





# Some usually overlooked aspects in radiative and morphological modelling of pulsar wind nebulae



# Starting easy: $L_{sd}/D^2$ is not (in general) a good estimator of detection likelihood



#### Spin-down does not tell the whole story An example



**E Story MULTIMESSENGER ASTROPHYSICS** OSMIC RAYS - COMPACT OBJECTS - RELATIVISTIC ENVIRONMENTS THE INSTITUTE OF SPACE SCIENCES (ICE, CSIC) SINCE 2006 These are PWN spectra from pulsars with the same

- spin-down evolution,
- spin-down power  $(1.7 \times 10^{37} \text{ erg s}^{-1})$
- magnetic fraction,
- injection spectrum,
- photon background parameters than Crab,

but two different characteristic ages of 1500 and 8000 years.

Thus, today, B field and PWN size (which depend on evolution) are different and even if the high energy particles have limited life, they are subject to different losses producing different PWN SEDs.

Detectability estimations based on spin-down power (or spin-down power/ $D^2$ ) are naive; history counts.

#### Crab is not so energetically special

#### Table from Torres et al. 2014

**MULTIMESSENGER ASTROPHYSICS** COSMIC RAYS - COMPACT OBJECTS - RELATIVISTIC ENVIRONMENTS

Pulsars in the ATNF catalog with known period P, and period derivative P, and less than 10000 years of characteristic age (7). The first few columns are taken from ATNF data. The column "TeV Obs.?" answers whether the pulsar has been observed in TeV range, and, if so, by which telescope (noting H for H.E.S., M for MAGIC, and V for VERITAS). The column "TeV source" indicates whether there has been a detection of a PWN or in general a TeV source spatially co-located with the pulsar. This information comes from published literature. The last three columns represent, respectively, the age of Crab (assuming today's braking index) at which it would have the same characteristic age than the corresponding pulsar  $(T_t^{Crub})$ , the Crab's spin-down power at that age  $(L_{sd}^{Crub}(T_t^{Crub}))$ , and the spin-down power of the pulsar in terms of percentage of  $L_{sd}^{Crub}(T_t^{Crub})$ , which we refer to as CFP (Crab fractional power). Sources noted with  $\dagger$  are magnetars, which low rotational power is not expected to contubut significantly to the corresponding TeV sources (marked in red). Names of the TeV sources shown in blue are the ones studied in this work.

