime)} \rightarrow \hat{N}_1'^{(\prime\prime)} = x \left( M'^{(\prime\prime)2} - M_0'^{(\prime\prime)2} \right) \quad (14)$$

$$\chi_{P(T)} = H_{P(T)}/N'^{(\prime\prime)} \rightarrow h_{P(T)}/\hat{N}'^{(\prime\prime)}, \quad D_{T,\text{con}} \rightarrow D_{T,\text{LF}}, \quad (\text{type-I}) \quad (15)$$

其中, 顶角  $h_{P(T)}$  为

$$h_{P(T)}/\hat{N}'^{(\prime\prime)} = \frac{1}{\sqrt{2N_c}} \sqrt{\frac{\bar{x}}{x}} \frac{\psi_{s(p)}}{\hat{M}_0'^{(\prime\prime)}}, \quad (16)$$

$$\chi_{P(T)} = H_{P(T)}/N'^{(\prime\prime)} \rightarrow h_{P(T)}/\hat{N}'^{(\prime\prime)}, \quad M \rightarrow M_0, \quad (\text{type-II}) \quad (17)$$

矩阵元:

$$\hat{B} = N_c \int \frac{dx d^2 \mathbf{k}'_\perp}{2(2\pi)^3} \frac{h_P h_T}{\bar{x} \hat{N}_1' \hat{N}_1'} \hat{S}_{\mathcal{B}} \cdot \epsilon^*, \quad (18)$$

为了有效确定zero-mode贡献，我们需要以下的分解替换：

Jaus, Phys. Rev. D **60**, 054026 (1999); H. Y. Cheng, Phys. Rev. D **69**, 074025 (2004)

$$\begin{aligned} \hat{k}_1'^\mu \hat{k}_1'^\nu &\rightarrow g^{\mu\nu} A_1^{(2)} + P^\mu P^\nu A_2^{(2)} + (P^\mu q^\nu + q^\mu P^\nu) A_3^{(2)} + q^\mu q^\nu A_4^{(2)} \\ &+ \frac{P^\mu \omega^\nu + \omega^\mu P^\nu}{\omega \cdot P} B_1^{(2)} + \dots (\omega, C_i^{(j)}) , \end{aligned} \tag{19}$$

CLF QM中形状因子完整结果：

$$[\mathcal{F}]^{\text{full}} = [\mathcal{F}]^{\text{CLF}} + [\mathcal{F}]^{\text{B}} . \tag{20}$$

# 数值结果与分析

$P \rightarrow T$ 跃迁形状因子的定义:

$$\langle T(\epsilon^{\mu\nu}, p'') | \bar{q}_2 \gamma_\mu q_1 | P(p') \rangle = i \varepsilon_{\mu\nu\alpha\beta} e^{*\nu} P^\alpha q^\beta \frac{V(q^2)}{M' + M''}, \quad (21)$$

$$\begin{aligned} \langle T(\epsilon^{\mu\nu}, p'') | \bar{q}_2 \gamma_\mu \gamma_5 q_1 | P(p') \rangle &= -2M'' \frac{e^* \cdot q}{q^2} q_\mu A_0(q^2) \\ &\quad - (M' + M'') \left( e_\mu^* - \frac{e^* \cdot q}{q^2} q_\mu \right) A_1(q^2) \\ &\quad + \frac{e^* \cdot q}{M' + M''} \left( P_\mu - \frac{M'^2 - M''^2}{q^2} q_\mu \right) A_2(q^2), \end{aligned} \quad (22)$$

$$\begin{aligned} \langle T(\epsilon^{\mu\nu}, p'') | \bar{q}_2 \sigma_{\mu\nu} q^\nu (1 + \gamma_5) q_1 | P(p') \rangle &= -\varepsilon_{\mu\nu\alpha\beta} e^{*\nu} P^\alpha q^\beta T_1(q^2) \\ &\quad + i \left[ (M'^2 - M''^2) e_\mu^* - (e^* \cdot q) P_\mu \right] T_2(q^2) \\ &\quad + i \left( e^* \cdot q \right) \left[ q_\mu - \frac{q^2}{M'^2 - M''^2} P_\mu \right] T_3(q^2), \end{aligned} \quad (23)$$

其中,  $\varepsilon_{0123} = -1$ ,  $P = p' + p''$ ,  $q = p' - p''$ ,  $e^{*\nu} \equiv \frac{\epsilon^{*\mu\nu} \cdot p'_\mu}{M'}$ .

## ■ 自洽性问题

$$\begin{aligned}\tilde{T}_3^B = & \frac{2(M'^2 - M''^2)}{e^* \cdot q} \frac{\epsilon^{\lambda\delta*} q_\lambda \omega_\delta}{\omega \cdot P} \left\{ B_1^{(2)} \left[ 3 + \frac{4(m_1'' + 2m_2 - 2m_1'')}{D_{V,\text{con}}} \right] \right. \\ & \left. + 4B_1^{(3)} \left( 1 + \frac{m_1' - m_1'' - 2m_2}{D_{V,\text{con}}} \right) + \frac{8(m_1' - m_2)B_2^{(3)}}{D_{V,\text{con}}} \right\},\end{aligned}\quad (24)$$

$$\tilde{T}_3^B = \begin{cases} \frac{2M'(M'^2 - M''^2)(M'^2 - M''^2 + q_\perp^2)}{(M'^2 - M''^2)^2 + 2(M'^2 - 2M''^2)q_\perp^2 + q_\perp^4} \left\{ B_1^{(2)} \left[ 3 + \frac{4(m_1'' + 2m_2 - 2m_1')}{D_{V,\text{con}}} \right] \right. \\ \left. + 4B_1^{(3)} \left( 1 + \frac{m_1' - m_1'' - 2m_2}{D_{V,\text{con}}} \right) + \frac{8(m_1' - m_2)B_2^{(3)}}{D_{V,\text{con}}} \right\}, & \lambda'' = 0 \\ \frac{M'(M'^2 - M''^2)}{M'^2 - M''^2 + q_\perp^2} \left\{ B_1^{(2)} \left[ 3 + \frac{4(m_1'' + 2m_2 - 2m_1')}{D_{V,\text{con}}} \right] + 4B_1^{(3)} \left( 1 + \frac{m_1' - m_1'' - 2m_2}{D_{V,\text{con}}} \right) \right. \\ \left. + \frac{8(m_1' - m_2)B_2^{(3)}}{D_{V,\text{con}}} \right\}, & \lambda'' = \pm 1 \\ 0. & \lambda'' = \pm 2 \end{cases}\quad (25)$$

