# Axion Haloscope Meets the $\vec{E}$ Field

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# Outline

- Resonance in a 'haloscope'
- Axio-electric current in an  $\overrightarrow{E}$  field
- $\vec{E}$  field as conversion medium
- $\vec{E}$  field as signal: capability study

# Axion / ALPs as DM

Axion as a fast oscillating field at the bottom of the its instanton potential  $V(\phi) \sim (\phi - \phi_0)^2$ behaves on ave. as matter-like:  $\rho(z) \sim (1+z)^3$ 

➤`Wave-like' DM candidates via misalignment mech.

Nearly monochromatic signal:  $\delta f/f \approx 10^{-6}$ .

For terrestrial labs, as a coherent wave:  

$$a(x,t) \approx a_0 \cos \left[ m_a \vec{v}_a \cdot \vec{x} - \left( m_a + \frac{m_a}{2} v_a^2 \right) t \right]$$
Local DM velocity

Can coherently convert into photon/EM fields via 'axion-like' interaction

$$\mathcal{L}_{a\gamma\gamma} = -g_{a\gamma}a\vec{E}\cdot\vec{B}$$



M. Turner, 83'

### Axion Haloscope:

A new  $f^{-1}$  frontier:

A resonant DM axion -> photon converter (P. Sikivie, 83')

- Primakoff Effect: a under a strong EM field
- DM in QCD axion theory predicts a microwave frequency band.
- High `Quality factor' given by DM energy dispersion

Search for high U(1)<sub>PQ</sub> scale physics at a low  $\sim \frac{\Lambda_{QCD}^2}{\Lambda_{PQ}}$  scale

• Tunable resonator to scan over a mass range



Cavity tuned to expected axion signal frequency

QCD axion dark matter: typically ~ O(50)  $\mu$ eV. General ALP(s): m<sub>a</sub>-  $f_a$  not restricted.  $m_a = 60-150 \ \mu eV$  (T. Hiramatsu, et.al. 2012')  $m_a = 26.5 \pm 3.4 \ \mu eV$  (Klaer, Moore, 2017')

### Cryogenic resonant EM cavity



### Haloscope with strong B field: sharpest limits, so far.



ADMX,HAYSTAC: achieved sensitivity to theoretical par. space (DFSZ / KSVZ models)

Recent players: CAPP/IBS (2020) QUAX-aγ (2019) CAST-RADES(2021) TASEH (2022)

\*Higher freq. detectors (10 GHz or higher?)

+ many others.

## Success with a High-Q

Key to cavity's achievements: high quality factor

For classical, see P. Sikivie, 84'

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$$R = g_{a\gamma\gamma}^2 \frac{\rho_a}{m_a^2} B_0^2 C_k V \cdot \boldsymbol{Q}$$

 $\mathbf{\Delta}$ 

 $Q \sim 10^6$  Provide both resonant  $a \rightarrow \gamma$  enhancement & bkg suppression

Thermal noise power: 
$$P_{Bkg} \sim 4k_B T \frac{m_a}{2\pi \cdot Q}$$

Quantum mechanically, interaction between a cavity-mode  $\vec{E}(x)$  and the plane wave:

$$H_{I} = -\int d^{3}x \mathcal{L}_{a\gamma\gamma}$$
$$= \left(g_{a\gamma\gamma} \frac{\sqrt{2\rho_{a}}}{m_{a}} B_{0} \int dx^{3} \hat{z} \cdot \vec{E}\right) \cos(\omega_{a} t)$$

## So at the QM level!

**Cavity's**  $|0\rangle \rightarrow |1\rangle$  rate is enhanced by the incident wave's Q – factor.

$$R = \left| \int_{0}^{t} \langle 1 | H_{I} | 0 \rangle e^{i(\omega_{k} - \omega_{a})t} dt \right|^{2}$$
$$= \left( g_{a\gamma\gamma} \frac{\sqrt{2\rho_{a}}}{m_{a}} B_{0} \int dx^{3} \hat{z} \cdot |\langle 1 | \vec{E} | 0 \rangle | \right)^{2} \delta(\omega_{k} - \omega_{a})$$
$$R \approx \frac{\pi}{2} g_{a\gamma\gamma}^{2} \frac{\rho_{a}}{m_{a}^{2}} B_{0}^{2} V \sum_{k} C_{k} \omega_{k} \delta(\omega_{k} - \omega_{a})$$