| Name<br>J                                                                                                       | P<br>(s) | <i>₽</i><br>(s s <sup>−1</sup> ) | D<br>(kpc) | τ<br>(yr) | B <sub>d</sub><br>(G)  | $L_{sd}$<br>(erg s <sup>-1</sup> ) | $L_{sd}/D^2$<br>(erg s <sup>-1</sup> kpc <sup>-2</sup> ) | TeV<br>Obs.? | TeV<br>source            | $T_{\tau}^{Crab}$<br>(yr) | $L_{sd}^{Crab}(T_{\tau}^{Crab})$<br>(erg s <sup>-1</sup> ) | CFP<br>(%) |
|-----------------------------------------------------------------------------------------------------------------|----------|----------------------------------|------------|-----------|------------------------|------------------------------------|----------------------------------------------------------|--------------|--------------------------|---------------------------|------------------------------------------------------------|------------|
| 1808_2024                                                                                                       | 75550    | 5.49 × 10-10                     | 13.0       | 218       | $2.0 \times 10^{15}$   | $5.0 \times 10^{34}$               | $3.0 \times 10^{32}$                                     | н            | 11800-104/C11 0+0 08     |                           | (0/                                                        |            |
| 1846-0258                                                                                                       | 0.3265   | $7.10 \times 10^{-12}$           | 5.8        | 728       | $4.9 \times 10^{13}$   | $8.1 \times 10^{36}$               | $2.0 \times 10^{35}$                                     | н            | Kes 75                   | 238                       | $1.6 \times 10^{39}$                                       | 0.5        |
| 1907+0919†                                                                                                      | 51983    | $9.20 \times 10^{-11}$           | 5.0        | 895       | $7.0 \times 10^{14}$   | $2.6 \times 10^{34}$               | 2.4 × 10                                                 | н            | 11908+063/C401-0.89      | 459                       | $1.0 \times 10^{39}$                                       | 0.003      |
| 1714-3810†                                                                                                      | 3 8249   | $5.20 \times 10^{-11}$           |            | 1030      | $4.8 \times 10^{14}$   | $4.1 \times 10^{34}$               |                                                          | н            | 11718-385/CTB37A         | 638                       | $7.2 \times 10^{38}$                                       | 0.005      |
| 0534+2200                                                                                                       | 0.0334   | $4.21 \times 10^{-13}$           | 2.0        | 1258      | 3.8 × 10 <sup>12</sup> | $4.5 \times 10^{38}$               | 1.2 × 10 <sup>38</sup>                                   | HMV          | Crab nebula              | 940                       | $4.5 \times 10^{38}$                                       | 100        |
| 1550-5418                                                                                                       | 2.0698   | $2.32 \times 10^{-11}$           | 9.7        | 1410      | $2.2 \times 10^{14}$   | $1.0 \times 10^{35}$               | $1.1 \times 10^{33}$                                     | Н            |                          | 1141                      | $3.5 \times 10^{38}$                                       | 0.03       |
| 1513-5908                                                                                                       | 0.1512   | $1.53 \times 10^{-12}$           | 4.4        | 1560      | $1.5 \times 10^{13}$   | $1.7 \times 10^{37}$               | $9.0 \times 10^{35}$                                     | Н            | J1514–281/MSH 15–52      | 1340                      | $2.8 \times 10^{38}$                                       | 6          |
| 1119-6127                                                                                                       | 0.4079   | $4.02 \times 10^{-12}$           | 8.4        | 1610      | $4.1 \times 10^{13}$   | $2.3 \times 10^{30}$               | $3.3 \times 10^{34}$                                     | Н            | J1119-6127/G292.1-0.54   | 1406                      | $2.6 \times 10^{38}$                                       | 0.9        |
| 0540-6919                                                                                                       | 0.0504   | $4.79 \times 10^{-13}$           | 53.7       | 1670      | $5.0 \times 10^{12}$   | $1.5 \times 10^{38}$               | 5.1 × 10 <sup>34</sup>                                   | Н            |                          | 1486                      | $2.4 \times 10^{38}$                                       | 63         |
| 0525-6607                                                                                                       | 8.0470   | $6.50 \times 10^{-11}$           |            | 1960      | $7.3 \times 10^{14}$   | $4.9 \times 10^{33}$               |                                                          |              |                          | 1871                      | $1.6 \times 10^{38}$                                       | 0.003      |
| 1048-5937                                                                                                       | 6.4520   | $3.81 \times 10^{-11}$           | 9.0        | 2680      | $5.0 \times 10^{14}$   | $5.6 \times 10^{33}$               | $6.9 \times 10^{31}$                                     | Н            |                          | 2825                      | $7.8 \times 10^{37}$                                       | 0.007      |
| 1124-5916                                                                                                       | 0.1354   | $7.52 \times 10^{-13}$           | 5.0        | 2850      | $1.0 \times 10^{13}$   | $1.2 \times 10^{37}$               | $4.8 \times 10^{35}$                                     | н            |                          | 3050                      | $6.8 \times 10^{37}$                                       | 18         |
| 1930+1852                                                                                                       | 0.1368   | $7.50 \times 10^{-13}$           | 7.0        | 2890      | $1.0 \times 10^{13}$   | $1.2 \times 10^{37}$               | $2.4 \times 10^{35}$                                     | v            | J1930+188/G54.1+0.3      | 3103                      | $6.6 \times 10^{37}$                                       | 18         |
| 1622-4950                                                                                                       | 4.3261   | $1.70 \times 10^{-11}$           | 9.1        | 4030      | $2.7 \times 10^{14}$   | $8.3 \times 10^{33}$               | 9.9 × 10 <sup>31</sup>                                   | Н            |                          | 4614                      | $3.0 \times 10^{37}$                                       | 0.03       |
| 1841-0456                                                                                                       | 11.7789  | $4.47 \times 10^{-11}$           | 9.6        | 4180      | $7.3 \times 10^{14}$   | $1.1 \times 10^{33}$               | $1.2 \times 10^{31}$                                     | Н            |                          | 4813                      | $2.8 \times 10^{37}$                                       | 0.004      |
| 1023-5746                                                                                                       | 0.1115   | $3.84 \times 10^{-13}$           | 8.0        | 4600      | $6.6 \times 10^{12}$   | $1.1 \times 10^{37}$               | $1.7 \times 10^{35}$                                     | Н            | J1023+575                | 5370                      | $2.2 \times 10^{37}$                                       | 50         |
| 1833-1034                                                                                                       | 0.0618   | $2.02 \times 10^{-13}$           | 4.10       | 4850      | $3.6 \times 10^{12}$   | $3.4 \times 10^{37}$               | $2.0 \times 10^{36}$                                     | Н            | J1833-105/G21.5-0.9      | 5701                      | $2.0 \times 10^{37}$                                       | 170        |
| 1838-0537                                                                                                       | 0.1457   | $4.72 \times 10^{-13}$           |            | 4890      | $8.4 \times 10^{12}$   | $6.0 \times 10^{36}$               |                                                          | Н            | J1841-055                | 5754                      | $1.9 \times 10^{37}$                                       | 32         |
| 0537-6910                                                                                                       | 0.0161   | $5.18 \times 10^{-14}$           | 53.7       | 4930      | $9.2 \times 10^{11}$   | $4.9 \times 10^{38}$               | $1.7 \times 10^{35}$                                     | Н            | N157B (in the LMC)       | 5807                      | $1.9 \times 10^{37}$                                       | 2579       |
| 1834-0845†                                                                                                      | 2.4823   | $7.96 \times 10^{-12}$           |            | 4940      | $1.4 \times 10^{14}$   | $2.1 \times 10^{34}$               |                                                          | Н            | J1834-087/W41            | 5820                      | $1.9 \times 10^{37}$                                       | 0.1        |
| 1747-2809                                                                                                       | 0.0521   | $1.55 \times 10^{-13}$           | 17.5       | 5310      | $2.9 \times 10^{12}$   | 4.3 × 10 <sup>37</sup>             | 1.4 × 10 <sup>35</sup>                                   | H            | J1747-281/C0.9+0.1       | 6311                      | $1.6 \times 10^{37}$                                       | 269        |
| 0205+6449                                                                                                       | 0.0657   | $1.94 \times 10^{-13}$           | 3.2        | 5370      | $3.6 \times 10^{12}$   | $2.7 \times 10^{37}$               | $2.6 \times 10^{36}$                                     | MV           |                          | 6390                      | $1.6 \times 10^{37}$                                       | 169        |
| 181                                                                                                             | ~ 1      |                                  |            |           |                        |                                    |                                                          |              |                          |                           | 1037                                                       | 400        |
| <sup>010</sup> Whe                                                                                              | en Cra   | b has ~64                        | 100 ve     | ears, 11  | twould                 | have the                           | e same ch                                                | aracte       | ristic                   |                           | 1030                                                       | 0.02       |
| 135                                                                                                             |          |                                  |            |           |                        |                                    |                                                          | 41           |                          |                           |                                                            |            |
| <sup>161</sup> age than that 3C58 has today, and its luminosity would be almost a factor of 2 lower. $10^{161}$ |          |                                  |            |           |                        |                                    |                                                          | 22           |                          |                           |                                                            |            |
|                                                                                                                 |          |                                  |            |           |                        |                                    | 0.9                                                      |              |                          |                           |                                                            |            |
| 1617-5055                                                                                                       | 0.0693   | $1.35 \times 10^{-13}$           | 6.4        | 8130      | 3.1 ×10 <sup>12</sup>  | $1.6 \times 10^{37}$               | 3.8 × 10 <sup>35</sup>                                   | Н            | J1616–508                | 10048                     | 5.9 × 10 <sup>30</sup>                                     | 271        |
| 2022+3842                                                                                                       | 0.0242   | $4.32 \times 10^{-14}$           | 10.0       | 8910      | $1.0 \times 10^{12}$   | $1.2 \times 10^{-38}$              | $1.2 \times 10^{30}$                                     |              |                          | 11082                     | $4.8 \times 10^{30}$                                       | 2500       |
| 1708-4009†                                                                                                      | 11.0013  | $1.93 \times 10^{-11}$           | 3.8        | 9010      | $4.7 \times 10^{14}$   | $5.7 \times 10^{32}$               | $4.0 \times 10^{31}$                                     | Н            | J1708-443/G343.1-2.69    | 11215                     | $4.7 \times 10^{36}$                                       | 0.01       |
| 1745-2900†                                                                                                      | 3.76356  | $6.5 \times 10^{-12}$            | 8.0        | 9170      | 1.6 ×10 <sup>14</sup>  | 4.8 × 10 <sup>33</sup>             | 7.5 × 10 <sup>31</sup>                                   | HM           | (in the Galactic Center) | 11427                     | 4.4 × 10 <sup>36</sup>                                     | 0.99       |

