



Introduction of SRF Cavity System

Eiji Kako (KEK, Japan)

ASSCA2025 at IHEP
March 26, 2025'



1. Introduction
2. Fundamental of SRF Cavity
3. Overview of SRF Cavity System
4. Fabrication and Surface Preparation
5. Cavity Performances
6. Summary



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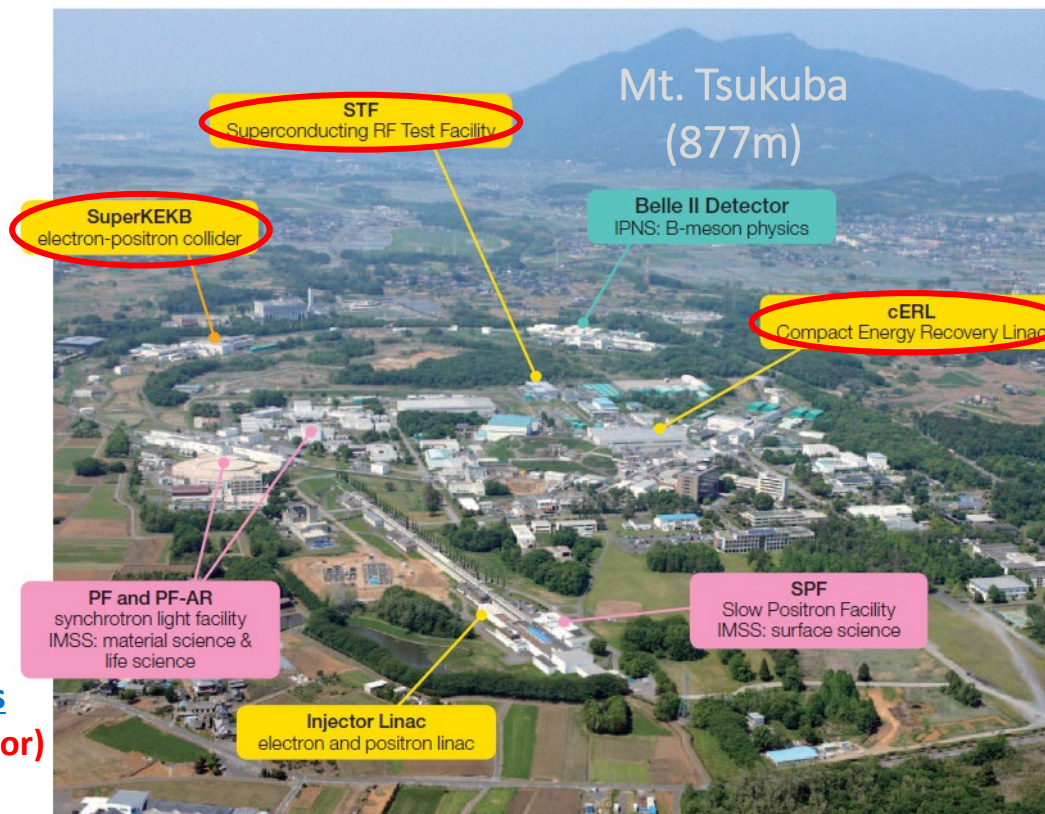


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High Energy Accelerator Research Organization

KEK



Tsukuba Campus
(Electron Accelerator)



Tokai Campus
(Proton Accelerator)

J-PARC

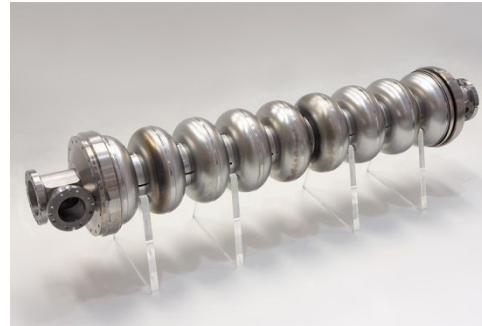


My life at KEK for 38 years.

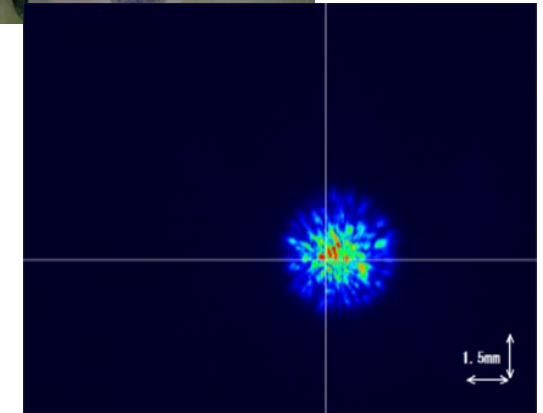
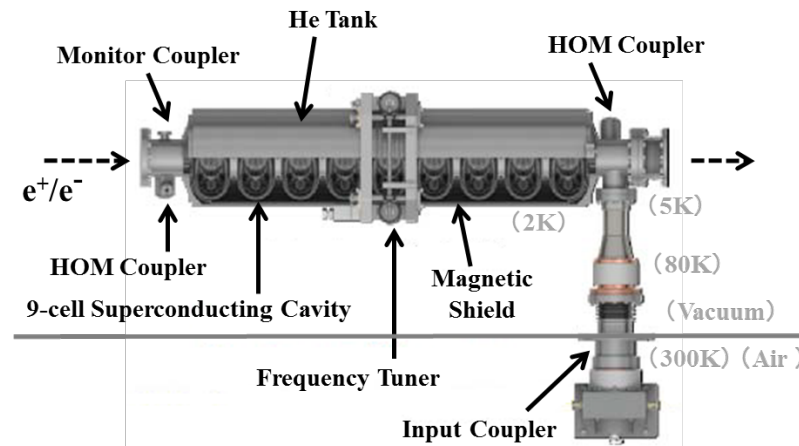
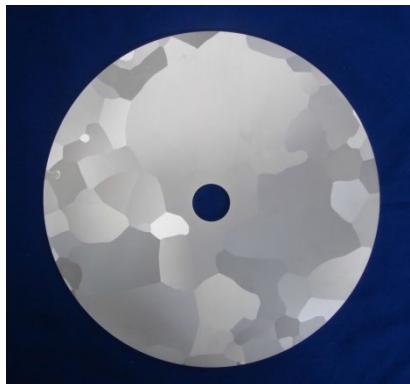
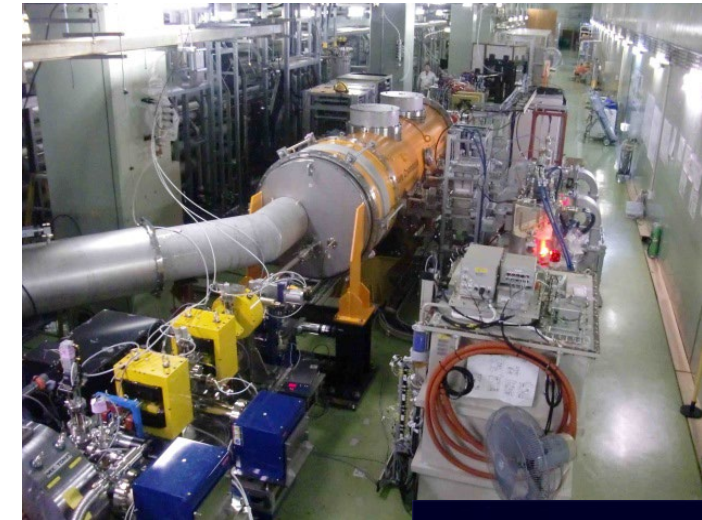
Superconducting RF (SRF) Cavity