( for any DM axion wave's  $Q_a \leq Q_{cavity}$  )

Cavity's  $|0\rangle \rightarrow |1\rangle$  state transition rate is **indeed enhanced** by the **cavity quality factor that matches with the DM wave's**.

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\* This is consistent with classical oscillation calculations.

\* Opens up new methods based on single photons: dual-path HBT, antibunching...

### What about lower/higher m<sub>a</sub>?



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### W/O cavity? – `aQED' induction effects



### Axio-electric & axio-magnetic effective currents





 $\vec{E} \times \vec{k}_a$ 

 $j_a$  under *E* field: Depend on both E field and axion flow directions  $\vec{B} \cdot \partial_t a$ 

*j*<sub>a</sub> under *B* field:
 (anti)parallel with
 B field direction

### Magnetic signal from B field

➢'LC'-type designs: ADMX-SLIC, Abracadabra, DM-Radio, etc.



### Resonance without a cavity

High quality factor filtering is still essential for noncavity.

$$R = g_{a\gamma\gamma}^2 \frac{\rho_a}{m_a^2} B_0^2 C_k V Q$$

Popular solution: electronic (LC) circuit (P.Sikivie,13') resonance tuned to axion frequency (used in ADMX-SLIC, ABRACADABRA, BASE, etc.)







# $\vec{E}$ field or $\vec{B}$ field?

#### [As the medium]

Both induce effective currents
B field is (by Nature's choice) more effective in conversion rate:

\* 10 Tesla ~  $v_{DM}$ \*10<sup>13</sup> V/m \*  $j_a$  in *E* has velocity suppression.

- Strong solenoid *B* field: instabilities?
- E field: j<sub>a</sub> has directional dependance – 24 hr modulation
- E field: apparatus orientation dependance – bkg veto
- ➤ E field is cheaply maintained as a static field → less fluctuation

#### [As the signal]

Both E and B signals can be quite efficiently measured nowadays.
 (down to ~ single photon level)
 Typical E field signal:

- \* cavity's resonance modes.
- \* voltage differences.

≻Typical B field signal:

\* induced magnetic flux

Pick E or B that easily distinguishes
 from the experimental background.
 (Cavity: *E* signal from solenoid *B*)

### Magnetic signal from *E* field (broadband)



Pure inductance SC pickup coils: Low noise, high signal gain. Broad-band:

- \* not resonance enhanced
- \* compared signal magnitude to detector sensitivity.

- Cylindrical capacitor: between plate electrodes, the radial static E field, j<sub>a</sub> forms alternating loops.
- Modern SQUIDS sensitive to  $\delta B \sim 10^{-15} \, \mathrm{T}$
- No strong B field near pickup ring



Induction signal along cylinder axis:

$$B_{a} = \mu_{0} R j_{a} = g_{a\gamma} \bar{E}_{0} v \sqrt{2\rho_{CDM}} R \cos(\omega_{a} t)$$
  
=  $2.0 \times 10^{-7} T \left(\frac{g_{a\gamma}}{\text{GeV}^{-1}}\right) \left(\frac{\bar{E}_{0}}{\text{Gvolt/m}}\right) \left(\frac{R}{1\text{m}}\right)$   
×  $\cos(\omega_{a} t)$ 

SQUID sensitivity reach

$$\Delta B \sim 10^{-16} \text{ Tesla} \cdot \sqrt{\Delta f/\text{Hz}} + \Delta B_{\text{min}}$$

$$g_{a\gamma} = 1.7 \times 10^{-13} \text{GeV}^{-1} \left(\frac{1\text{m}}{R}\right) \left(\frac{1\text{GV/m}}{\bar{E}_0}\right) \left(\frac{10^4}{M_B}\right)$$
$$\cdot \sqrt{\frac{m_a}{10^{-5} \text{eV}} \frac{\delta v}{10^{-7}}}$$

Directionality: signal is daily modulated and depends on apparatus orientation

## Magnetic signal from *E* field (LC-res.)

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Cylindrical capacitor

+ LCR resonance enhancement



Low *T* on resistance parts for noise control.