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#### The PWN phases



#### Plot from Olmi & Bucciantini 2023



Free expansion proceeds until the PWN reaches the reverse shock (RS).

After that time, the shell experiences a strong deceleration, which in many cases leads to a compression of the PWN.

When due to compression the PWN internal pressure becomes high enough, the PWN bounces and re-expands again.

Reverberation (compression bounce) last for a few kyrs or less, and happens relatively shortly after birth - at the end of free expansion.

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## Then, knowing the shock positions is key



#### Knowing the shock positions

Bandiera, Bucciantini, Martin, Olmi & DFT, MNRAS 2021

Truelove and McKee (1999, TM99) solutions were used in all models when incorporating the dynamics in radiative models of pulsar wind nebulae (PWNe).

Through a mix of analytical limits, semi-analytical formulae, and fits to numerical simulations, TM99 provides a series of approximations to describe the evolution of the SNR during its different stages.

TM99 has become a widely used reference for the time evolution of the FS and **RS**.

$$R_{\rm ch} = M_{\rm ej}^{1/3} \rho_0^{-1/3}$$
  

$$\simeq 7.4 \, {\rm pc} \left(\frac{M_{\rm ej}}{10 \,{\rm M}_\odot}\right)^{1/3} \left(\frac{m_{\rm p} n_0}{g \, {\rm cm}^{-3}}\right)^{-1/3},$$
  

$$t_{\rm ch} = E_{\rm sn}^{-1/2} M_{\rm ej}^{5/6} \rho_0^{-1/3}$$
  

$$\simeq 3241 \, {\rm yr} \left(\frac{E_{\rm sn}}{10^{51} \, {\rm erg}}\right)^{-1/2} \left(\frac{M_{\rm ej}}{10 \,{\rm M}_\odot}\right)^{5/6} \left(\frac{m_{\rm p} n_0}{g \, {\rm cm}^{-3}}\right)^{-1/3}$$
  

$$V_{\rm ch} = \frac{E_{\rm sn}^{1/2}}{M_{\rm ej}^{1/2}} \simeq 2240 \, {\rm km \, s}^{-1} \left(\frac{E_{\rm sn}}{10^{51} \, {\rm erg}}\right)^{1/2} \left(\frac{M_{\rm ej}}{10 \,{\rm M}_\odot}\right)^{-1/2}$$

