

## **Phase Noise and its Measurements**

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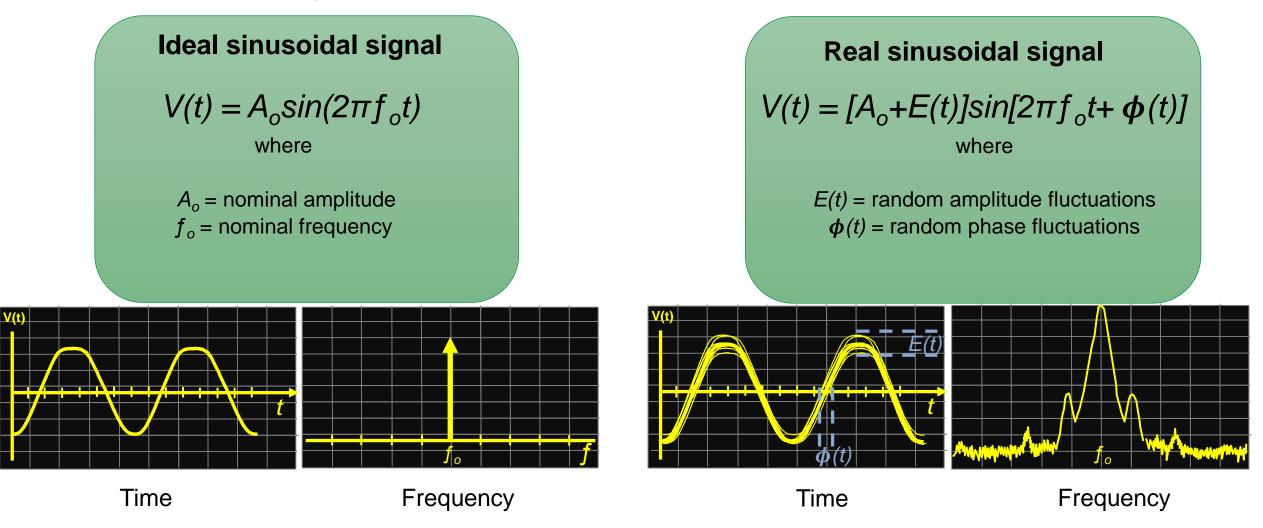
## Agenda

- Phase Noise Basics
  - What is Phase Noise  $\mathcal{L}(f)$  ?
  - Spectral Density of Phase Fluctuations  $S_{\phi}(f)$ 
    - Relations between SSB PN and RMS phase deviation
  - Jitter and Phase Noise
    - Relations between Jitter and RMS phase deviation
- Phase Noise Measurements
  - Direct-Spectrum Method
  - Phase Detector Method
  - Cross-correlation of 2-Channel Measurements
- Keysight Phase Noise Measurement Solutions



## What is Phase Noise?

Ideal versus real-world signals



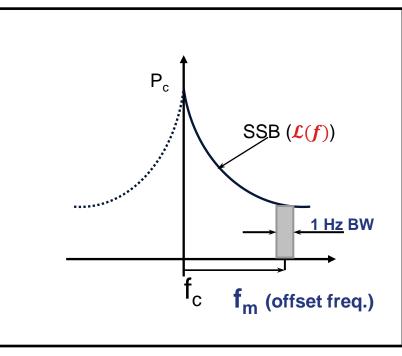
**KEYSIGHT** 

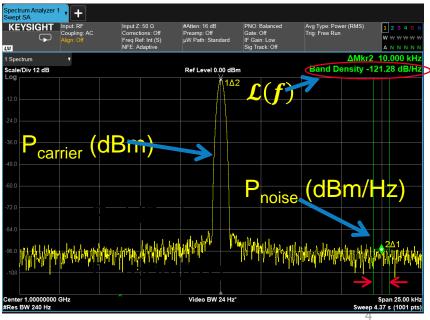
## What is Phase Noise?