- \* Originate from the search for the (dipole) radiating power from an alternating  $j_a$  loop
- \* Connect a LCR circuit to the coil pickup
- \* High *Q* resonant point requires relatively low resistance need SC parts.
- \* Fast resonance saturation (~  $f^{-1}$ )
- \* Loose winding to let in the induced signal

Pickup Inductance ~  $10\mu$ H per meter for mm–diameter wiring

SC: Lenient on pickup temperature: NbTi superconductor transition ~ 9.7K Allow for a sizeable pick coil. Axion-induced B field strength:

$$B_a = g_{a\gamma} E_0 v_{\rm DM} c_R \sqrt{2\rho_{\rm DM}} R_1$$
  
~  $2 \times 10^{-10} \mathrm{T} \cdot \left(\frac{g_{a\gamma}}{\mathrm{GeV}^{-1}}\right) \left(\frac{E_0}{10^7 \mathrm{V/m}}\right) \left(\frac{R_1}{0.1\mathrm{m}}\right)$ 

Signal current:

$$I_a = Q_c \cdot (\pi R_1^2 N_1 B_a L^{-1}) \cos \omega t$$

LCR capacitance (~ 0.1 GHz) $C = (2\pi f)^{-2}/L \sim 0.3 \text{pF} (\mu \text{H}/L) (0.1 \text{ GHz}/f)^2$  $Q_c = \omega_a L/R_s \text{ matches with axion's Q~10^6}.$ 

Maximal LCR dissipation power: (saturate to axion conversion)

$$P_{\rm dis.} = Q_c \cdot (N_1 \Phi_a/L)^2 \omega_a L/2$$

Low resistance @ LCR resonance:

 $R_s = \omega L/Q_c = 0.04\Omega \cdot (f/\text{GHz})$ 

Helps reduce thermal noise under cryogenic cond. ( $T_c \sim mK$ ) SC coils need a less stringent temperature (K) (yet its thermal noise should not exceed that in LCR)

> Assuming the LCR's noise (it's amplified) dominates total noise

$$P_n = k_B T_c \Delta f + k_B T_D \Delta f$$

$$SNR = \frac{(Q_c N_1 \Phi_a / L)^2 R_s}{2k_B T_c} \sqrt{\frac{t}{\Delta f}} ,$$
$$= \frac{Q_c (N_1 \cdot \pi R_1^2 B_a)^2}{2L k_B T_c} \sqrt{Q_c \cdot 2\pi \omega_a \cdot t}$$

$$g_{a\gamma} = \frac{\sqrt{\mathrm{SNR} \cdot 2N_1 L_{1,0} \cdot k_B T_c}}{(\pi R_1^3 N_1 E_0 v_a c_R \sqrt{2\rho_{\mathrm{DM}}}) \sqrt[4]{Q_c^3} 2\pi \omega_a t},$$
  

$$\approx 1.6 \times 10^{-12} \ \mathrm{GeV}^{-1} \left(\frac{R_1}{1 \ \mathrm{m}}\right)^{-3} \left(\frac{E_0}{\mathrm{MVm}^{-1}}\right)$$
  

$$\times \left(\frac{m_a}{10^{-6} \ \mathrm{eV}} \cdot \frac{t}{\mathrm{hr}}\right)^{-1/4}, \qquad \text{Better sens. at larger}$$
  
size, E-field, coil turns

#### Modest, medium & optimistic setups

Benchmark	$R_1(m)$	$N_1$	E(V/m)	$T_c(\mathrm{mK})$
А	0.2	5	$10^{6}$	10
В	1	10	$10^{7}$	1
С	3	20	$10^{9}$	1

Insulators:



# *E* field as the signal

Effective current j<sub>a</sub> (under a static B field) induces both time-variant mag. & ele. signals



 $B_{a}$  signal: magnetic flux at pickup loop

$$P_{sig.} = \frac{\langle \Phi^2 \rangle}{L} \omega$$



**E**<sub>a</sub> signal: charge buildup on surface(s)

$$P_{sig.} = \frac{\langle q^2 \rangle}{C} \omega$$
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# E Signal power strength

Is  $E_a$  signal a good way to catch the DM axion oscillation signal?