Typical models assume a **core** with a shallow radial profile  $\propto r^{-\delta}$  (with  $\delta < 3$ ), plus an **envelope** with a steep power-law one  $\propto r^{-\omega}$ (with  $\omega > 5$ ),

$$\rho_{\rm ej}(r,t) = \begin{cases} A \left( v_{\rm t}/r \right)^{\delta}/t^{3-\delta}, & \text{if } r < v_{\rm t}t, \\ A \left( v_{\rm t}/r \right)^{\omega} t^{\omega-3}, & \text{if } v_{\rm t}t \le r < R_{\rm RS} \end{cases} \quad \begin{bmatrix} v_{\rm t} = \sqrt{\frac{2(5-\delta)(\omega-5)}{(3-\delta)(\omega-3)}} \frac{E_{\rm sn}}{M_{\rm ej}} \\ A = \frac{(5-\delta)(\omega-5)}{2\pi(\omega-\delta)} \frac{E_{\rm sn}}{v_{\rm t}^5}. \end{bmatrix}$$

 $\delta(\omega-3)$   $M_{\rm ei}$ 

- δ)





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#### PWN behavior very sensitive to RS location

Bandiera, Bucciantini, Martin, Olmi & Torres, MNRAS 2020, 2021



Even small variations of the position and velocity of the RS at the onset of reverberation may produce large variations in the final compression factor of the PWN.



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. Direct comparison of our formulae for the characteristic trajectories RS, CD, FS with those of TM99 (only valid for  $\delta = 0$ ).

| Truelove J. | K., McKee C. F., 1999, ApJS, 120, 299 (TM99)                                                                                                                                                                                                                               | ω                   | t                                 | SUPPORTING FORMULAS                                                                                                                                                                                        |
|-------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------|-----------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
|             | $1.83t(1 + 3.26t^{3/2})^{-2/3}$                                                                                                                                                                                                                                            | $\omega = 0$        | $t < t_{ct}$                      | $t_{\rm rt} = (2\omega/[5(\omega-3)]\hat{A}^{-\omega/(\omega-3)}\sqrt{2.026})^{2\omega/[3(\omega-5)]}$                                                                                                     |
|             | $t(0.779 - 0.106t - 0.533\ln t)$                                                                                                                                                                                                                                           | $\omega = 0$        | $t \ge t_{\rm st}$                | $\hat{A} = \{27l_{\text{ed}}^{(\omega-2)}/[4\pi\omega(\omega-3)\phi_{\text{ed}}](10[\omega-5]/[3(\omega-3)])^{(\omega-3)/2}\}^{1/\omega}$ $l_{\text{ed}} = \{1.39, 1.26, 1.21, 1.19, 1.17, 1.15, 1.14\}^*$ |
|             | $\hat{A}t^{(\omega-3)/\omega}$                                                                                                                                                                                                                                             | $5 < \omega \le 14$ | $t \leq t_{\rm core}$             | $t_{\rm core} = [27/(4\pi\omega[\omega-3]l_{ed}^2\phi_{ed})]^{1/3}\sqrt{3(\omega-3)/(10[\omega-5])}$                                                                                                       |
| RS          | $t\left(\hat{A}t_{ m core}^{(\omega-3)/\omega}/l_{ m ed} ight)$                                                                                                                                                                                                            | $5 < \omega \le 14$ | $t_{\rm core} < t \le t_{\rm st}$ | $\phi_{\rm ed} = \{0.39, 0.47, 0.52, 0.55, 0.57, 0.6, 0.62\}^*$                                                                                                                                            |
|             | $t \left[ (\hat{A}t_{\text{core}}^{(\omega-3)/\omega}) / (l_{\text{ed}}t_{\text{core}}) - a_{\text{core}}(t - t_{\text{core}}) + -(3/(l_{\text{ed}}\omega)\hat{A}t_{\text{core}}^{[(\omega-3)/\omega]-1} - a_{\text{core}}t_{\text{core}}) \ln(t/t_{\text{core}}) \right]$ | $5 < \omega \le 14$ | $t > t_{\rm st}$                  | $a_{\text{core}} = \{0.112, 0.116, 0.139, 0.162, 0.192, 0.251, 0.277\}^*$                                                                                                                                  |
| CD          | _                                                                                                                                                                                                                                                                          | -                   | _                                 | _                                                                                                                                                                                                          |
|             | $2.01t(1+1.72t^{3/2})^{-2/3}$                                                                                                                                                                                                                                              | $\omega = 0$        | $t < t_{st}$                      |                                                                                                                                                                                                            |
|             | $(1.42t - 0.254)^{2/5}$                                                                                                                                                                                                                                                    | $\omega = 0$        | $t \ge t_{ m st}$                 |                                                                                                                                                                                                            |
| FS          | $\hat{A}t^{(\omega-3)/\omega}$                                                                                                                                                                                                                                             | $5 < \omega \le 14$ | $t \leq t_{ m st}$                |                                                                                                                                                                                                            |
|             | $(\hat{A}t_{\rm st}^{(\omega-3)/\omega})^{5/2} + \sqrt{2.026}(t-t_{\rm st})^{2/5}$                                                                                                                                                                                         | $5 < \omega < 14$   | $t > t_{st}$                      |                                                                                                                                                                                                            |