Cavity



Cryomodule



Stable Beam Operation

Niobium Material



**Superconducting
RF cavity system**

Superconductivity
and material science

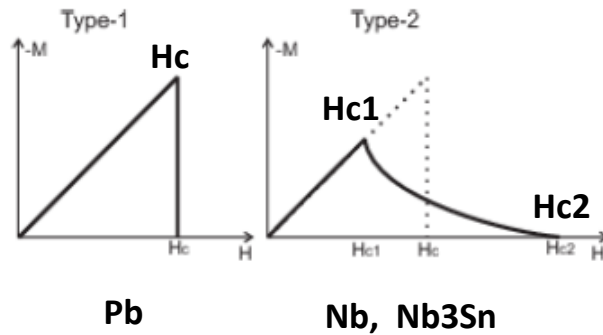
Ultra-high vacuum &
clean technology

RF technology

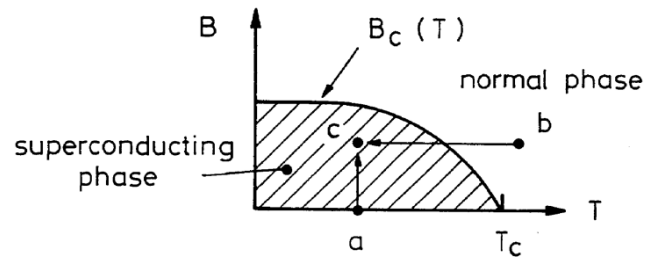
Cryogenic technology



Type-1, Type-2 Superconductor



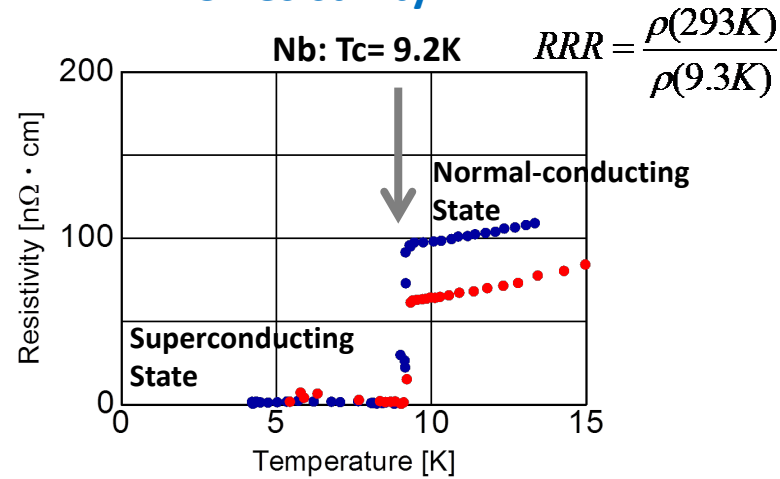
Phase diagram



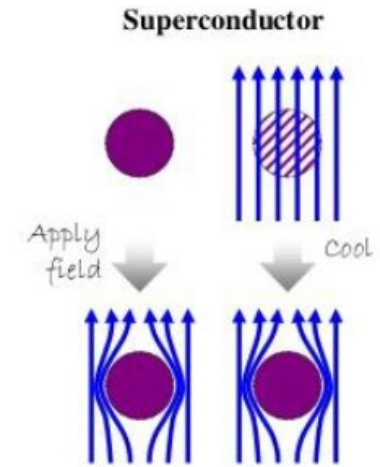
$$H_{c1}(T) = H_{c1}(0) \times (1 - (T/T_c)^2)$$

$$T < T_c/2$$

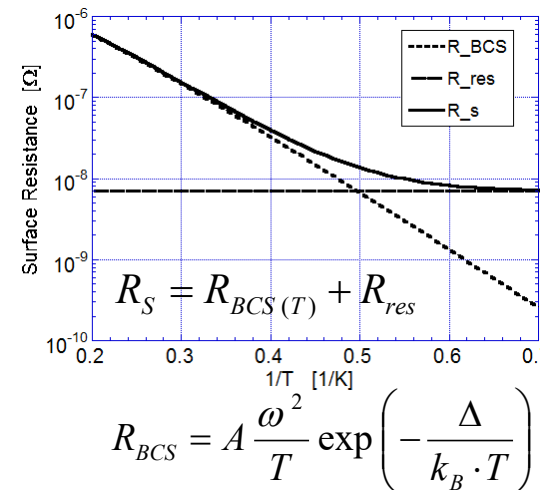
DC Resistivity



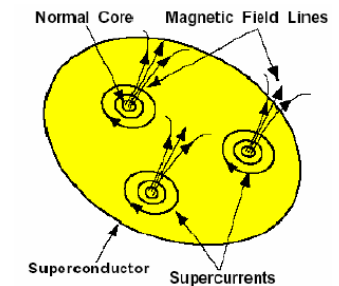
Meissner effect



RF Surface Resistance

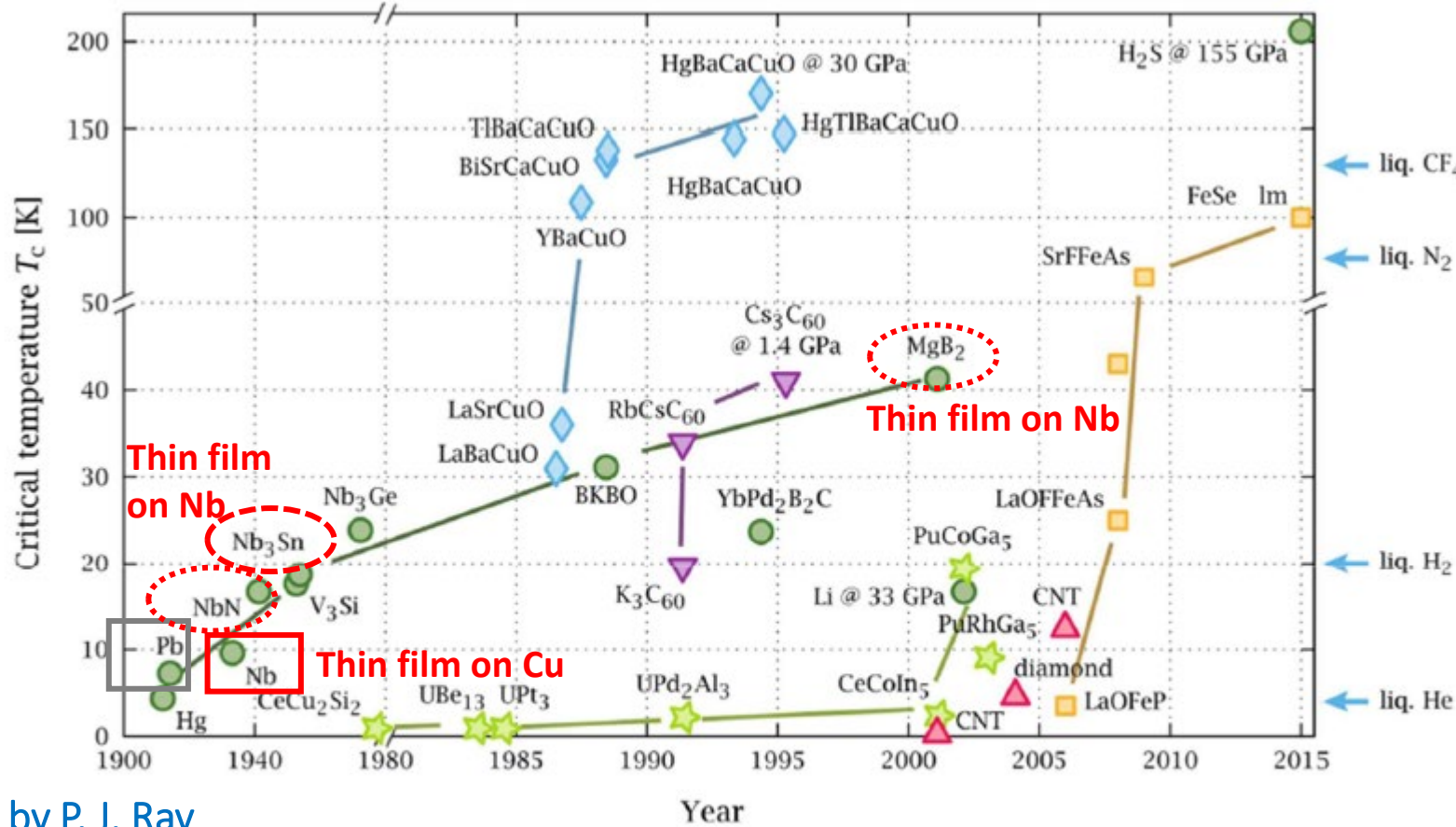


Flux trapping



$$R_{res} = 0.3 \sim 0.4 \text{ [n}\Omega / \text{mG]}$$

Critical Temperatures of Superconductors



by P. J. Ray

- BCS超伝導体
- ◆ 銅酸化物超伝導体
- 鉄系超伝導体
- ▼ フラーレン
- ★ 重い電子系

	T_c	$H_c(0)$	λ
Nb	9.2 K	0.20 T	40 nm
NbN	16.2 K	0.23 T	~350 nm
Nb ₃ Sn	18 K	0.54 T	~100 nm
MgB ₂	40 K	0.43 T	140 nm

Question (1)



What is the advantage using Niobium for SRF cavities?



What is the advantage using Niobium for SRF cavities?

- Suitable critical temperature (T_c) at 9.2 K
 - Cooling by liquid He: at 4.2 K and at 2.0 K
- Availability of high purity Niobium metal
 - Production by Electron Beam (EB) melting
- Better fabrication property from Niobium sheets
 - Forming by deep drawing and joining by EB welding



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Rest Energy of Particles



$$1 \text{ Joule} = 1 \text{ Nm} = 1 \text{ kgm}^2/\text{sec}^2$$

$$1 \text{ eV} = 1.6 \times 10^{-19} \text{ Joule}$$

$$c = 2.9979 \times 10^8 \text{ m/sec}$$

$$m_e = 0.9109 \times 10^{-27} \text{ g} ; \text{ mass of electron}$$

$$m_p = 1.6925 \times 10^{-24} \text{ g} ; \text{ mass of proton}$$

Rest Energy

$$E_e = m_e c^2 = 0.511 \text{ MeV}$$

$$E_p = m_p c^2 = 938 \text{ MeV}$$



Rest Energy $E_0 = m_0 c^2 \quad (v = 0)$

$(v > 0)$

$$E = \frac{m_0 c^2}{\sqrt{1 - (v/c)^2}} = \frac{m_0 c^2}{\sqrt{1 - \beta^2}} = m_0 \gamma c^2$$