显然，这依赖于螺旋度 $\lambda''$ 的选择。

$$[T_3]_{\lambda=0}^{\text{full}} \neq [T_3]_{\lambda=\pm 1}^{\text{full}} \neq [T_3]_{\lambda=\pm 2}^{\text{full}}$$

# 数值结果与分析

定义 $\Delta_B(x)$ 为

$$\Delta_B(x) \equiv \frac{d[\mathcal{F}^B]_{\lambda''}}{dx}, \quad (26)$$

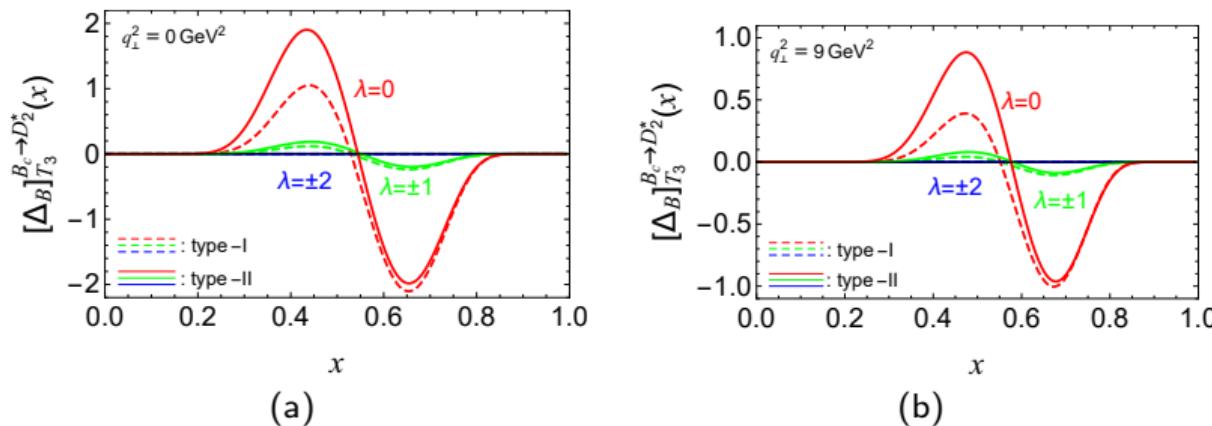


Figure:  $B_c \rightarrow D_2^*$  在  $q_\perp^2 = (0, 0.2) \text{ GeV}^2$  时  $[\Delta_B]_{T_3}(x)$  对  $x$  的依赖性。

# 数值结果与分析

**Table:**  $B_c \rightarrow D_2^*$  过程形状因子  $T_3(q_\perp^2)$  在  $q_\perp^2 = (0, 1, 4, 9) \text{ GeV}^2$  数值结果。

$B_c \rightarrow D_2^*$		$[T_3]_{\lambda''=\pm 2}^{\text{SLF}}$	$[T_3]_{\lambda''=0}^{\text{full}}$	$[T_3]_{\lambda''=\pm 1}^{\text{full}}$	$[T_3]_{\lambda''=\pm 2}^{\text{full}}$	$[T_3]^{\text{val.}}$	$[T_3]^{\text{CLF}}$
$q_\perp^2 = 0$	type-I	0.03	-0.14	-0.04	0.05	0.10	0.05
	type-II	0.08	0.08	0.08	0.08	0.08	0.08
$q_\perp^2 = 1$	type-I	0.03	-0.13	-0.04	0.05	0.09	0.05
	type-II	0.07	0.07	0.07	0.07	0.07	0.07
$q_\perp^2 = 4$	type-I	0.02	-0.11	-0.04	0.03	0.07	0.03
	type-II	0.05	0.05	0.05	0.05	0.05	0.05
$q_\perp^2 = 9$	type-I	0.02	-0.08	-0.03	0.02	0.05	0.02
	type-II	0.04	0.04	0.04	0.04	0.04	0.04

$$[T_3]_{\lambda=0}^{\text{full}} \neq [T_3]_{\lambda=\pm 1}^{\text{full}} \neq [T_3]_{\lambda=\pm 2}^{\text{full}} \quad (\text{type - I}) \quad (27)$$

$$[T_3]_{\lambda=0}^{\text{full}} \doteq [T_3]_{\lambda=\pm 1}^{\text{full}} \doteq [T_3]_{\lambda=\pm 2}^{\text{full}} \quad (\text{type - II}) \quad (28)$$

## ■ “新”的自治性问题

H. Y. Cheng and C. K. Chua, Phys. Rev. D **69**, 094007 (2004)

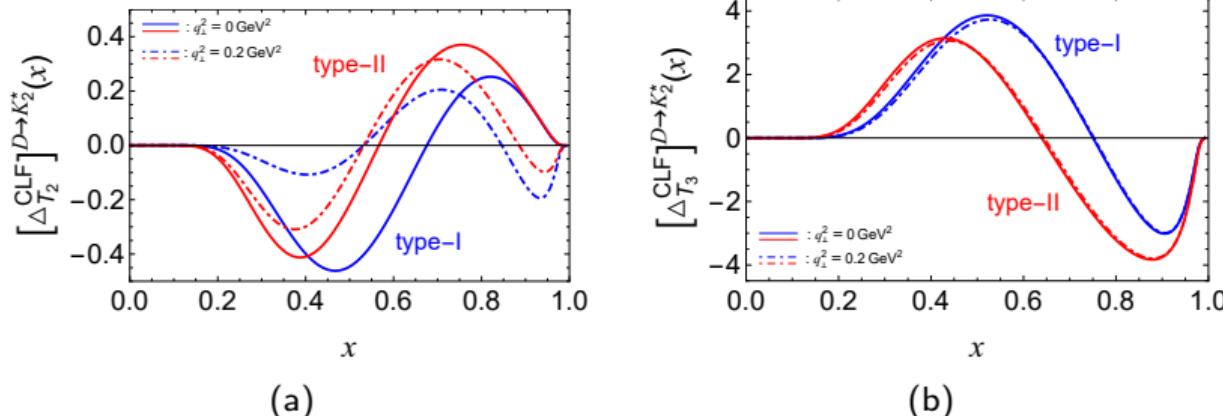
$$\begin{aligned}
 \text{CC : } & 2ig_{\nu\lambda}g_{\alpha\mu}g_{\beta\sigma}(P+q)^\beta \hat{k}'^\sigma_1 \hat{k}'^\alpha_1 \hat{k}'_{1\delta} = 2ig_{\nu\lambda}g_{\alpha\mu}g_{\beta\sigma}(P+q)^\beta \left[ (g^{\alpha\sigma}P_\delta + g_\delta^\alpha P^\sigma \right. \\
 & \quad \left. + g_\delta^\sigma P^\alpha)A_1^{(3)} + (g^{\alpha\sigma}q_\delta + g_\delta^\alpha q^\sigma + g_\delta^\sigma q^\alpha)A_2^{(3)} \right. \\
 & \quad \left. + P^\sigma P^\alpha P_\delta A_3^{(3)} + \dots \right] \\
 \text{ours : } & 2ig_{\nu\lambda}g_{\alpha\mu}g_{\beta\sigma}(P+q)^\beta \hat{k}'^\sigma_1 \hat{k}'^\alpha_1 \hat{k}'_{1\delta} = 2ig_{\nu\lambda} \hat{k}'_{1\mu} \hat{k}'_{1\delta} \hat{k}'_1 \cdot (P+q)
 \end{aligned} \tag{29}$$