Note that according to  $\omega$  (the power law index of the ejecta profile) the time and extent of the compression varies a lot.

Not monotonous, not linear



\*All the listed numerical values must be considered relative to the range  $\omega = \{6, 7, 8, 9, 10, 12, 14\}$ .



. Direct comparison of our formulae for the characteristic trajectories RS, CD, FS with those of TM99 (only valid for  $\delta = 0$ ).

| Truelove J. K | ., McKee C. F., 1999, ApJS, 120, 299 (TM99)                                                                                                                                                                                                                              | ω                   | t                                 | SUPPORTING FORMULAS                                                                                                                                                                                  |
|---------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------|-----------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
|               | $1.83t(1+3.26t^{3/2})^{-2/3}$                                                                                                                                                                                                                                            | $\omega = 0$        | $t < t_{\rm st}$                  | $t_{\rm st} = (2\omega/[5(\omega-3)]\hat{A}^{-\omega/(\omega-3)}\sqrt{2.026})^{2\omega/[3(\omega-5)]}$                                                                                               |
|               | $t(0.779 - 0.106t - 0.533\ln t)$                                                                                                                                                                                                                                         | $\omega = 0$        | $t \ge t_{\rm st}$                | $\hat{A} = \{27l_{\rm ed}^{(\omega-2)} / [4\pi\omega(\omega-3)\phi_{\rm ed}](10[\omega-5]/[3(\omega-3)])^{(\omega-3)/2}\}^{1/\omega} \\ l_{\rm ed} = \{1.39, 1.26, 1.21, 1.19, 1.17, 1.15, 1.14\}^*$ |
|               | $\hat{A}t^{(\omega-3)/\omega}$                                                                                                                                                                                                                                           | $5 < \omega \le 14$ | $t \leq t_{\rm core}$             | $t_{\rm core} = [27/(4\pi\omega[\omega - 3]l_{ed}^2\phi_{ed})]^{1/3}\sqrt{3(\omega - 3)/(10[\omega - 5])}$                                                                                           |
| RS            | $t\left(\hat{A}t_{\rm core}^{(\omega-3)/\omega}/l_{\rm ed}\right)$                                                                                                                                                                                                       | $5 < \omega \le 14$ | $t_{\rm core} < t \le t_{\rm st}$ | $\phi_{\rm ed} = \{0.39, 0.47, 0.52, 0.55, 0.57, 0.6, 0.62\}^*$                                                                                                                                      |
|               | $t \left[ (\hat{A}t_{\text{core}}^{(\omega-3)/\omega}) / (l_{\text{ed}}t_{\text{core}}) - a_{\text{core}}(t-t_{\text{core}}) + -(3/(l_{\text{ed}}\omega)\hat{A}t_{\text{core}}^{[(\omega-3)/\omega]-1} - a_{\text{core}}t_{\text{core}}) \ln(t/t_{\text{core}}) \right]$ | $5 < \omega \le 14$ | $t > t_{\rm st}$                  | $a_{\text{core}} = \{0.112, 0.116, 0.139, 0.162, 0.192, 0.251, 0.277\}^*$                                                                                                                            |
| CD            |                                                                                                                                                                                                                                                                          | _                   | —                                 | —                                                                                                                                                                                                    |
|               | $2.01t(1+1.72t^{3/2})^{-2/3}$                                                                                                                                                                                                                                            | $\omega = 0$        | $t < t_{\rm st}$                  |                                                                                                                                                                                                      |
|               | $(1.42t - 0.254)^{2/5}$                                                                                                                                                                                                                                                  | $\omega = 0$        | $t \ge t_{ m st}$                 |                                                                                                                                                                                                      |
| FS            | $\hat{A}t^{(\omega-3)/\omega}$                                                                                                                                                                                                                                           | $5 < \omega \le 14$ | $t \leq t_{\rm st}$               |                                                                                                                                                                                                      |
|               | $(\hat{A}t_{\rm st}^{(\omega-5)/\omega})^{5/2} + \sqrt{2.026(t-t_{\rm st})^{2/5}}$                                                                                                                                                                                       | $5 < \omega < 14$   | $t > t_{\rm st}$                  |                                                                                                                                                                                                      |

We did 1D Lagrangian simulations for a large number of PWN, with different energetics,  $\omega$  and  $\delta$  parameters, and different characteristic values of the system and directly measured the shock positions.