Kinetic Energy $E_K = m_0 \gamma c^2 - m_0 c^2 = m_0 c^2 (\gamma - 1)$

$$\gamma = 1 / \sqrt{1 - \beta^2}$$

$$\beta = v/c$$

$$\beta \approx 1 \quad (v \approx c)$$

$$\beta < 0.5 \quad (v \ll c)$$

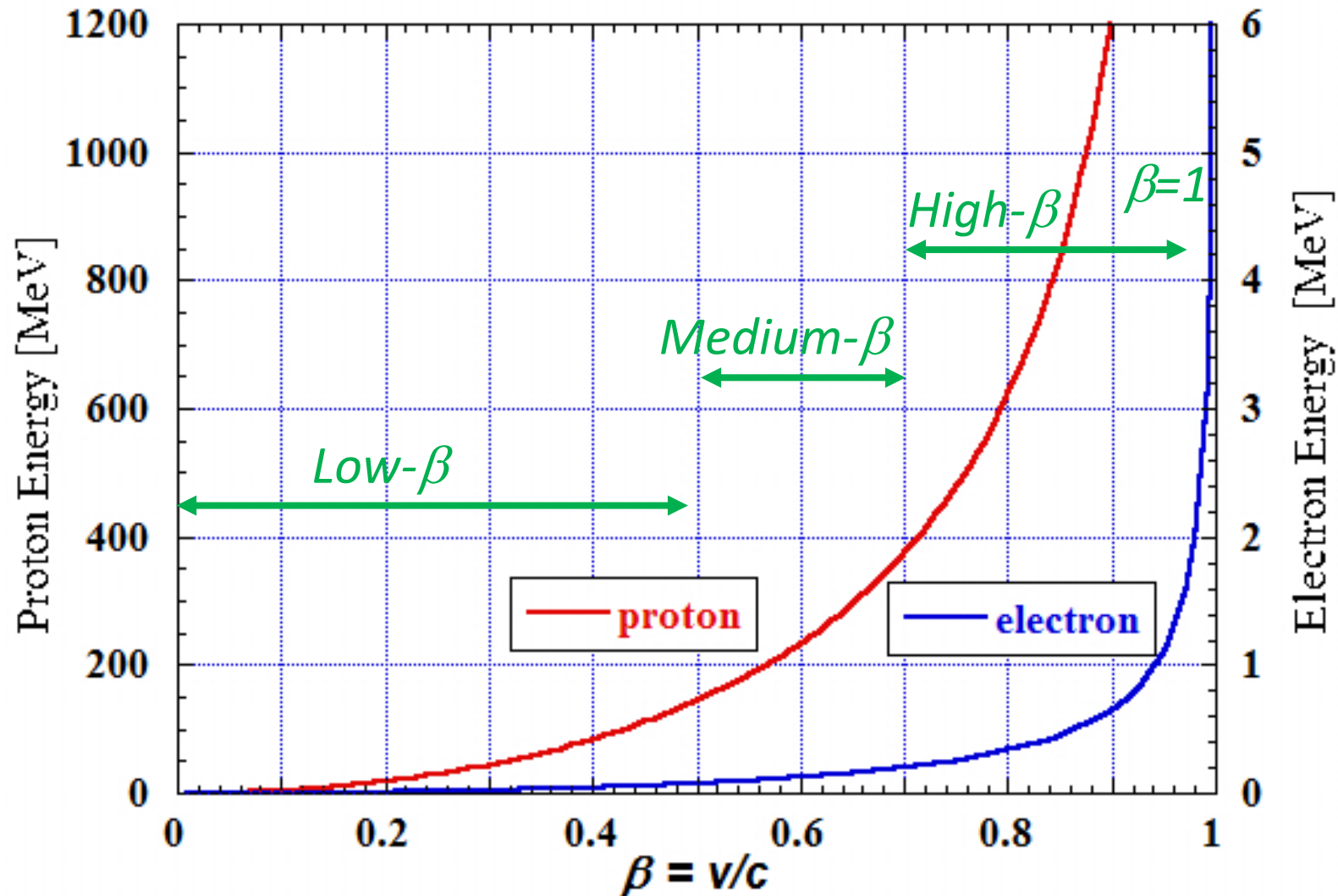
$$\beta \approx 0.5 \sim 0.7$$

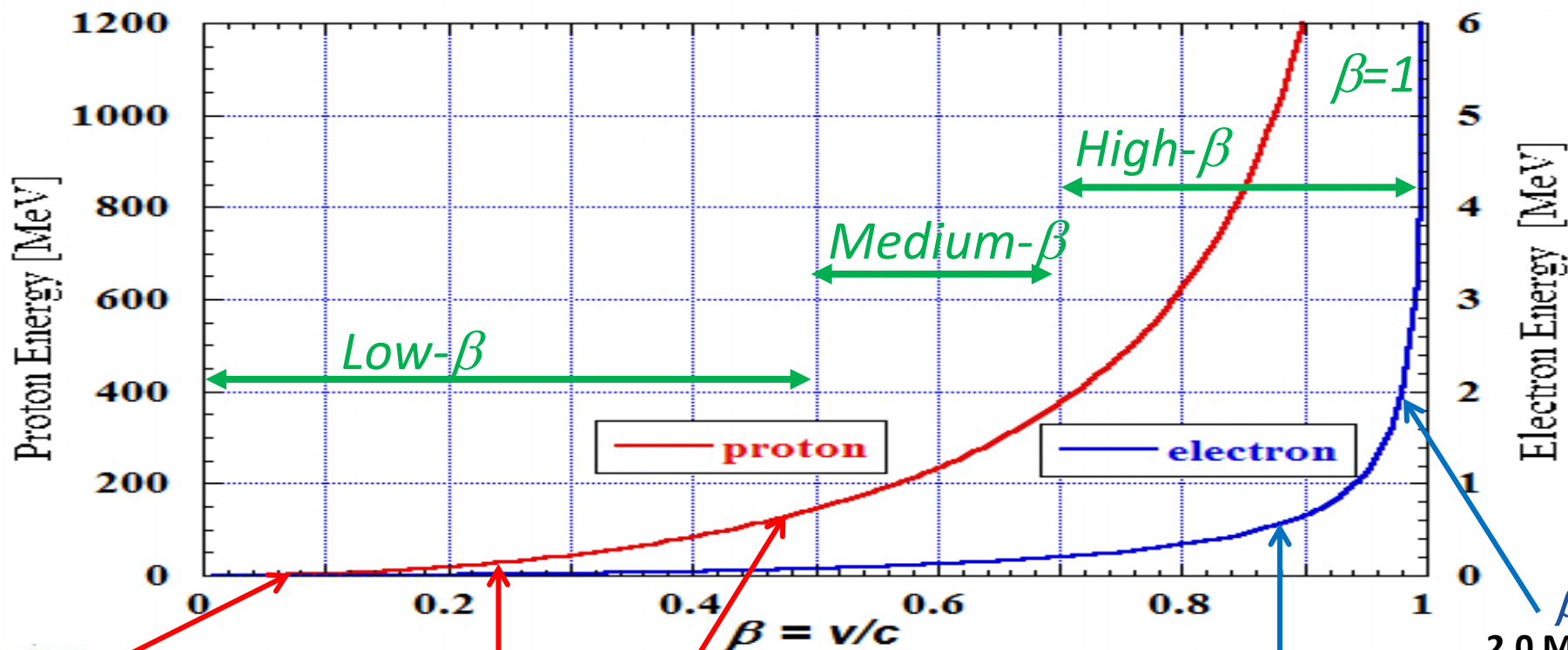
$$\beta > 0.7$$

Low- β

Medium- β

High- β





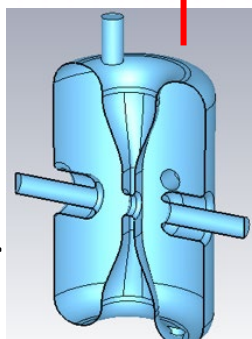
$\beta = 0.07$

QWR:
Quarter-wave Resonator



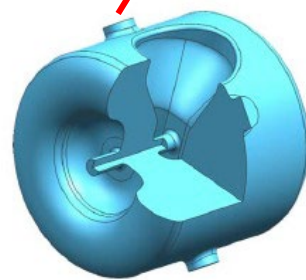
$\beta = 0.24$

HWR:
Half-wave Resonator



$\beta = 0.47$

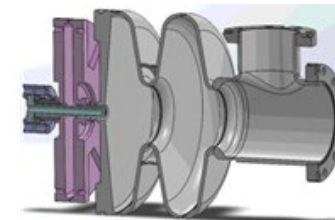
SSR:
Single-Spoke Resonator



$\beta = 0.88$

500 keV CW e-beam
500 kV DC-Gun

$\beta = 0.98$
2.0 MeV CW e-beam

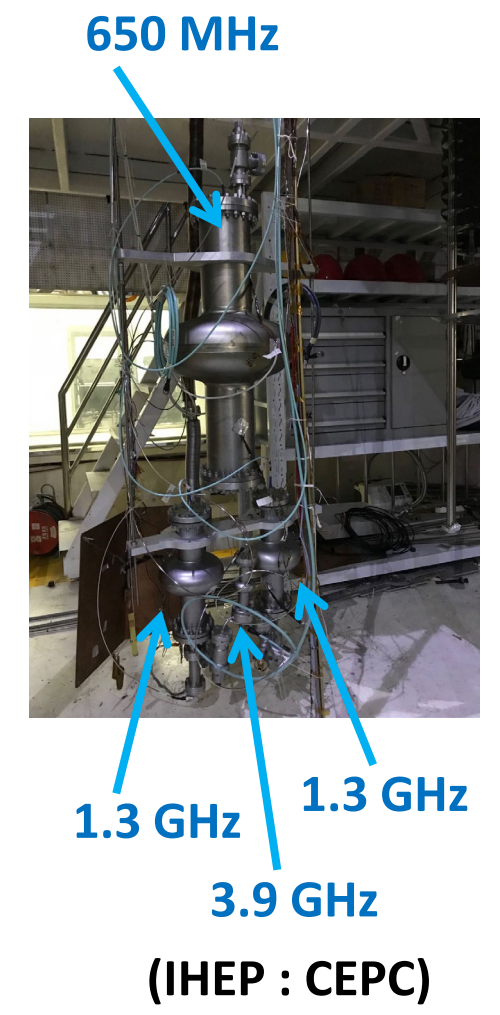
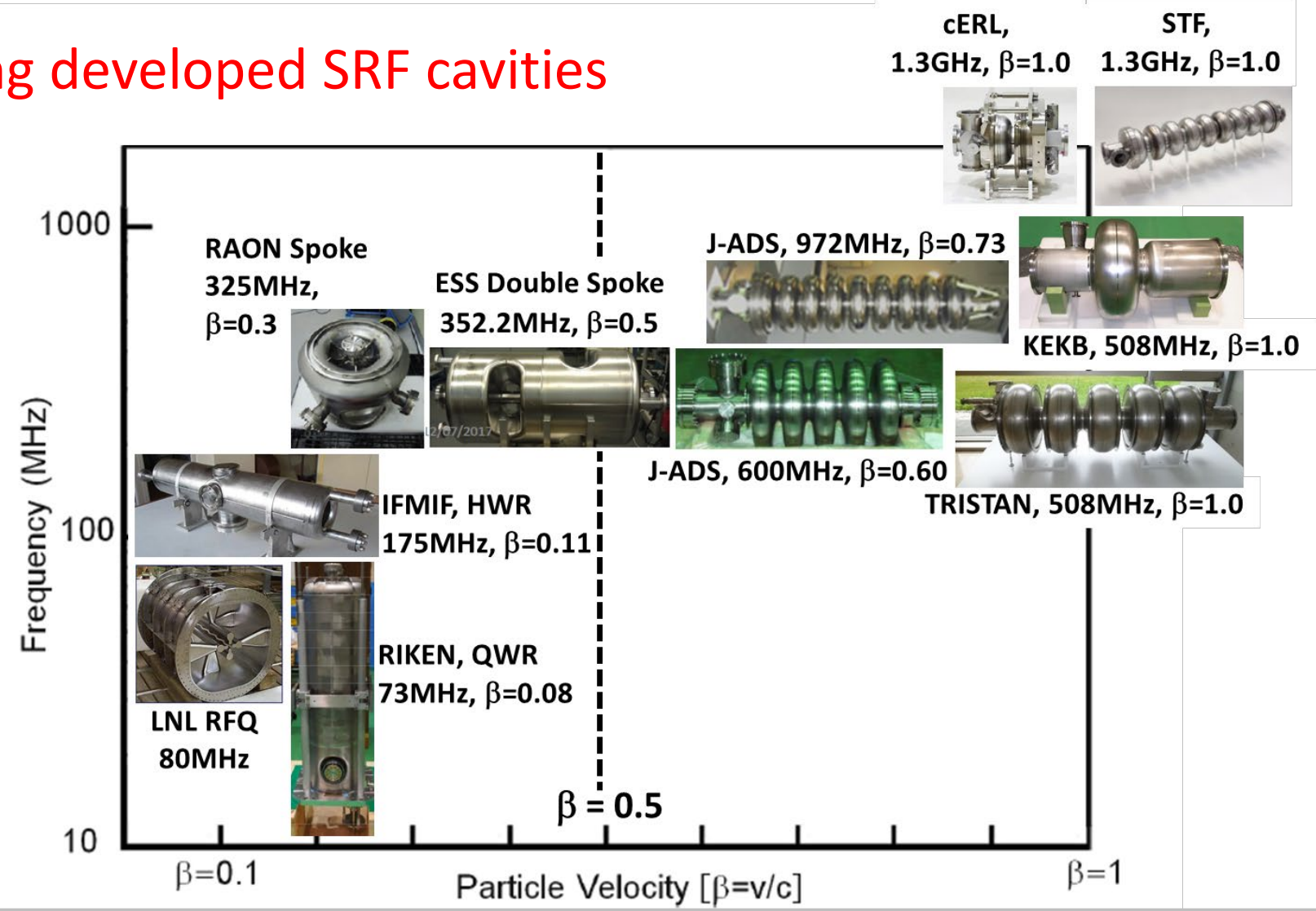


1.3 GHz, 1.5-cell SRF-Gun Cavity

Accelerating Structures for Proton/Ions and Electrons



Existing developed SRF cavities





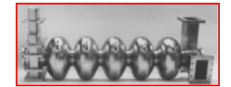
FERMI 3.9 GHz



S-DALINAC 3 GHz



CEBAF 1.5 GHz



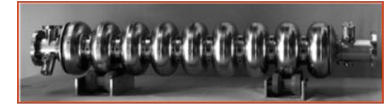
HEPL 1.3 GHz



CESR 0.5 GHz



TESLA/ILC 1.3 GHz



SNS $\beta=0.61, 0.81, 0.805$ GHz