定义：

$$\Delta_{\mathcal{F}}^{\text{CLF}}(x, \mathbf{q}_\perp^2) \equiv \frac{d[\mathcal{F}]_{\text{ours}}^{\text{CLF}}}{dx} - \frac{d[\mathcal{F}]_{\text{CC}}^{\text{CLF}}}{dx}, \tag{30}$$

其中， $\mathcal{F} = T_{2,3\circ}$

# 数值结果与分析



**Figure:**  $D \rightarrow K_2^*$  在  $q_\perp^2 = (0, 0.2) \text{ GeV}^2$  时  $\Delta_{T_{2,3}}^{\text{CLF}}$  对  $x$  的依赖性。

## ■ 协变性问题

$$\begin{aligned}
 \tilde{\mathcal{B}}_B(\Gamma = \sigma_{\mu\nu}\gamma_5 q^\nu) = & 4i\omega_\mu \epsilon^{*\lambda\delta} q_\lambda q_\delta \left\{ \frac{B_1^{(2)}}{\omega \cdot P} \left[ 2M'^2 - M''^2 + (m'_1 - m_2)(m_2 - m''_1) + q^2 \right. \right. \\
 & - \frac{2}{D_{V,\text{con}}} \left( (M'^2 - M''^2)(m'_1 + m''_1) - q^2(m'_1 - m''_1 - 2m_2) \right) \left. \right] \\
 & + \dots
 \end{aligned} \tag{31}$$

type-I: 矩阵元的协变性被破坏。

type-II: 协变性问题得以解决。

## ■ 零模贡献

$$[\mathcal{F}]^{\text{CLF}} = [\mathcal{F}]^{\text{val.}} + [\mathcal{F}]^{\text{z.m.}}$$

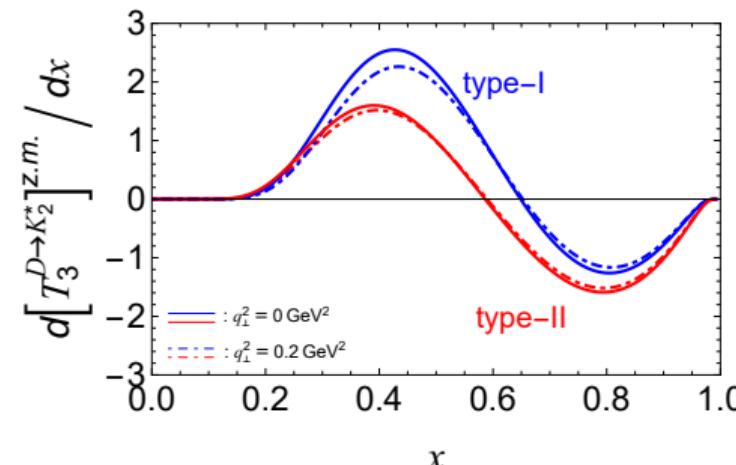


Figure:  $D \rightarrow K_2^*$  在  $\mathbf{q}_{\perp}^2 = (0, 0.2) \text{ GeV}^2$  时  $d[T_3]^{\text{z.m.}} / dx$  对  $x$  的依赖性。

# 数值结果与分析

## ■ 数值结果

拟合方式:

$$\mathcal{F}(q^2) = \frac{\mathcal{F}(0)}{1 - q^2/m_{i,pole}^2} \left\{ 1 + \sum_{k=1}^N b_k [z(q^2, t_0)^k - z(0, t_0)^k] \right\}, \quad (32)$$

其中,  $z(q^2, t_0) = \frac{\sqrt{t_+ - q^2} - \sqrt{t_+ - t_0}}{\sqrt{t_+ - q^2} + \sqrt{t_+ - t_0}}$ ,  $t_{\pm} = (M' \pm M'')^2$ ,  $t_0 = (M' + M'')(\sqrt{M'} - \sqrt{M''})^2$ 。

**Table:**  $q^2 = (3, 5, 7) \text{GeV}^2$  处  $B \rightarrow D_2^*$  跃迁过程  $Z_k(q^2)$  的数值结果。

$B \rightarrow D_2^*$	$q^2 = 3 \text{GeV}^2$	$q^2 = 5 \text{GeV}^2$	$q^2 = 7 \text{GeV}^2$
$Z_1(q^2)$	$-1.28 \times 10^{-2}$	$-2.18 \times 10^{-2}$	$-3.11 \times 10^{-2}$
$Z_2(q^2)$	$-2.92 \times 10^{-4}$	$-3.00 \times 10^{-4}$	$-1.40 \times 10^{-4}$

# 数值结果与分析

Table:  $B \rightarrow D_2^*$  过程形状因子  $b_1$  和  $b_2$  的数值。

$B \rightarrow D_2^*$	$V$	$A_0$	$A_1$	$A_2$	$T_1$	$T_2$	$T_3$
$b_1$	$-6.59(-6.20)$	$-6.64(-6.20)$	$-3.19(-3.00)$	$-6.44(-6.10)$	$-6.61(-6.30)$	$-2.47(-2.40)$	$-5.85(-5.91)$
$b_2$	5.94	6.51	2.44	5.93	4.87	1.17	0.50