Then fitted with functions providing much better than 1% accuracy, and compared the results with TM99 solutions.

\*All the listed numerical values must be considered relative to the range  $\omega = \{6, 7, 8, 9, 10, 12, 14\}$ .



. Direct comparison of our formulae for the characteristic trajectories RS, CD, FS with those of TM99 (only valid for  $\delta = 0$ ).

| Truelove J.     | . K., McKee C. F., 1999, ApJS, 120, 299 (TM99)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | ω                        | t                                       | SUPPORTING FORMULAS                                                                                                                                                                                                                                                                                                                                                                |
|-----------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------|-----------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| -               | $1.83t(1+3.26t^{3/2})^{-2/3}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | $\omega = 0$             | $t < t_{\rm st}$                        | $t_{\rm st} = (2\omega/[5(\omega-3)]\hat{A}^{-\omega/(\omega-3)}\sqrt{2.026})^{2\omega/[3(\omega-5)]}$                                                                                                                                                                                                                                                                             |
|                 | $t(0.779 - 0.106t - 0.533\ln t)$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | $\omega = 0$             | $t \ge t_{\rm st}$                      | $\hat{A} = \{27l_{ed}^{(\omega-2)}/[4\pi\omega(\omega-3)\phi_{ed}](10[\omega-5]/[3(\omega-3)])^{(\omega-3)/2}\}^{1/\omega}$ $l_{ed} = \{1.39, \ 1.26, \ 1.21, \ 1.19, \ 1.17, \ 1.15, \ 1.14\}^*$                                                                                                                                                                                  |
|                 | $\hat{A}t^{(\omega-3)/\omega}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | $5 < \omega \le 14$      | $t \leq t_{\rm core}$                   | $t_{\rm core} = [27/(4\pi\omega[\omega-3]l_{ed}^2\phi_{ed})]^{1/3}\sqrt{3(\omega-3)/(10[\omega-5])}$                                                                                                                                                                                                                                                                               |
| RS              | $t\left(\hat{A}t_{\rm core}^{(\omega-3)/\omega}/l_{\rm ed} ight)$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | $5 < \omega \le 14$      | $t_{\rm core} < t \le t_{\rm st}$       | $\phi_{\rm ed} = \{0.39, 0.47, 0.52, 0.55, 0.57, 0.6, 0.62\}^*$                                                                                                                                                                                                                                                                                                                    |
|                 | $t \left[ (\hat{A}t_{\text{core}}^{(\omega-3)/\omega}) / (l_{\text{ed}}t_{\text{core}}) - a_{\text{core}}(t-t_{\text{core}}) + (l_{\text{core}}) + (l_$ |                          |                                         |                                                                                                                                                                                                                                                                                                                                                                                    |
|                 | $-(3/(l_{\rm ed}\omega)\hat{A}t_{\rm core}^{\lfloor(\omega-3)/\omega\rfloor-1}-a_{\rm core}t_{\rm core})\ln(t/t_{\rm core})\Big]$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | $5 < \omega \le 14$      | $t > t_{st}$                            | $a_{\text{core}} = \{0.112, 0.116, 0.139, 0.162, 0.192, 0.251, 0.277\}^*$                                                                                                                                                                                                                                                                                                          |
| CD              | _                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | -                        | —                                       | _                                                                                                                                                                                                                                                                                                                                                                                  |
|                 | $2.01t(1+1.72t^{3/2})^{-2/3}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | $\omega = 0$             | $t < t_{st}$                            |                                                                                                                                                                                                                                                                                                                                                                                    |
|                 | $(1.42t - 0.254)^{2/5}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | $\omega = 0$             | $t \ge t_{\rm st}$                      |                                                                                                                                                                                                                                                                                                                                                                                    |
| FS              | $\hat{A}t^{(\omega-3)/\omega}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | $5 < \omega \le 14$      | $t \leq t_{ m st}$                      |                                                                                                                                                                                                                                                                                                                                                                                    |
|                 | $(\hat{A}t_{\rm st}^{(\omega-3)/\omega})^{5/2} + \sqrt{2.026}(t-t_{\rm st})^{2/5}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | $5 < \omega < 14$        | $t > t_{\rm st}$                        |                                                                                                                                                                                                                                                                                                                                                                                    |
| Bandiera,       | Bucciantini, Martin, Olmi & DFT, MNRAS 2021                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | ω                        | t                                       | SUPPORTING FORMULAS<br>$x = t/t_{imple}(\omega, \delta)$                                                                                                                                                                                                                                                                                                                           |
| RS              | $\mathcal{R}(x) 	imes \mathcal{F}(\omega)$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | $\omega \ge 6$           | $t_{\rm core} < t \le t_{\rm implo}$    | $\begin{aligned} t_{\text{implo}} &= 2.399 + \{(0.1006\Omega)^2 + \\ + [(-0.06494 + 0.7063\Omega)/(1 + 1/\Omega^2)]^2\}^{0.5} \\ \Omega &= 1/(\omega - 5) \end{aligned}$<br>$\mathcal{R}(x) &= [x^{1.5551}(1 - x)^{0.68236}] [0.01961 + 0.5093x + 0.1874x^2]^{-1} \\ \mathcal{F}(\omega) &= 1 + \{0.02171[\Omega/0.3338 - 1]\}\{1 + [\Omega/0.3338]^{-2.778}\}^{-1} \end{aligned}$ |
| CD              | $\tilde{a}(\omega)t^{(\omega-3)/\omega}/[1+b_{	ext{CD}}(\omega)t^{c_{	ext{CD}}(\omega)}]$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | $\omega \ge 6$           | $t_{\rm core,CD} < t \le t_{\rm implo}$ | $\tilde{a}(\omega) = (1.141 + 1.806\omega)(7.636 + \omega)^{-1}$<br>$b_{\rm CD} = -1.051 - 0.1961\tilde{a}(\omega)$<br>$c_{\rm CD} = -(5.561 + 0.6741\omega)(\omega - 4.826+)^{-1}$                                                                                                                                                                                                |
| FS              | $\xi_0(t+1.94)^{2/5}/[1+0.672(1/t)+0.00373(1/t)^2]$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | $\omega \ge 6$           | $t > t_{\rm core,FS}$                   | $\xi_0 = 1.15169$ (from the standard Sedov solution)                                                                                                                                                                                                                                                                                                                               |
| *All the listed | numerical values must be considered relative to the range $\omega = \{0, 0\}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 6, 7, 8, 9, 10, 12, 14}. |                                         | Valid for all w larger than 6, all values of $\delta$ .                                                                                                                                                                                                                                                                                                                            |