HERA 0.5 GHz



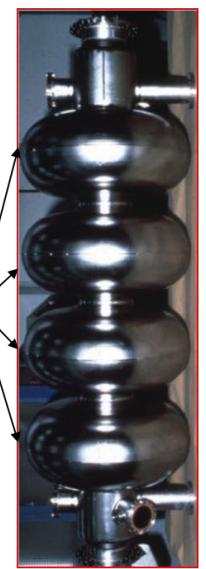
TRISTAN 0.5 GHz



KEK-B 0.5 GHz



LEP 0.352 GHz



cells

Elliptical multi-cell cavities

Quarter Wave Resonators (QWR)



Half Wave Resonators (HWR)

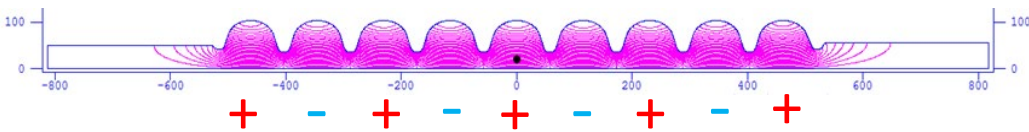


Spoke cavities

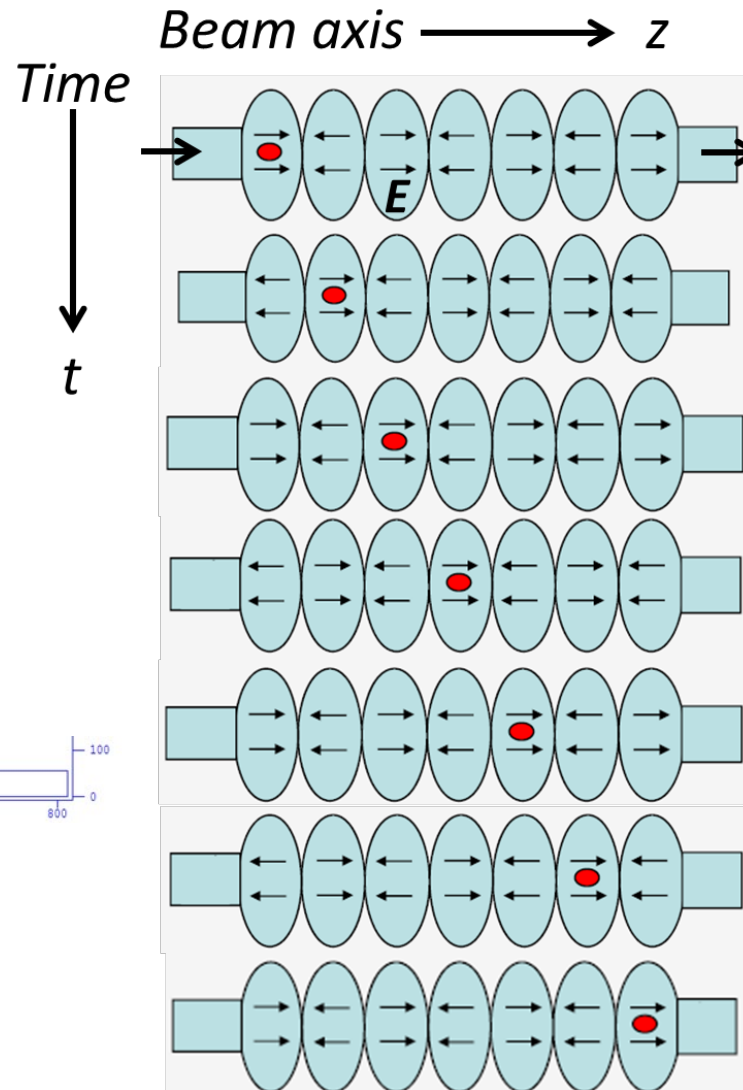




1.3 GHz, 9-cell Cavity



Accelerating Electric Field
(TM010 π -mode)



$$z = v \cdot t$$

$$E = E_0 \sin(\omega t)$$

$$= E_0 \sin(kz)$$

Synchronized condition

$$v = c, (\beta = 1)$$

$$f = \frac{\omega}{2\pi} = \frac{c}{\lambda}$$



Several important equations and useful formulas are now introduced in order to better understand the behavior of the electromagnetic fields inside an RF cavity:

- Maxwell's equations:

$$\operatorname{div} \vec{B} = 0 \quad \operatorname{div} \vec{D} = \rho \quad \operatorname{rot} \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \quad \operatorname{rot} \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

- Wave equation:

$$\nabla^2 \vec{H} = \sigma \mu \frac{\partial}{\partial t} \vec{H} + \varepsilon \mu \frac{\partial^2}{\partial t^2} \vec{H}$$