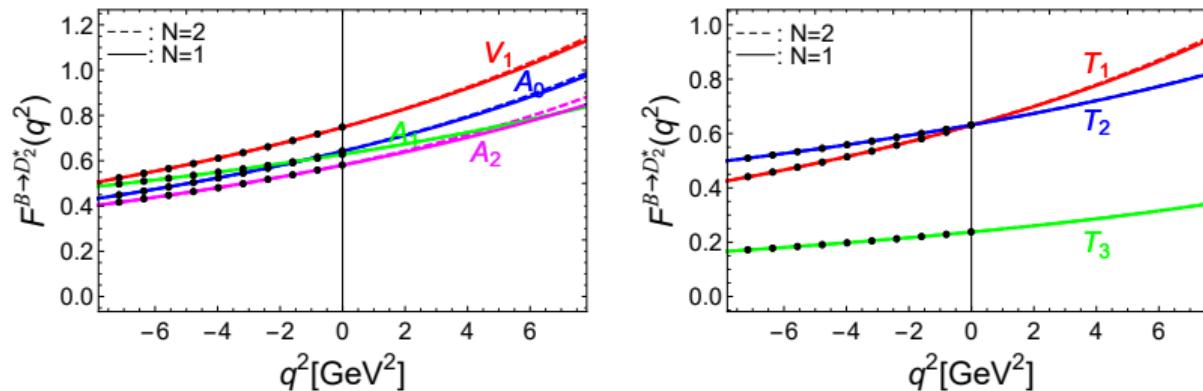


Figure:  $B \rightarrow D_2^*$  过程在  $N = 1$  和  $N = 2$  截断方案下对  $q^2$  的依赖图。

# 数值结果与分析

$\mathcal{F}$	$F(0)$	$b_1$	$\mathcal{F}$	$F(0)$	$b_1$	$\mathcal{F}$	$F(0)$	$b_1$
$V^{D \rightarrow a_2}$	$0.96_{-0.16}^{+0.18}$	$-4.60_{-2.70}^{+3.60}$	$V^{D \rightarrow K_2^*}$	$1.00_{-0.16}^{+0.15}$	$-4.60_{-2.32}^{+2.84}$	$V^{D_s \rightarrow K_2^*}$	$0.98_{-0.19}^{+0.22}$	$-4.80_{-3.10}^{+4.00}$
$A_0^{D \rightarrow a_2}$	$0.62_{-0.07}^{+0.07}$	$-3.70_{-2.90}^{+3.90}$	$A_0^{D \rightarrow K_2^*}$	$0.68_{-0.08}^{+0.06}$	$-3.70_{-2.48}^{+3.10}$	$A_0^{D_s \rightarrow K_2^*}$	$0.58_{-0.08}^{+0.08}$	$-4.20_{-3.40}^{+4.50}$
$A_1^{D \rightarrow a_2}$	$0.63_{-0.10}^{+0.11}$	$-2.00_{-1.80}^{+2.60}$	$A_1^{D \rightarrow K_2^*}$	$0.71_{-0.10}^{+0.09}$	$-1.90_{-1.63}^{+1.98}$	$A_1^{D_s \rightarrow K_2^*}$	$0.61_{-0.10}^{+0.12}$	$-2.60_{-2.30}^{+3.00}$
$A_2^{D \rightarrow a_2}$	$0.45_{-0.10}^{+0.10}$	$-3.70_{-1.90}^{+2.70}$	$A_2^{D \rightarrow K_2^*}$	$0.58_{-0.10}^{+0.11}$	$-4.90_{-1.97}^{+2.58}$	$A_2^{D_s \rightarrow K_2^*}$	$0.51_{-0.10}^{+0.14}$	$-5.10_{-2.50}^{+3.40}$
$T_1^{D \rightarrow a_2}$	$0.61_{-0.08}^{+0.08}$	$-4.06_{-3.00}^{+3.80}$	$T_1^{D \rightarrow K_2^*}$	$0.68_{-0.09}^{+0.07}$	$-3.63_{-2.27}^{+2.27}$	$T_1^{D_s \rightarrow K_2^*}$	$0.58_{-0.09}^{+0.09}$	$-4.58_{-3.42}^{+3.00}$
$T_2^{D \rightarrow a_2}$	$0.61_{-0.08}^{+0.08}$	$4.78_{-1.38}^{+2.00}$	$T_2^{D \rightarrow K_2^*}$	$0.68_{-0.09}^{+0.08}$	$4.64_{-1.29}^{+1.66}$	$T_2^{D_s \rightarrow K_2^*}$	$0.58_{-0.09}^{+0.09}$	$4.23_{-1.23}^{+1.87}$
$T_3^{D \rightarrow a_2}$	$0.22_{-0.06}^{+0.03}$	$-4.85_{-1.81}^{+1.85}$	$T_3^{D \rightarrow K_2^*}$	$0.17_{-0.10}^{+0.07}$	$-2.85_{-1.58}^{+1.35}$	$T_3^{D_s \rightarrow K_2^*}$	$0.15_{-0.06}^{+0.05}$	$-4.21_{-2.42}^{+1.97}$
$V^{D_s \rightarrow f'_2}$	$1.19_{-1.20}^{+0.19}$	$-4.40_{-2.50}^{+3.00}$	$V^{n_c(1S) \rightarrow D_2^*}$	$2.87_{-0.93}^{+1.47}$	$-19.4_{-10.4}^{+10.8}$	$V^{n_c(1S) \rightarrow D_{s2}^*}$	$3.67_{-1.12}^{+1.53}$	$-14.6_{-8.34}^{+9.59}$
$A_0^{D_s \rightarrow f'_2}$	$0.72_{-0.08}^{+0.07}$	$-3.70_{-2.80}^{+3.42}$	$A_0^{n_c(1S) \rightarrow D_2^*}$	$0.96_{-0.20}^{+0.22}$	$-18.5_{-10.8}^{+11.4}$	$A_0^{n_c(1S) \rightarrow D_{s2}^*}$	$1.28_{-0.24}^{+0.25}$	$-13.3_{-8.85}^{+9.59}$
$A_1^{D_s \rightarrow f'_2}$	$0.77_{-0.11}^{+0.10}$	$-2.10_{-1.11}^{+2.21}$	$A_1^{n_c(1S) \rightarrow D_2^*}$	$1.10_{-0.27}^{+0.34}$	$-15.8_{-8.7}^{+12.2}$	$A_1^{n_c(1S) \rightarrow D_{s2}^*}$	$1.47_{-0.35}^{+0.35}$	$-10.8_{-7.32}^{+7.86}$