The relative variation between models is typically of order of 10 to 30% per cent. Impact of a 10% change in the compression is large and cannot be neglected!

Even larger relative differences closer to the implosion time, of the order of 100 per cent!





#### Age is not a good estimation of the PWN phase



# Characteristic age of the SNR, not of the pulsar, as a marker of PWN stage

•  $t_{ch} = E_{sn}^{-1/2} M_{ej}^{5/6} \rho^{-1/3}$ ,

- provides the typical time scale for the evolution of the SNR.
- Large variations of the implosion time only appear when drastically changing the structure of the ejecta core, being ~2.4 times the characteristic time of the SNR in many cases.
  - ~2.4  $t_{ch}$  represents a theoretical maximum for the time the PWN can remain in free-expansion, as for typical PSR energy injection, the duration of the free-expansion phase we found to be no longer than about half of the implosion time.
- This clarifies why the age of the pulsar may have no direct appeal in defining the phases, as for instance changes in the ejecta mass have an almost linear dependence on  $t_{ch}$ .







# Reverberation has its complexities, disregarding/ignoring them leads to unreliable estimates



PWN 1-zone-models: literature either ignores reverberation at all, or treats it in simplified ways

In the latter case, there are 3 main assumptions:

- 1. The PWN is a **uniform** (one-zone) bubble of particles and field
- 2. The shell at the PWN boundary is **thin** ( $R_{shell} \sim R_{pwn}$ ;  $\Delta R_{shell} \ll R_{pwn}$ )
- 3. The pressure outside the PWN is equal to or a constant fraction of the pressure at the FS in the Sedov solution

$$P_{\rm Sedov} = 0.1592 \left(\frac{t}{t_{\rm ch}}\right)^{-6/5} \frac{\rho_{\rm ISM} E_{\rm sn}}{M_{\rm ej}}$$

[Gelfand et al. 2009 - Fang & Zhang 2010 - Tanaka & Takahara 2010 - Martin et al. 2012 - Tanaka & Takahara 2013 - Vorster et al. 2013 - Torres et al. 2013-2019 - Gelfand et al. 2015-2017 - Bandiera et al. 2021 - Fiori et al. 2022]

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#### The thin-shell is not thin in reverberation

Bandiera, Bucciantini, Martin, Olmi & DFT, MNRAS 2023a



- For a scaled radius ranging between 1 and 1.02, the profiles are related to the density profile inside the shell.
- They are superimposed, meaning that the density preserves its profile, apart from a slight decrease with time of the shell relative width.
- The sharp break in the profiles (reflecting a density jump) indicates the position of the shock at the outer boundary of the shell;
- The scaled mass higher than unity means that the real swept-up mass is that within the outer boundary of the shell, rather than within R<sub>pwn</sub>(t).
- After  $t_{\text{beg,rev}}$  the mass within the shell, now scaled with the swept-up mass at  $t_{\text{beg,rev}}$ , does not change with time: note the constancy of the vertical coordinate of the break
- The relative width of the shell increases with time, partly reflecting its physical broadening, and partly as a consequence PWN decreasing of its size.

This figure justifies the assumption of a **fixed shell mass during reverberation** and that when the PWN has been compressed, the **needed conditions for treating the shell as a thin-shell are no longer valid.** 

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#### The thin-shell is not thin in reverberation

Bandiera, Bucciantini, Martin, Olmi & DFT, MNRAS 2023a



For  $t < t_{beg,rev}$  the shell boundaries are very close each other, meaning that the thin-shell approximation is well satisfied.