- Helmholtz equation: $\nabla^2 \vec{H} + k^2 \vec{H} = 0$

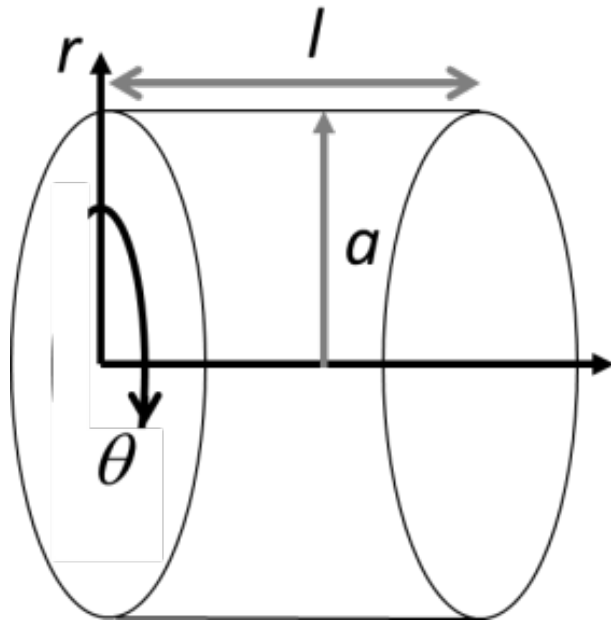
$$\nabla^2 \vec{E} + k^2 \vec{E} = 0$$

- Bessel equation and Bessel functions:

$$\frac{d^2 R}{dr^2} + \frac{1}{r} \frac{dR}{dr} + \left(k_c^2 - \frac{n^2}{r^2} \right) R = 0 \quad J_n(k_c r) = \sum_{m=0}^{\infty} \frac{(-1)^m (k_c r / 2)^{n+2m}}{m! (n+m)!}$$



The following important RF parameters for the case of the pill-box cavity are calculated analytically from the fundamental equations obtained in the previous formulas.



A pill-box cavity, (circular cylindrical resonator):
The symbol a and l represents the radius and the cavity length of the pill-box cavity, respectively.

- Resonant frequency: f_0
- Stored energy: W_s
- RF loss (dissipation power): P_d
- RF surface resistance: R_s
- Quality factor: Q
- Geometrical factor: G
- Transit-time factor: T
- Accelerating gradient: E_{acc}
- Shunt impedance: R_{sh}
- R over Q: R/Q
- Energy gain

Accelerating mode (TM₀₁₀)



TM₀₁₀ mode is known as “accelerating mode”. The boundary conditions of electromagnetic fields of the accelerating mode inside a pill-box cavity can be written as follows:

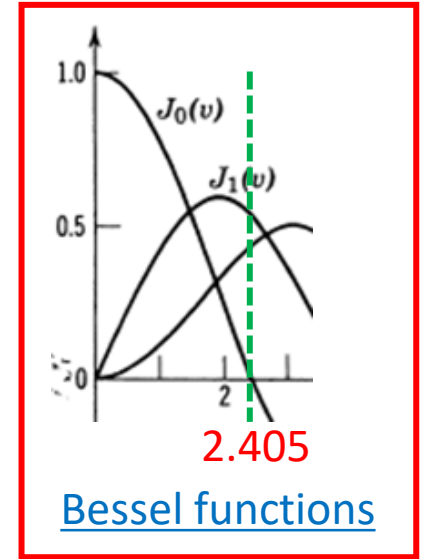
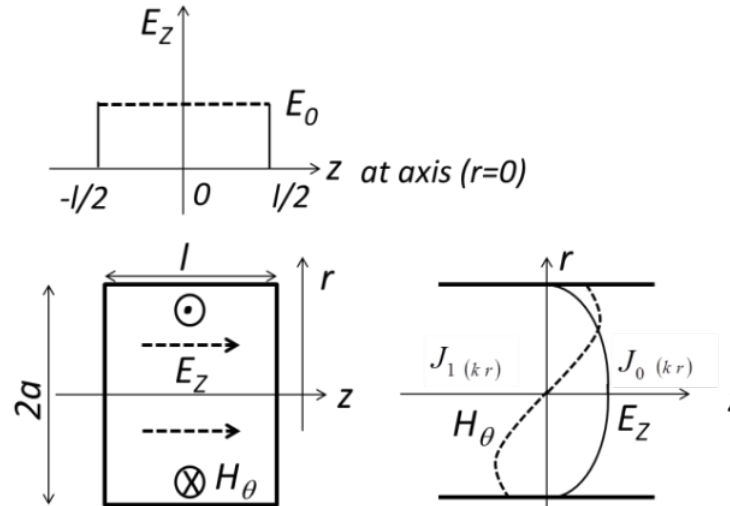
$$\begin{aligned} H_z &= 0, \\ E_r &= 0, \\ H_r &= 0, \\ E_\theta &= 0. \end{aligned}$$

Only two components of $E_z(r)$ and $H_\theta(r)$ exist.

$$\begin{aligned} E_{z(r)} &= E_0 J_0(kr) \cos \omega t \\ H_{\theta(r)} &= -\left(\frac{E_0}{Z_0}\right) J_1(kr) \sin \omega t \end{aligned}$$

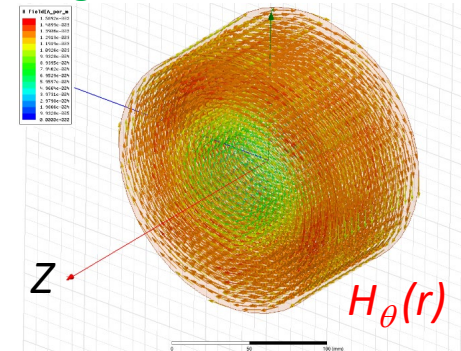
where the following relation holds:

$$Z_0 = E_0/H_0 = (\mu_0/\epsilon_0)^{0.5} = 120 \pi = 377 \Omega .$$

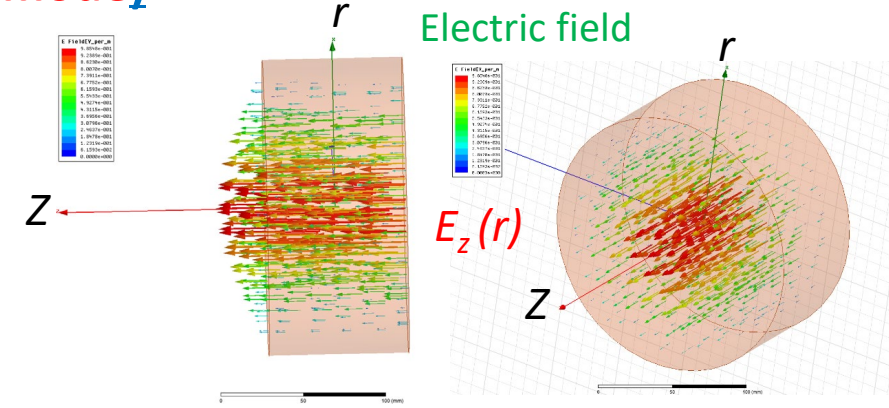


Accelerating mode (TM₀₁₀ mode)

Magnetic field r



Electric field





The essential RF parameters can be summarized as follows:

- Electric RF field E [V/m]: $\vec{E} \exp(j\omega t)$

- Magnetic RF field H [A/m]: $\vec{H} \exp\left\{j\left(\omega t + \frac{\pi}{2}\right)\right\}$

- Accelerating gradient E_{acc} [V/m]:

$$E_{acc} = \frac{1}{l} \int_{-l/2}^{l/2} E_Z(z, r=0) \cos(k \cdot z) dz$$

- RF Loss / Dissipated RF power P_d [W]:

$$P_d = \frac{R_s}{2} \int_A |\vec{H}|^2 dA$$

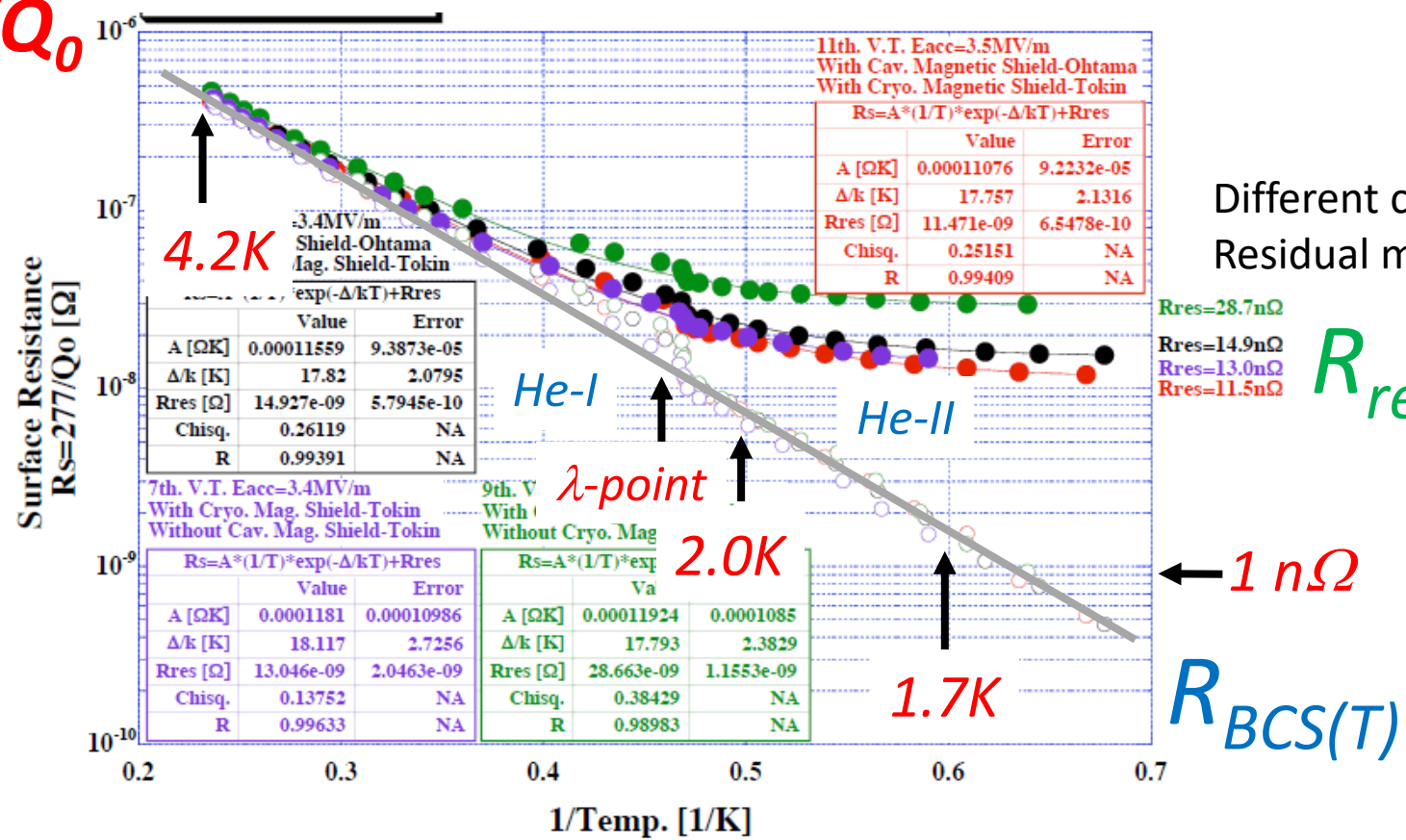


- Stored energy W_S [J]:
$$W_S = \frac{\mu_0}{2} \int_V |\vec{H}|^2 dV = \frac{\epsilon_0}{2} \int_V |\vec{E}|^2 dV$$
- Quality factor Q :
$$Q = \frac{\omega_0 W_S}{P_d} = \frac{G}{R_S}$$
- Geometrical factor G [Ω]:
$$G = \omega_0 \mu_0 \frac{\int_V |\vec{H}|^2 dV}{\int_A |\vec{H}|^2 dA}$$
- Effective shunt impedance R_{sh} [Ω]:
$$R_{sh} = \frac{V_{acc}^2}{P_d} = \frac{E_{acc}^2}{P_d} L_{cavity}^2$$
- R/Q [Ω]:
$$\left(\frac{R}{Q} \right) = \frac{E_{acc}^2}{\omega W_S} L_{cavity}^2$$



1.3 GHz, 9-cell Superconducting Cavity

$$R_S = G/Q_0$$



Different condition of Residual magnetic field

$$R_S = R_{BCS}(T) + R_{res}, \quad R_{BCS} = A \frac{\omega^2}{T} \exp\left(-\frac{\Delta}{k_B \cdot T}\right)$$



Normal-conducting Cavity ;

- Surface resistance; R_S [Ω]

$$R_S = \sqrt{\frac{\omega \mu}{2 \sigma}} = \frac{1}{\sigma \delta} \quad [\Omega]$$

$$f = 1.3 \text{ GHz}, \quad G = 270 \Omega$$

$$\text{Cu (20°C)} ; \quad \sigma = 0.58 \times 10^8 \text{ [1/}\Omega\text{m]}$$

$$\underline{R_S = 9.4 \text{ m}\Omega, \quad (\delta = 1.8 \text{ }\mu\text{m})}$$

$$\underline{Q = G / R_S = 2.9 \times 10^4}$$

Superconducting Cavity ;

- Surface resistance; R_S [Ω]

$$R_S = R_{BCS(T)} + R_{res}$$

$$R_{BCS} = A \frac{\omega^2}{T} \exp\left(-\frac{\Delta}{k_B \cdot T}\right)$$

$$f = 1.3 \text{ GHz}, \quad G = 270 \Omega$$

$$\text{Nb (2K)} ; \quad R_{BCS} = 7 \text{ [n}\Omega\text{]}$$

$$R_{res} = 7 \text{ [n}\Omega\text{]}$$

$$\underline{R_S = 14 \text{ n}\Omega, \quad (\lambda_0 = 44 \text{ nm})}$$

$$\underline{Q = G / R_S = 1.9 \times 10^{10}}$$

R_{BCS} : BCS resistance

R_{res} : Residual surface resistance

k_B : Boltzmann constant

Δ : Gap energy of Cooper pair

Question (2)



What is the advantage of superconducting cavities?



What is the advantage of superconducting cavities?

- low surface loss → higher Q → higher Ws
- high acceleration gradient
→ higher energy in smaller space
- better efficiency to beam power
→ smaller RF power source
- ***CW operation at higher fields***

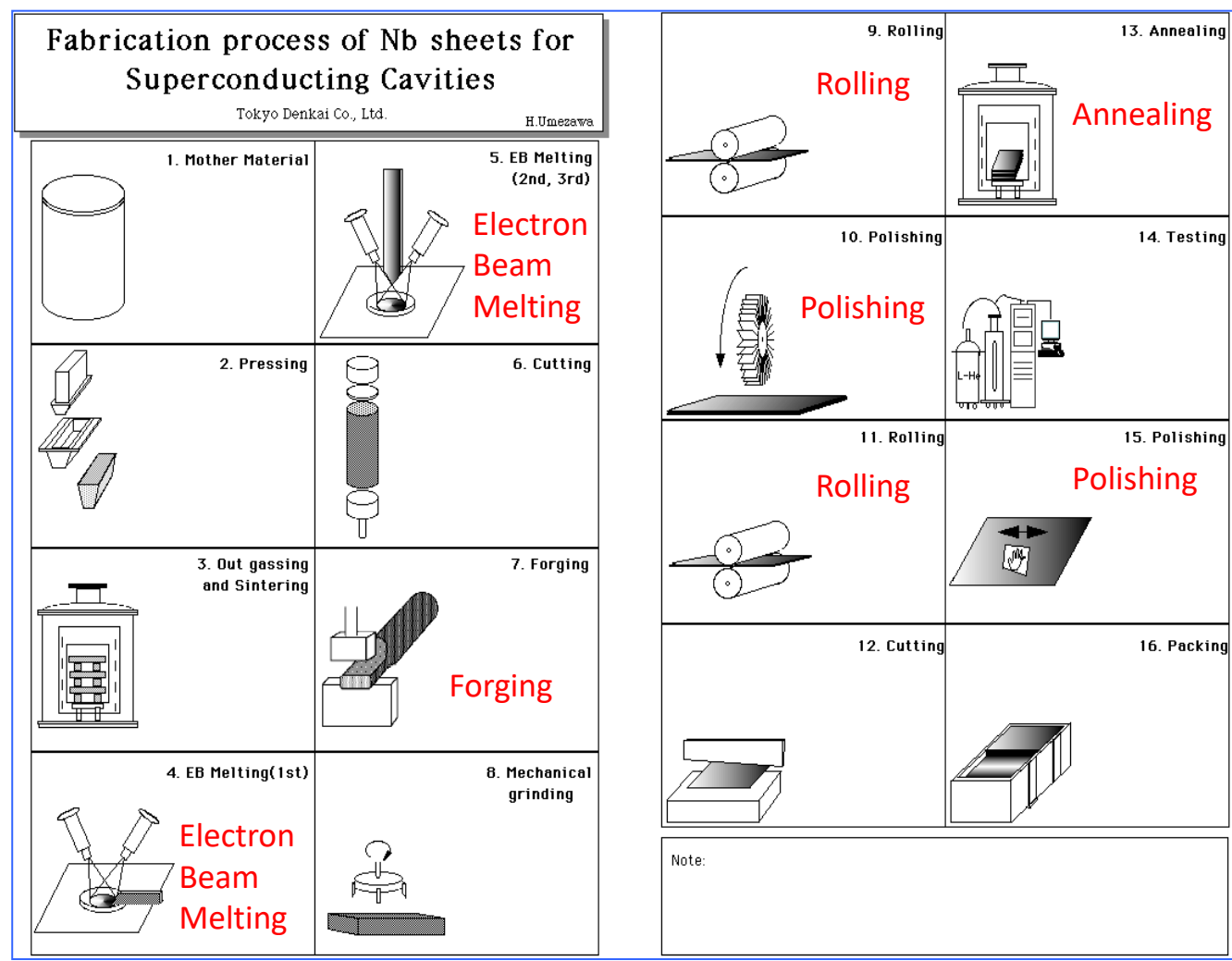
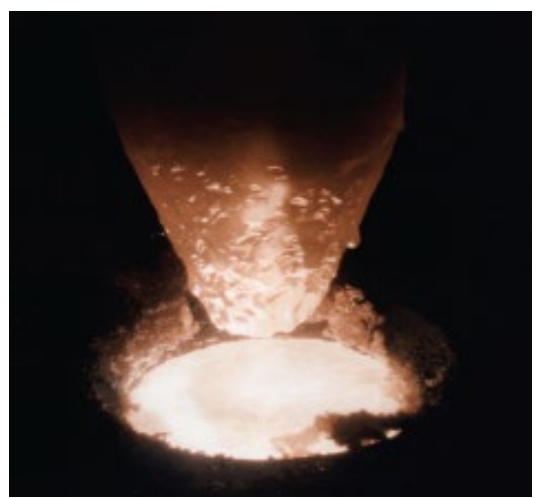