$A_2^{D_s \rightarrow f'_2}$	$0.67_{-0.13}^{+0.15}$	$-4.90_{-2.36}^{+2.99}$	$A_2^{n_c(1S) \rightarrow D_2^*}$	$0.98_{-0.30}^{+0.55}$	$-14.2_{-10.1}^{+13.0}$	$A_2^{n_c(1S) \rightarrow D_{s2}^*}$	$1.13_{-0.62}^{+0.62}$	$-8.39_{-10.3}^{+13.4}$
$T_1^{D_s \rightarrow f'_2}$	$0.73_{-0.10}^{+0.08}$	$-3.64_{-2.31}^{+2.59}$	$T_1^{n_c(1S) \rightarrow D_2^*}$	$1.04_{-0.23}^{+0.27}$	$-22.1_{-10.4}^{+10.9}$	$T_1^{n_c(1S) \rightarrow D_{s2}^*}$	$1.38_{-0.28}^{+0.30}$	$-16.9_{-8.56}^{+9.07}$
$T_2^{D_s \rightarrow f'_2}$	$0.75_{-0.09}^{+0.08}$	$6.30_{-1.85}^{+1.89}$	$T_2^{n_c(1S) \rightarrow D_2^*}$	$1.04_{-0.23}^{+0.27}$	$28.4_{-13.8}^{+7.53}$	$T_2^{n_c(1S) \rightarrow D_{s2}^*}$	$1.38_{-0.28}^{+0.30}$	$88.1_{-21.7}^{+26.1}$
$T_3^{D_s \rightarrow f'_2}$	$0.15_{-0.12}^{+0.07}$	$-2.27_{-1.83}^{+1.09}$	$T_3^{n_c(1S) \rightarrow D_2^*}$	$0.16_{-0.23}^{+0.18}$	$-41.1_{-10.6}^{+8.96}$	$T_3^{n_c(1S) \rightarrow D_{s2}^*}$	$0.35_{-0.35}^{+0.28}$	$-30.0_{-2.50}^{+6.30}$
$V^{B_c \rightarrow B_s^*}$	$13.4_{-11.1}^{+5.30}$	$-87.6_{-23.5}^{+26.7}$	$V^{B_c \rightarrow B_s^*}$	$14.8_{-4.12}^{+5.59}$	$-74.7_{-14.1}^{+20.2}$	$V^{B_c \rightarrow B_s^*}$	$14.8_{-4.12}^{+5.59}$	$-74.7_{-14.1}^{+20.2}$
$A_0^{B_c \rightarrow B_s^*}$	$2.01_{-0.37}^{+0.33}$	$-19.3_{-1.39}^{+3.39}$	$A_0^{B_c \rightarrow B_s^*}$	$2.45_{-0.14}^{+0.11}$	$-20.5_{-1.03}^{+5.34}$	$A_0^{B_c \rightarrow B_s^*}$	$2.45_{-0.14}^{+0.11}$	$-20.5_{-1.03}^{+5.34}$
$A_1^{B_c \rightarrow B_s^*}$	$2.42_{-0.60}^{+0.60}$	$-35.4_{-3.03}^{+1.13}$	$A_1^{B_c \rightarrow B_s^*}$	$2.94_{-0.30}^{+0.10}$	$-35.4_{-3.03}^{+2.79}$	$A_1^{B_c \rightarrow B_s^*}$	$2.94_{-0.30}^{+0.10}$	$-35.4_{-3.03}^{+2.79}$
$A_2^{B_c \rightarrow B_s^*}$	$2.51_{-1.15}^{+2.42}$	$-31.6_{-14.1}^{+32.0}$	$A_2^{B_c \rightarrow B_s^*}$	$3.45_{-1.60}^{+3.15}$	$-29.4_{-7.91}^{+16.5}$	$A_2^{B_c \rightarrow B_s^*}$	$3.45_{-1.60}^{+3.15}$	$-29.4_{-7.91}^{+16.5}$
$T_1^{B_c \rightarrow B_s^*}$	$2.24_{-0.43}^{+0.43}$	$-77.1_{-11.7}^{+10.1}$	$T_1^{B_c \rightarrow B_s^*}$	$2.69_{-0.49}^{+0.43}$	$-74.5_{-3.43}^{+4.74}$	$T_1^{B_c \rightarrow B_s^*}$	$2.69_{-0.49}^{+0.43}$	$-74.5_{-3.43}^{+4.74}$
$T_2^{B_c \rightarrow B_s^*}$	$2.25_{-0.45}^{+0.45}$	$89.2_{-20.2}^{+22.9}$	$T_2^{B_c \rightarrow B_s^*}$	$2.69_{-0.18}^{+0.10}$	$117_{-26.4}^{+23.5}$	$T_2^{B_c \rightarrow B_s^*}$	$2.69_{-0.18}^{+0.10}$	$117_{-26.4}^{+23.5}$
$T_3^{B_c \rightarrow B_s^*}$	$-0.06_{-1.43}^{+0.90}$	$-60.1_{-24.8}^{+13.0}$	$T_3^{B_c \rightarrow B_s^*}$	$-0.52_{-1.82}^{+1.29}$	$-61.1_{-26.1}^{+21.3}$	$T_3^{B_c \rightarrow B_s^*}$	$-0.52_{-1.82}^{+1.29}$	$-61.1_{-26.1}^{+21.3}$