How to define phase noise and its measurements

- Phase noise is the phase fluctuation of an oscillator, produced by random noise modulation on its main carrier signal.
- In frequency domain where phase noise is simply noise sidebands or skirt around "ideal" delta function from sinusoidal oscillator, which is symmetrical in magnitude around center frequency, so we can measure a single noise sideband (SSB)
- Three elements:
  - Offset frequency (fm) from carrier frequency (fc)
  - Power spectral density, in 1 Hz BW
  - PSD relative to carrier power in dBc

$$\mathcal{L}(f) = \frac{P_{SSB}}{P_c} \left(\frac{\mathrm{dBc}}{Hz}\right)$$





## **Spectral Density of Phase Fluctuations**

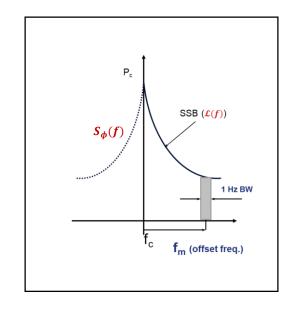
Mean-square Phase Deviation & Phase Noise

• If we can measure phase deviation  $(\Delta \phi)$ , we can convert mean-square phase deviation measurement (i.e.,  $\phi_{RMS}^2$ ) into a spectral density by dividing by the noise bandwidth and normalizing it to 1 Hz BW:

**Spectral Density of Phase Fluctuations:**  $S_{\phi}(f) = \phi_{RMS}^2(\frac{1}{BW})(\frac{rad^2}{Hz})$ 

• In case of small angle PM (where  $m = \beta = \phi_{pk} \le 0.2 rad$ ), which like we mentioned above in the case of small noise modulates the carrier with small angle deviation in the phase noise situation:

$$\frac{P_{SSB}}{P_c} = (\frac{1}{2}\phi_{pk})^2 = \frac{1}{4}(\sqrt{2}\phi_{RMS})^2 = \frac{1}{2}\phi_{RMS}^2 (rad^2)$$

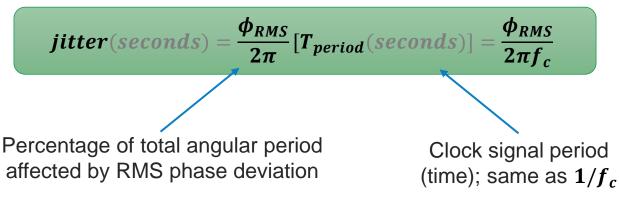


$$\phi_{RMS}(rad) = \sqrt{2 \int_{f_{start}}^{f_{stop}} \mathcal{L}(f) df}$$

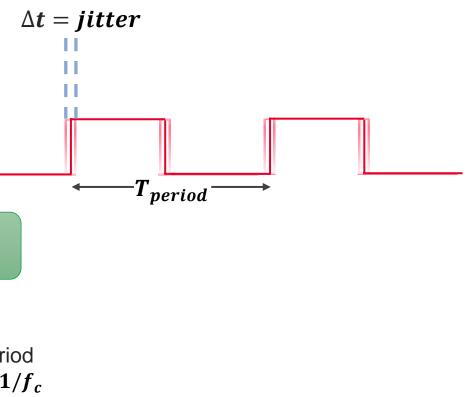
## **Jitter and Phase Noise**

**Jitter definition** 

- Time-domain RMS phase deviation is called jitter
- Those concerned about jitter frequently deal with clock signals, which are usually the measurements of square wave-type signals rather than sinusoids
- The following relates RMS phase deviation to jitter:



\*  $f_c$  is the clock frequency and when viewed in the frequency domain, is equal to the spacing between the spectral lines



## **Jitter and Phase Noise**

Measurement Principles Using a Real-time Oscilloscope

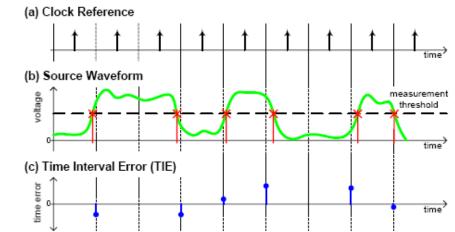
A time interval error (TIE) or Jitter measurement on an oscilloscope will produce a time series of the absolute time error of each edge relative to the ideal clock. To convert to phase (radians), the error is simply multiplied by 2πf<sub>c</sub> where f<sub>c</sub> is the clock carrier frequency:

 $\varphi = 2\pi \cdot TIE(t) \cdot f_c$ 

 A Time Interval Error (TIE) trend can be transformed to frequency domain with an FFT to give something called a Jitter Spectrum. Most modern oscilloscopes have this capability built in or as an

option:







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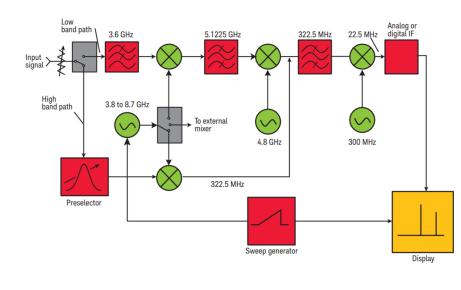
## **Measuring Phase Noise in Frequency Domain**

### **Direct-Spectrum Method**

• As mentioned earlier, we use spectrum analyzer to measure the SSB PN:

$$\mathcal{L}(f) = \frac{P_{SSB}}{P_c} \left(\frac{\mathrm{dBc}}{Hz}\right)$$

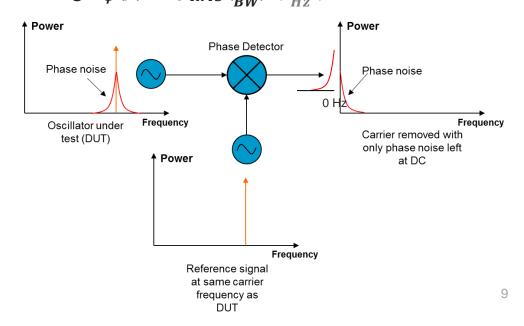
- It is far less sensitive than carrier-removal method because of spectrum analyzer's limitations.
  - Can not separate AM Noise
  - Has LO PN, preamp noise, ADC noise, etc.



## Phase Detector Method

(Carrier-removal method)

- Has increased sensitivity obtained by nulling carrier & then amplifying & measuring phase noise of resulting baseband signal with high-gain, low noise figure amplifiers
- It uses a phase detector to convert phase fluctuation into voltage of noise. We are measuring  $S_{\phi}(f) = \phi_{RMS}^2(\frac{1}{RW}) (\frac{rad^2}{H_T})$



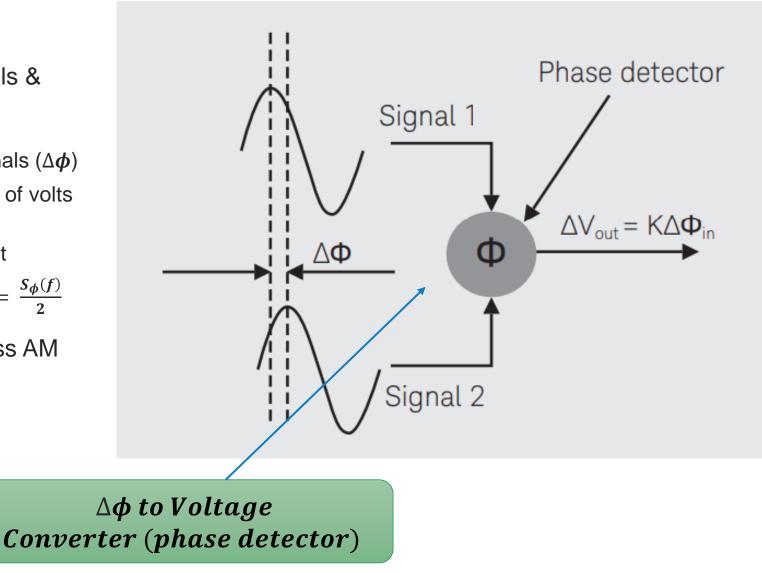
## **Phase Detector Techniques**

#### **Carrier-removal method**

- Phase detector takes two input signals & compares phase
  - Output of phase detector is DC voltage proportional to delta phase of input signals ( $\Delta \phi$ )
  - Constant of proportionality, K, has units of volts per radian (V/rad) & must be measured
  - When we got the  $\Delta \phi(t)$ , we FFT it to get