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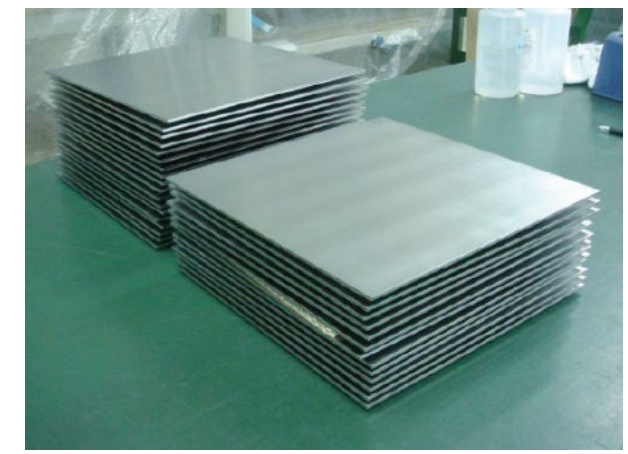
Fabrication Process of Nb Sheets



Electron Beam Melting



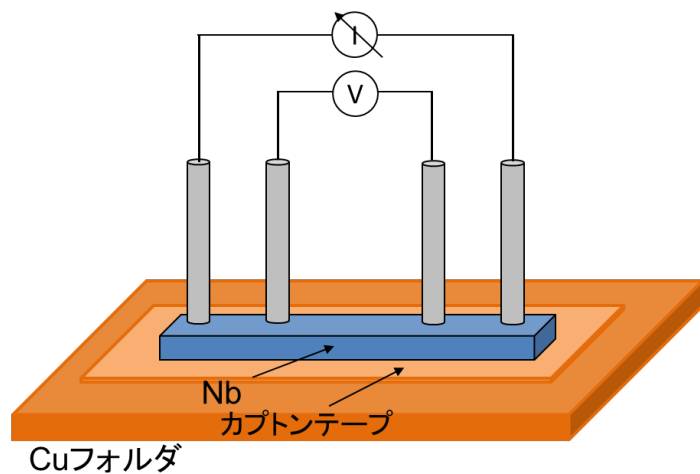
[by H. Umezawa (Tokyo Denkai)]



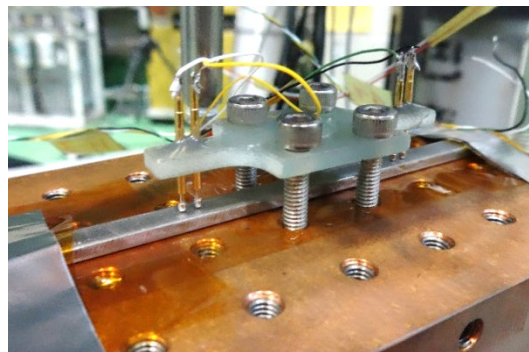
Material certification of Nb: (Mill sheet)



Customer Messrs.		MATERIAL TEST RESULTS										No. 28378		
御納入先 高エネルギー加速器研究機構 殿		試験成績表												
Surveyor 御立会者 殿		Date 日付 平成25年3月4日					TOKYO DENKAI CO., LTD. 東京電解株式会社							
Material 材質	Article 品名	Quantity 数量	Mechanical properties 機械的特性											
			T.S 引張強さ N/mm ²	Y.S 耐力 N/mm ²	Elongation 伸び %	Hardness かたさ Hv								
Specification No.	仕様書番号	pcs or gr	Spec 規格	min	max	Longitudinal								
Nb	Disc					120	39	35						
4378		58 pcs	2.8t × 258 φ - 56 φ	162	47	56	50.8							
				171	51	54								
Lot No.	Element 成分	Chemical Composition (in Wt%) 化学成分												
		Ta	W	Ti	Fe	Si	Mo	Ni	C	Nb				
4378	Spec 規格	min	max	0.15	0.02	0.005	0.005	0.005	0.005	0.005	0.01			
	Test Results 試験結果	0.0115	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001	balance			
				Ta	W									
Lot No.	Element 成分	Chemical Composition (in Wt%) 化学成分												
		O	N	H	C									
4378	Spec 規格	min	max	0.015	0.01	0.002	0.01							
	Test Results 試験結果	<0.001	<0.001	<0.0005	<0.001									
				O	N	H	C							
Remarks 備考		Starting Ingot Lot No. NC-1830 RRR Value of Sheet: 298 Grain size ASTM #6										Inspection Section Manage TOKYO DENKAI Engine		
		Purity, Thermal property RRR = 298										[by H. Umezawa (Tokyo Denkai)]		
		T.S.=Tensile Strength Y.S.=Yield Strength E.V.=Erichsen Value												



RRR measurement system

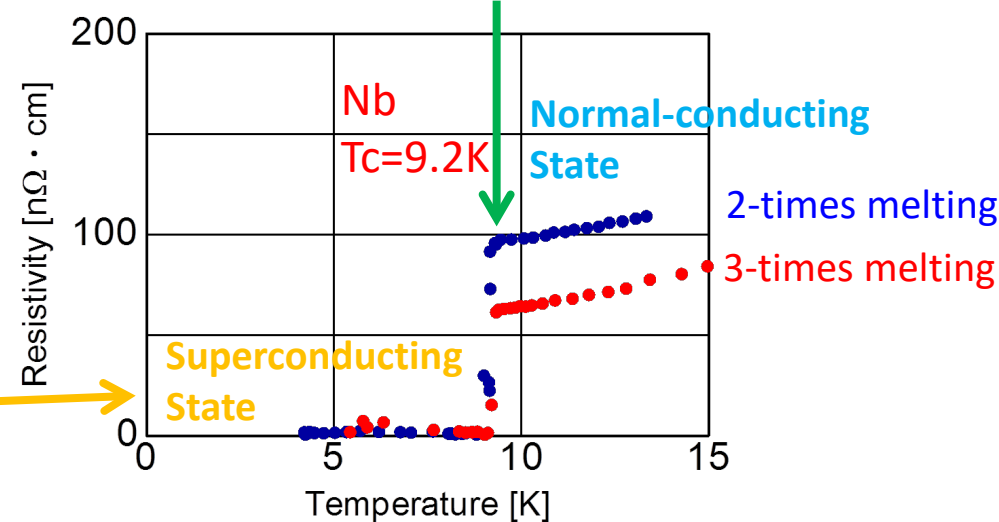
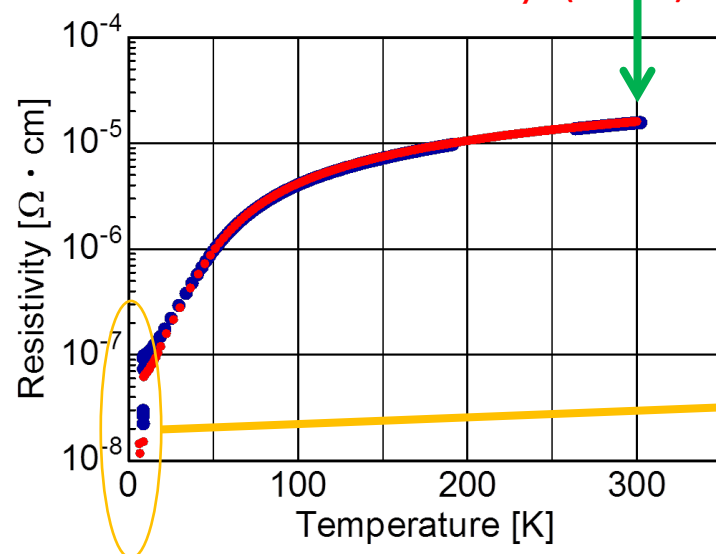