$\mathcal{F}$	$F(0)$	$b_1$	$\mathcal{F}$	$F(0)$	$b_1$	$\mathcal{F}$	$F(0)$	$b_1$
$V^{B \rightarrow a_2}$	$0.24_{-0.03}^{+0.03}$	$-5.30_{-0.61}^{+1.10}$	$V^{B \rightarrow K_2^*}$	$0.28_{-0.05}^{+0.05}$	$-5.50_{-0.59}^{+1.10}$	$V^{B \rightarrow D_2^*}$	$0.75_{-0.13}^{+0.13}$	$-6.20_{-0.50}^{+0.52}$
$A_0^{B \rightarrow a_2}$	$0.21_{-0.03}^{+0.03}$	$-5.40_{-0.61}^{+0.74}$	$A_0^{B \rightarrow K_2^*}$	$0.21_{-0.04}^{+0.05}$	$-5.60_{-0.59}^{+0.74}$	$A_0^{B \rightarrow D_2^*}$	$0.64_{-0.13}^{+0.13}$	$-6.20_{-0.51}^{+0.53}$
$A_1^{B \rightarrow a_2}$	$0.13_{-0.04}^{+0.04}$	$-2.30_{-0.52}^{+0.52}$	$A_1^{B \rightarrow K_2^*}$	$0.20_{-0.04}^{+0.07}$	$-2.50_{-0.51}^{+0.51}$	$A_1^{B \rightarrow D_2^*}$	$0.62_{-0.11}^{+0.11}$	$-3.00_{-0.49}^{+0.51}$
$A_2^{B \rightarrow a_2}$	$0.17_{-0.02}^{+0.02}$	$-4.80_{-0.80}^{+0.83}$	$A_2^{B \rightarrow K_2^*}$	$0.20_{-0.04}^{+0.04}$	$-5.20_{-0.92}^{+0.93}$	$A_2^{B \rightarrow D_2^*}$	$0.58_{-0.12}^{+0.12}$	$-6.10_{-0.38}^{+0.52}$
$T_1^{B \rightarrow a_2}$	$0.13_{-0.03}^{+0.03}$	$-5.40_{-0.75}^{+0.75}$	$T_1^{B \rightarrow K_2^*}$	$0.23_{-0.04}^{+0.04}$	$-5.60_{-0.75}^{+0.75}$	$T_1^{B \rightarrow D_2^*}$	$0.65_{-0.11}^{+0.11}$	$-6.30_{-0.31}^{+0.52}$
$T_2^{B \rightarrow a_2}$	$0.10_{-0.03}^{+0.03}$	$-2.00_{-0.42}^{+0.42}$	$T_2^{B \rightarrow K_2^*}$	$0.23_{-0.04}^{+0.04}$	$-2.20_{-0.26}^{+0.41}$	$T_2^{B \rightarrow D_2^*}$	$0.63_{-0.12}^{+0.12}$	$-2.40_{-0.33}^{+0.20}$
$T_3^{B \rightarrow a_2}$	$0.12_{-0.01}^{+0.01}$	$-4.90_{-0.32}^{+1.35}$	$T_3^{B \rightarrow K_2^*}$	$0.13_{-0.01}^{+0.03}$	$-5.20_{-0.32}^{+1.30}$	$T_3^{B \rightarrow D_2^*}$	$0.24_{-0.01}^{+0.01}$	$-5.91_{-0.30}^{+0.47}$
$V^{B_c \rightarrow K_2^*}$	$0.23_{-0.04}^{+0.04}$	$-6.50_{-0.66}^{+1.26}$	$V^{B_c \rightarrow f'_2}$	$0.37_{-0.06}^{+0.06}$	$-6.30_{-0.37}^{+0.66}$	$V^{B_c \rightarrow D_2^*}$	$0.96_{-0.17}^{+0.18}$	$-6.50_{-0.66}^{+0.66}$
$A_0^{B_c \rightarrow K_2^*}$	$0.18_{-0.04}^{+0.04}$	$-6.80_{-0.42}^{+0.42}$	$A_0^{B_c \rightarrow f'_2}$	$0.20_{-0.05}^{+0.05}$	$-6.50_{-0.47}^{+0.47}$	$A_0^{B_c \rightarrow D_2^*}$	$0.76_{-0.13}^{+0.13}$	$-6.60_{-0.67}^{+0.67}$
$A_1^{B_c \rightarrow K_2^*}$	$0.17_{-0.03}^{+0.03}$	$-4.09_{-0.04}^{+0.04}$	$A_1^{B_c \rightarrow f'_2}$	$0.21_{-0.05}^{+0.05}$	$-3.70_{-0.10}^{+0.19}$	$A_1^{B_c \rightarrow D_2^*}$	$0.74_{-0.14}^{+0.14}$	$-3.40_{-0.67}^{+0.67}$
$A_2^{B_c \rightarrow K_2^*}$	$0.10_{-0.03}^{+0.03}$	$-6.10_{-0.12}^{+0.31}$	$A_2^{B_c \rightarrow f'_2}$	$0.22_{-0.04}^{+0.04}$	$-6.00_{-0.37}^{+0.40}$	$A_2^{B_c \rightarrow D_2^*}$	$0.66_{-0.20}^{+0.20}$	$-6.00_{-0.60}^{+0.64}$
$T_1^{B_c \rightarrow K_2^*}$	$0.17_{-0.04}^{+0.04}$	$-6.80_{-0.12}^{+0.12}$	$T_1^{B_c \rightarrow f'_2}$	$0.25_{-0.04}^{+0.04}$	$-6.30_{-0.37}^{+0.37}$	$T_1^{B_c \rightarrow D_2^*}$	$0.75_{-0.14}^{+0.14}$	$-6.70_{-0.67}^{+0.67}$
$T_2^{B_c \rightarrow K_2^*}$	$0.17_{-0.04}^{+0.04}$	$-3.70_{-0.12}^{+0.02}$	$T_2^{B_c \rightarrow f'_2}$	$0.34_{-0.04}^{+0.04}$	$-3.40_{-0.03}^{+0.03}$	$T_2^{B_c \rightarrow D_2^*}$	$0.75_{-0.14}^{+0.14}$	$-2.30_{-0.38}^{+0.12}$
$T_3^{B_c \rightarrow K_2^*}$	$0.10_{-0.03}^{+0.03}$	$-6.30_{-0.18}^{+0.18}$	$T_3^{B_c \rightarrow f'_2}$	$0.14_{-0.03}^{+0.03}$	$-6.10_{-0.01}^{+0.18}$	$T_3^{B_c \rightarrow D_2^*}$	$0.29_{-0.18}^{+0.22}$	$-6.00_{-0.50}^{+0.50}$