But especially close to the maximum compression, the shell boundaries separate, and the combination of a higher shell thickness and a smaller shell size implies that a thin-shell approach is no longer justified.

During the reverberation phase, the outer edge of the shell is defined by the mass collected before  $t_{beg,rev}$  and one may clearly see that the shell becomes thicker, and as the PWN starts to contract the shell inflates progressively

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ASTROP

#### The outer pressure is not a constant nor Sedov like



Bandiera, Bucciantini, Martin, Olmi & DFT, MNRAS 2023a



#### Modeling middle age systems



Bandiera, Bucciantini, Martin, Olmi & DFT, MNRAS 2023b

#### TIDE+L

Hybrid radiative – HD model

- Radiative model until reverberation, with dynamics incoporated
  - then use this stage just before reveberation as input for a...
- Lagrangian model thereafter,
  - But with radiation incorporated
- Correctly converges to the Lagrangian model all along when no losses are considered.
- Correctly matches at the interface between the two approaches.
- Relative fast for reasonable computational grid (few minutes per PWN).
- Can go to whatever age in a safe manner.

(State-of-the-art Radiative PWN code: correct shock positions, radiative, full ODEs, time-energy-dependent, Lagrangian after Reverberation)

Of course, recall, all of this is 3D in nature. Still an approximation!



#### How to model middle age systems? Spectra





# Significant spectral variability as time goes by

Superefficiency

Population analysis finally possible (ongoing research)





# PWN morphology very strongly depends on the environment, and the latter is not mainly determined by the ISM



#### HD/MHD models of PWN





#### Previously: hydrodynamical models of PWN





Temim et al. (2015, 2017a,b, 2022)

Pulsar wind that is moving inside supernova ejecta and/or in a density gradient in the ISM

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#### HD/MHD models of PWN: so far without stellar wind 🖕





#### Stellar history + wind





The interaction of the pulsar wind and SNR with the CSM generated by the supergiant and eventual phases of WR Or blue star has been essentially been neglected.



Runaway massive star die in their own bow shock

The circumstellar medium of massive (runaway) star is a governing parameter in the morphology, distribution and mixing of materials in plerion

#### MHD num simulations of PWN/SNR w/CSM

D. Meyer, & D. F. Torres, Material mixing in pulsar wind nebulae of massive runaway stars. <u>A&A 2024</u>
 D. Meyer, Z. Meliani & D. F. Torres, Pulsar wind nebulae meeting the circumstellar medium of their progenitors <u>A&A 2024</u>
 D. Meyer et al. Supernova remnants of red supergiants: From barrels to loops, <u>A&A 2024</u>

D. Meyer et al. On the plerionic rectangular supernova remnants of static progenitors, A&A 2024





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## Concluding remarks



#### Conclusions



- Don't forget that it's more complicated that finding a pulsar with a high E<sub>sd.</sub> Crab is young, but we all were.
- Go beyond Truelove and McKee, we now have well-behaving formulae mimicking directly HD simulations.
- Mixed one-zone/HD models solve the problems introduced by the pure thin-shell approximation in the treatment of the reverberation phase: they catch the global behavior and estimate the PWN compression
- First relatively consistent numerical passage through reverberation for a radiative/HD model (TIDE-L)
- Some PWNe can reduce themselves in size by more than two orders of magnitude, at least in the 1D representation.
  - Such systems with large compression CF ≫ 100 are possible but rare, limited to the extremes of the known population of PWNe.
  - But reductions in size by a factor of a few-10x are quite common.
  - Superefficiency appears often at UV/optical, and less often in X-rays
- Understanding and correctly modelling reverberation is critical for population studies (e.g., how many PWN will we see in future surveys at different frequencies) and individual predictions / description of all middle-age systems
- The circumstellar (not just the interstellar) medium affects it all, opening a whole lot of new complexities into the problem.









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#### MHD num simulations of PWN/SNR w/CSM

D. Meyer, & D. F. Torres, Material mixing in pulsar wind nebulae of massive runaway stars. <u>A&A 2024</u> D. Meyer, Z. Meliani & D. F. Torres, Pulsar wind nebulae meeting the circumstellar medium of their progenitors <u>A&A 2024</u>

D. Meyer et al. Supernova remnants of red supergiants: From barrels to loops, A&A 2024

D. Meyer et al. On the plerionic rectangular supernova remnants of static progenitors, A&A 2024







#### **PWN in magnetised ISM**





The magnetisation of the ISM changes the circumstellar medium of massive stars, and, consequently, their supernova remnant and PWN



## Progenitor's stellar wind history induces asymmetric reverberation in PWN





#### Wind nebulae of SN progenitors





The interaction of the pulsar wind and SNR with the CSM generated by the supergiant and eventual phases of WR Or blue star has been essentially been neglected so far.

Meyer, Meliani, Torres (2024)