Experimental sizes/detectors/noises vary. Yet we can compare the axion conversion (signal) power.

Charge accumulation on plate surface: Pair of parallel plates form a capacitor: Use a LCR enhancement on current:

$$q = \int \vec{E} \cdot d\vec{A}_{1}$$
$$C \sim \pi R^{2}/d$$

$$I_a = Q_c \cdot q_0 \omega \cos(\omega t)$$

 $\eta(\omega) \equiv \frac{\int E_a \cdot d\vec{A}}{\int a_{acc} a \vec{B}_{acc} \cdot d\vec{A}}$ 



actual charge build up

theoretical upper limit:

E~g<sub>av</sub>\*a\*B

Geometric form factor:  $\eta = q/q_{max}$ (ratio of actual/max charge)

at `optimal' frequencies one would have  $\eta \sim O(1)$ 

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### As good as a cavity haloscope?

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LCR enhanced signal power:

 $P_{\rm sig}$ 

$$= \frac{(Q_c \omega q_0)^2}{2Q_c \omega C}$$
$$= Q_c \cdot \left(g_{a\gamma}^2 \eta(\omega)^2 \cdot \frac{\rho_{\rm DM}}{m_a} B_0^2\right) \left(\pi R^2 d\right)$$

At the maximal wavelength (half-wave cutoff)

$$V \sim \left(\frac{\lambda}{2}\right)^3 = (\pi/m_a)^3$$

 $P_{
m sig} = \mathcal{C}Q_c \cdot g_{a\gamma}^2 \cdot rac{
ho_{
m DM}}{m_a} B_0^2 \cdot V_{\gamma}$ 

 $\square$ 

A volume-dimension quantity: grasps the size of the region that axion field converts coherently to EM.

Form factor  $C = \eta^2 f_c^{-1}$ is around unity at cut-off

$$P_{
m sig} < \mathcal{O}(1) \cdot Q \cdot \pi^3 \cdot rac{g_{a\gamma}^2 
ho_{
m DM} B_0^2}{m_a^4}$$

(\* same signal power af for a cavity haloscope)

# Complication w geometric factors

### Long solenoid analytic solutions, see 1803.07755, 1812.05487



Simulated Ez distribution, 2206.13543

Ez isn't homogeneous; form factor depends on freq.

$$\eta(\omega) \approx \frac{1}{\pi R^2} \left| \int_0^R [\alpha(\omega) J_0(\omega r) - 1] \cdot 2\pi r \mathrm{d}r \right|$$
$$= \left| i\pi J_1(\omega R) H_1^+(\omega R) - 1 \right|$$

Evenly distributed ja generates a difference btw  $E_z(r \neq 0)$  and  $E_z(0)$ 





### Electric sensitivity (w LCR res.)

j<sub>a</sub> induced electric signal inside a solenoid Resonance-enhanced design <u>2206.13543</u> \* ready to go with most cryo. magnets.

\* Resonant ELEctric Axion Probe (ReLEAP)

\* Best sensitivity at larger frequency\* other geometric setups are possible

$$g_{a\gamma}^{\text{limit}} = \left(\frac{\text{SNR} \cdot 2k_B T_N}{\eta^2 f_c^{-1} R^2 d \ \rho_{\text{DM}} B_0^2 \sqrt{\Delta t}}\right)^{1/2} \left(\frac{m_a}{2\pi Q_c}\right)^{3/4}$$





### New haloscopes: open up $m_a < \mu eV$ range