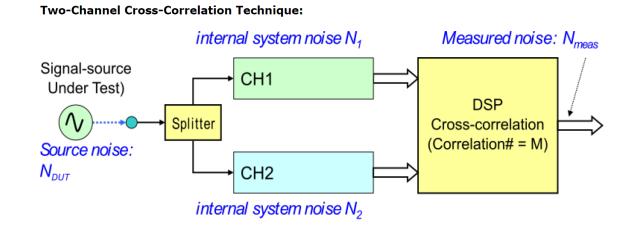
$$S_{\phi}(f) = \phi_{RMS}^2(\frac{1}{BW}) \left(\frac{rad^2}{Hz}\right) \text{ and } \mathcal{L}(f) \left(\frac{1}{Hz}\right) = \frac{S_{\phi}(f)}{2}$$

Phase detectors also tend to suppress AM noise



## **Cross-Correlation Technique**

- We can use two phase detectors to further improve phase noise floor (i.e., sensitivity)
- Two channels are uncorrelated so remove noise from references & system components through computational process.
- DUT signal is common to both channels so is perfectly correlated in both channels & kept as measurement result
- The two-channel cross-correlation technique achieves superior measurement sensitivity without requiring exceptional performance of the hardware components.
- However, the measurement speed suffers when increasing the number of computational correlations.



$$N_{meas} = N_{DUT} + (N_1 + N_2) / \sqrt{M}$$
 Assuming N<sub>1</sub> and N<sub>2</sub> are uncorrelated.

M (number of correlation)	10	100	1,000	10,000
Noise reduction on $(N_1+N_2)$	-5dB	-10dB	-15dB	-20dB

DUT noises through each channel are coherent and are not affected by the cross-correlation, whereas the internal noises generated by each channel are incoherent and are diminished by the cross-correlation operation at the rate of  $M^{1/2}$  (M being the number of correlations). This can be expressed as:

$$N_{meas} = N_{DUT} + (N_1 + N_2) / \sqrt{M}$$

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## **Keysight Phase Noise Solution Portfolio**



#### N5511A Phase Noise Test System (PNTS)

Fast and flexible noise measurement at the limit of physics (kT = -177 dBm/Hz)

- Absolute / residual / AM / baseband / pulse / transient
- 50 kHz to 3.0 / 26.5 / 40 GHz
- 0.01 Hz to 160 MHz offset frequency
- Cross correlation
- E5500 replacement (100% code compatible)
- External mixer support for mmWave measurements



Legacy SSA (E5052B) + Downconverter (E5053A)

Feb'24 Release



Building on 35 years of phase noise experience, Keysight solutions provide excellent performance and are economically tailored to fit your needs.

#### E505xA Signal Source Analyzer (SSA-X)

Everything you need for signal source analysis

- Absolute / residual / 2-port VNA (S-parameters) / AM / baseband / pulse / transient / SA / Clock jitter
- 1 MHz to 8 / 26.5 / 44 / 54 GHz
- >54 GHz with external mixers (sub-THz)
- 1 mHz to > 1 GHz offset frequency
- Cross correlation



#### **X-series Signal Analyzers**

N9068 Phase Noise Measurement Application

- Absolute / residual / AM / baseband / pulse / transient
- Frequency range, offset range and performance depends on X-series model

#### **PNA/PNA-X Network Analyzers**

S9303xxB Phase Noise Application

- Absolute / residual / AM / baseband / pulse / transient
- 10 MHz to 70 / 125 GHz
- 0.1 Hz to 10 MHz offset frequency

#### Infinium / MXR / UXR Oscilloscopes

D90x0JITA Jitter, Vertical and Phase Noise Analysis

- Absolute / residual / AM / baseband / pulse / transient
- Frequency range, offset range and performance depends
  on oscilloscope model
- Cross correlation
- · Best for measurements on digital signals, such as clocks

Ease of Use www.keysight.com/find/phasenoise



# Thank you