$V^{B_c \rightarrow D_2^*}$	$0.35_{-0.09}^{+0.09}$	$-14.0_{-0.99}^{+1.10}$	$V^{B_c \rightarrow D_{s2}^*}$	$0.62_{-0.19}^{+0.19}$	$-13.0_{-0.20}^{+2.40}$	$V^{B_c \rightarrow x_{c2}(1P)}$	$1.54_{-0.38}^{+0.31}$	$-13.0_{-0.20}^{+2.90}$
$A_0^{B_c \rightarrow D_2^*}$	$0.19_{-0.09}^{+0.09}$	$-15.0_{-0.91}^{+0.97}$	$A_0^{B_c \rightarrow D_{s2}^*}$	$0.37_{-0.19}^{+0.19}$	$-13.0_{-0.20}^{+0.98}$	$A_0^{B_c \rightarrow x_{c2}(1P)}$	$0.96_{-0.23}^{+0.20}$	$-13.0_{-0.20}^{+3.00}$
$A_1^{B_c \rightarrow D_2^*}$	$0.19_{-0.09}^{+0.09}$	$-12.0_{-0.91}^{+0.90}$	$A_1^{B_c \rightarrow D_{s2}^*}$	$0.38_{-0.19}^{+0.18}$	$-10.0_{-0.20}^{+1.40}$	$A_1^{B_c \rightarrow x_{c2}(1P)}$	$0.97_{-0.22}^{+0.20}$	$-8.00_{-0.20}^{+2.20}$
$A_2^{B_c \rightarrow D_2^*}$	$0.18_{-0.09}^{+0.09}$	$-13.0_{-0.91}^{+0.90}$	$A_2^{B_c \rightarrow D_{s2}^*}$	$0.31_{-0.19}^{+0.18}$	$-11.0_{-0.20}^{+1.20}$	$A_2^{B_c \rightarrow x_{c2}(1P)}$	$0.87_{-0.22}^{+0.22}$	$-12.0_{-0.20}^{+3.00}$
$T_1^{B_c \rightarrow D_2^*}$	$0.19_{-0.09}^{+0.09}$	$-15.0_{-0.91}^{+0.98}$	$T_1^{B_c \rightarrow D_{s2}^*}$	$0.37_{-0.19}^{+0.18}$	$-13.0_{-0.20}^{+0.98}$	$T_1^{B_c \rightarrow x_{c2}(1P)}$	$0.96_{-0.20}^{+0.20}$	$-13.0_{-0.20}^{+3.00}$
$T_2^{B_c \rightarrow D_2^*}$	$0.19_{-0.09}^{+0.09}$	$-12.0_{-0.91}^{+0.90}$	$T_2^{B_c \rightarrow D_{s2}^*}$	$0.37_{-0.19}^{+0.18}$	$-9.0_{-0.20}^{+0.99}$	$T_2^{B_c \rightarrow x_{c2}(1P)}$	$0.96_{-0.20}^{+0.20}$	$-7.0_{-0.20}^{+2.00}$
$T_3^{B_c \rightarrow D_2^*}$	$0.08_{-0.01}^{+0.03}$	$-15.5_{-0.75}^{+0.75}$	$T_3^{B_c \rightarrow D_{s2}^*}$	$0.15_{-0.04}^{+0.03}$	$-13.0_{-0.01}^{+1.00}$	$T_3^{B_c \rightarrow x_{c2}(1P)}$	$0.29_{-0.07}^{+0.03}$	$-13.0_{-0.10}^{+1.70}$
$V^{B_c(1S) \rightarrow B_s^*}$	$0.61_{-0.10}^{+0.10}$	$-57.4_{-4.43}^{+4.43}$	$V^{B_c(1S) \rightarrow D_{s2}^*}$	$0.90_{-0.24}^{+0.24}$	$-56.0_{-4.03}^{+4.43}$	$V^{B_c(1S) \rightarrow D_{s2}^*}$	$0.90_{-0.24}^{+0.24}$	$-56.0_{-4.03}^{+4.43}$
$A_0^{B_c(1S) \rightarrow B_s^*}$	$0.19_{-0.06}^{+0.07}$	$-58.5_{-1.27}^{+1.18}$	$A_0^{B_c(1S) \rightarrow D_{s2}^*}$	$0.29_{-0.06}^{+0.09}$	$-57.2_{-1.22}^{+1.27}$	$A_0^{B_c(1S) \rightarrow D_{s2}^*}$	$0.62_{-0.11}^{+0.11}$	$-57.2_{-1.22}^{+1.27}$
$A_1^{B_c(1S) \rightarrow B_s^*}$	$0.21_{-0.06}^{+0.06}$	$-53.0_{-1.20}^{+1.20}$	$A_1^{B_c(1S) \rightarrow D_{s2}^*}$	$0.32_{-0.06}^{+0.09}$	$-51.5_{-1.26}^{+1.26}$	$A_1^{B_c(1S) \rightarrow D_{s2}^*}$	$0.58_{-0.12}^{+0.12}$	$-51.5_{-1.26}^{+1.26}$
$A_2^{B_c(1S) \rightarrow B_s^*}$	$0.23_{-0.06}^{+0.06}$	$-52.8_{-0.84}^{+0.82}$	$A_2^{B_c(1S) \rightarrow D_{s2}^*}$	$0.35_{-0.11}^{+0.14}$	$-51.4_{-0.81}^{+0.96}$	$A_2^{B_c(1S) \rightarrow D_{s2}^*}$	$0.54_{-0.12}^{+0.12}$	$-51.4_{-0.81}^{+0.96}$
$T_1^{B_c(1S) \rightarrow B_s^*}$	$0.20_{-0.06}^{+0.06}$	$-58.7_{-1.20}^{+1.16}$	$T_1^{B_c(1S) \rightarrow D_{s2}^*}$	$0.30_{-0.06}^{+0.08}$	$-57.4_{-1.20}^{+0.99}$	$T_1^{B_c(1S) \rightarrow D_{s2}^*}$	$0.60_{-0.12}^{+0.12}$	$-57.4_{-1.20}^{+0.99}$
$T_2^{B_c(1S) \rightarrow B_s^*}$	$0.20_{-0.06}^{+0.06}$	$-54.1_{-1.75}^{+1.78}$	$T_2^{B_c(1S) \rightarrow D_{s2}^*}$	$0.30_{-0.06}^{+0.08}$	$-52.2_{-1.72}^{+0.92}$	$T_2^{B_c(1S) \rightarrow D_{s2}^*}$	$0.59_{-0.12}^{+0.12}$	$-52.2_{-1.72}^{+0.92}$
$T_3^{B_c(1S) \rightarrow B_s^*}$	$0.09_{-0.02}^{+0.03}$	$-73.6_{-2.28}^{+2.28}$	$T_3^{B_c(1S) \rightarrow D_{s2}^*}$	$0.08_{-0.03}^{+0.03}$	$-71.4_{-2.28}^{+2.28}$	$T_3^{B_c(1S) \rightarrow D_{s2}^*}$	$0.08_{-0.03}^{+0.03}$	$-71.4_{-2.28}^{+2.28}$

Figure:  $D \rightarrow (a_2, K_2^*)$ ,  $D_s \rightarrow (K_2^*, f'_2)$ ,  $B_c \rightarrow (B_s^*, D_{s2}^*)$ ,  $B \rightarrow (a_2, K_2^*, D_2^*)$ ,  $B_s \rightarrow (K_2^*, f'_2, D_{s2}^*)$ ,  $B_c \rightarrow (D_2^*, D_{s2}^*, \chi_{c2}(1P))$ ,  $\eta_b(1S) \rightarrow (B_2^*, B_{s2}^*)$  形状因子的拟合结果。

# 数值结果与分析

**Table:** 本文在  $q^2 = 0$  计算的  $B \rightarrow a_2$  和  $B \rightarrow K_2^*$  形状因子的理论预测, 以及采用 QCD SR 和传统 CLF QM 计算的结果。

	$B \rightarrow a_2$				$B \rightarrow K_2^*$			
	this work	LCSR	pQCD	CLF	this work	LCSR	pQCD	CLF
$V(0)$	$0.24^{+0.04}_{-0.04}$	$0.18^{+0.12}_{-0.07}$	$0.18^{+0.05}_{-0.04}$	0.28	$0.28^{+0.05}_{-0.05}$	$0.22^{+0.11}_{-0.08}$	$0.21^{+0.06}_{-0.05}$	0.29
$A_0(0)$	$0.21^{+0.03}_{-0.03}$	$0.30^{+0.06}_{-0.05}$	$0.18^{+0.06}_{-0.04}$	0.24	$0.24^{+0.04}_{-0.04}$	$0.30^{+0.06}_{-0.05}$	$0.18^{+0.05}_{-0.04}$	0.23
$A_1(0)$	$0.19^{+0.04}_{-0.03}$	$0.16^{+0.09}_{-0.05}$	$0.11^{+0.03}_{-0.03}$	0.21	$0.22^{+0.07}_{-0.01}$	$0.19^{+0.09}_{-0.07}$	$0.13^{+0.04}_{-0.03}$	0.22
$A_2(0)$	$0.17^{+0.03}_{-0.02}$	$0.07^{+0.08}_{-0.03}$	$0.06^{+0.02}_{-0.01}$	0.19	$0.20^{+0.04}_{-0.03}$	$0.11^{+0.05}_{-0.06}$	$0.08^{+0.03}_{-0.02}$	0.21
$T_1(0)$	$0.19^{+0.03}_{-0.03}$	$0.15^{+0.09}_{-0.05}$	$0.15^{+0.04}_{-0.03}$		$0.23^{+0.04}_{-0.04}$	$0.19^{+0.09}_{-0.06}$	$0.17^{+0.05}_{-0.04}$	0.28
$T_2(0)$	$0.19^{+0.03}_{-0.03}$	$0.15^{+0.09}_{-0.05}$	$0.15^{+0.04}_{-0.03}$		$0.23^{+0.04}_{-0.04}$	$0.19^{+0.09}_{-0.06}$	$0.17^{+0.05}_{-0.04}$	0.28
$T_3(0)$	$0.16^{+0.01}_{-0.05}$	$0.07^{+0.06}_{-0.03}$	$0.13^{+0.04}_{-0.03}$		$0.12^{+0.03}_{-0.01}$	$0.09^{+0.06}_{-0.04}$	$0.14^{+0.05}_{-0.03}$	-0.25

# 数值结果与分析

**Table:**  $B \rightarrow \bar{D}_2^* \ell^+ \nu_\ell$  ( $\ell = e, \mu$ ) 和  $B \rightarrow \bar{D}_2^* \tau^+ \nu_\tau$  分支比的数值结果。

	type-II	type-I	QCD SR	LCSR
$\mathcal{B}(B \rightarrow \bar{D}_2^* \ell^+ \nu_\ell)$	$(1.23^{+0.36}_{-0.39}) \times 10^{-2}$	$(0.63^{+0.39}_{-0.34}) \times 10^{-2}$	$(1.01^{+0.30}_{-0.30}) \times 10^{-3}$	$(3.80^{+0.74}_{-0.74}) \times 10^{-2}$
$\mathcal{B}(B \rightarrow \bar{D}_2^* \tau^+ \nu_\tau)$	$(0.49^{+0.15}_{-0.16}) \times 10^{-3}$	$(0.22^{+0.14}_{-0.13}) \times 10^{-3}$	$(0.16^{+0.06}_{-0.06}) \times 10^{-3}$	$(1.50^{+0.28}_{-0.28}) \times 10^{-3}$

$$\mathcal{B}(B^+ \rightarrow \bar{D}_2^{*0} \ell^+ \nu_\ell) = \begin{cases} (0.92^{+0.10+0.41}_{-0.10-0.35}) \times 10^{-2}, \\ (1.20^{+0.29+0.37}_{-0.29-0.47}) \times 10^{-2}, \end{cases}$$

$$R_{\bar{D}_2^*} \equiv \frac{\Gamma(B \rightarrow \bar{D}_2^* \tau^+ \nu_\tau)}{\Gamma(B \rightarrow \bar{D}_2^* \ell^+ \nu_\ell)}$$

$$R_{\bar{D}_2^*} = 0.040^{+0.002}_{-0.002} (0.035^{+0.004}_{-0.003}), \quad \text{type - II(type - I)}$$

## 总结与展望:

- CLF QM会出现协变性破坏和两种自治性问题：一种是由非零的类光矢量 $\omega$ 依赖项引起的，这部分贡献同时破坏了洛伦兹协变性；另一种是由于采用不同处理强子矩阵元方法导致的。
- 通过修改协变框架和光前框架的对应关系（type-II方案），即可同时解决自治性和协变性问题。
- 以上研究结果不仅能够改进CLF计算框架，而且可以为介子唯象学研究提供必要的非微扰输入。

感谢各位专家老师批评指正！