Residual Resistance Ratio

$$RRR = \frac{\rho(300K)}{\rho(9.2K)}$$

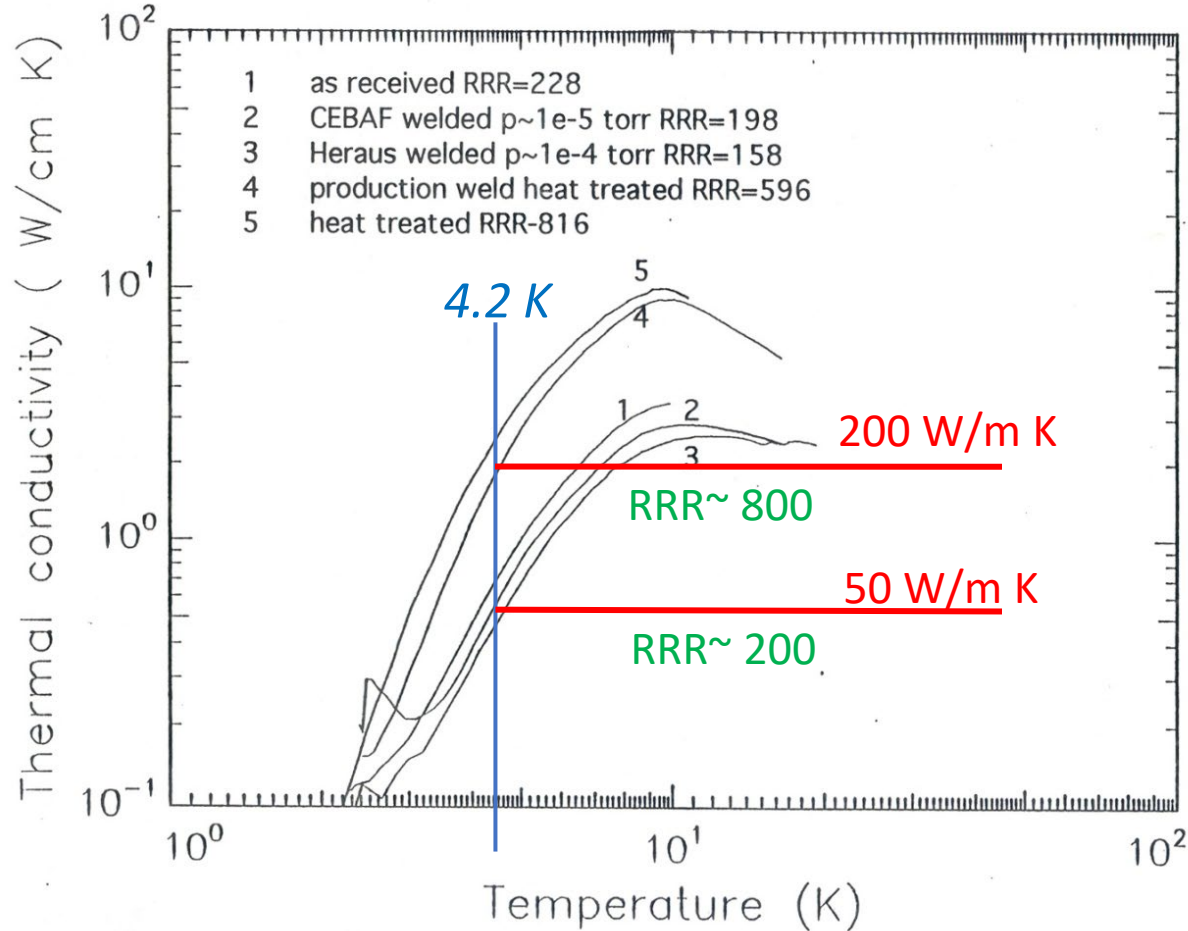
$\rho(300K) = 2 \times 10^{-5} \Omega \cdot \text{cm}$
 $\rho(300K) = 2 \times 10^{-5} \Omega \cdot \text{cm}$

$\rho(9.2K) = 1 \times 10^{-7} \Omega \cdot \text{cm}$ **RRR = 200**
 $\rho(9.2K) = 6 \times 10^{-8} \Omega \cdot \text{cm}$ **RRR = 330**





Thermal conductivity of Nb



RRR : Residual Resistance Ratio

$$RRR = \frac{\rho(300K)}{\rho(9.2K)}$$

K : Thermal Conductivity

$$K_{(4.2K)} \approx RRR / 4$$

[W / m · K]

Wiedemann-Franz's law

$$K \propto \sigma = \frac{1}{\rho}$$

H_{quench} : Quench field

$$H_{quench} = \sqrt{\frac{4 \kappa (T_c - T_{He})}{a R_{defect}}}$$

R_{defect} : Resistivity of Defect

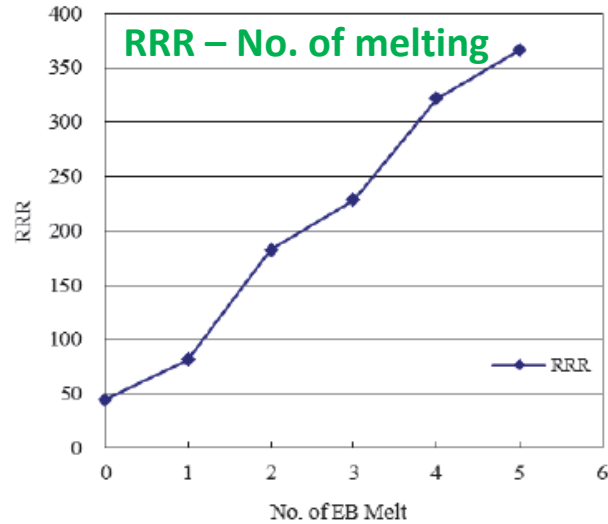
a : Radius of Defect

T_c : Critical Temperature

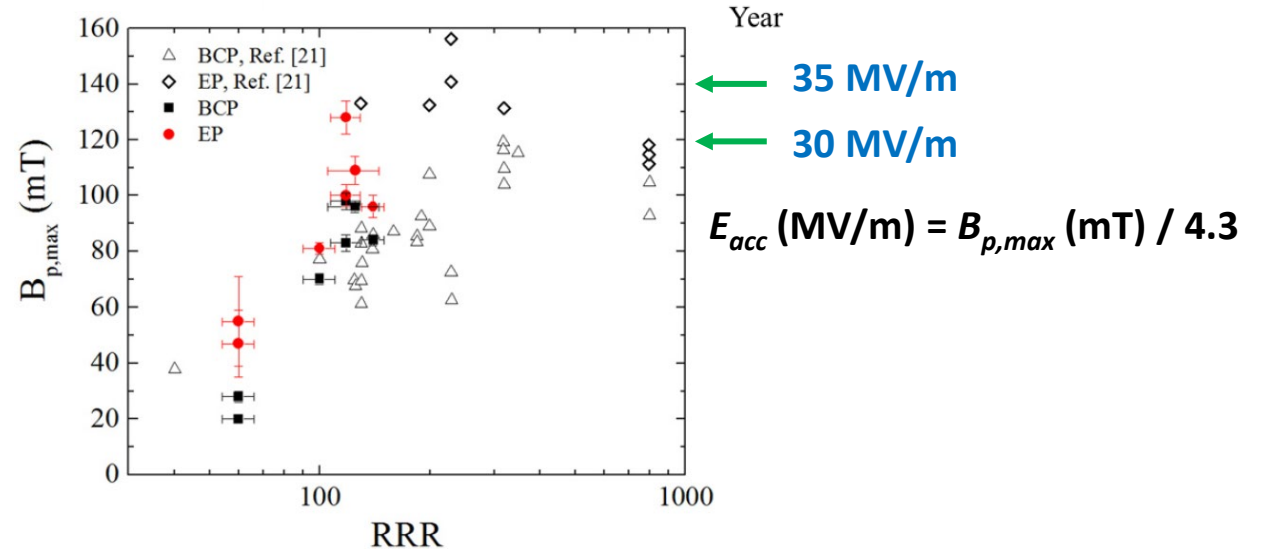
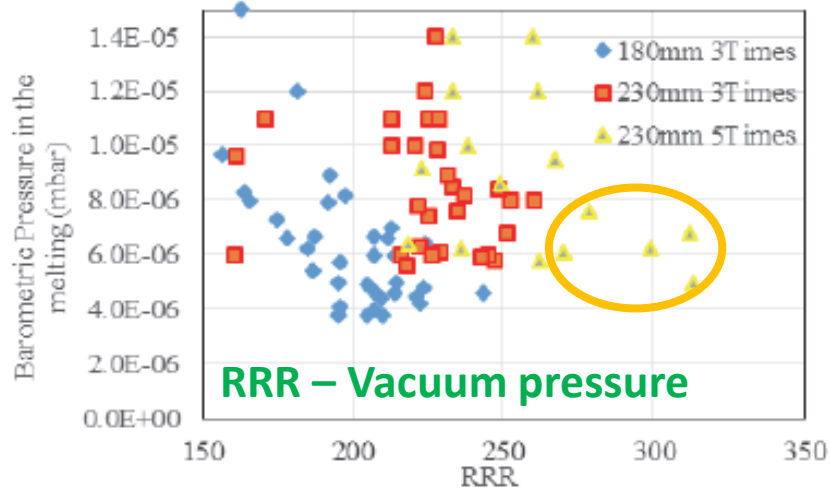
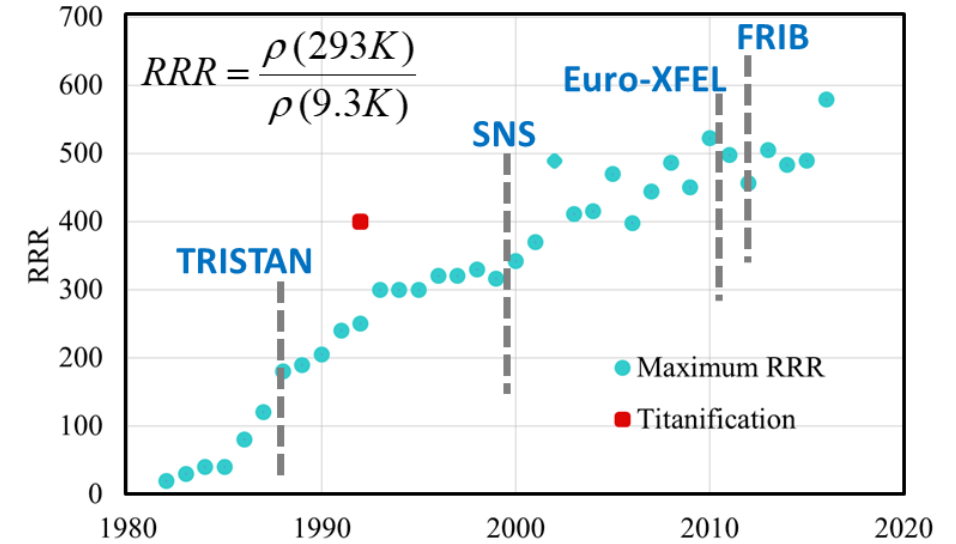
T_{He} : He Temperature

High RRR niobium with high thermal conductivity is preferable for achieving higher accelerating gradient.

Characteristics of Nb materials: (Improvement of RRR)



[by H. Umezawa (Tokyo Denkai)]



TRISTAN 508MHz 5-cell Cavity



He temperature at 4.2 K
 CW operation

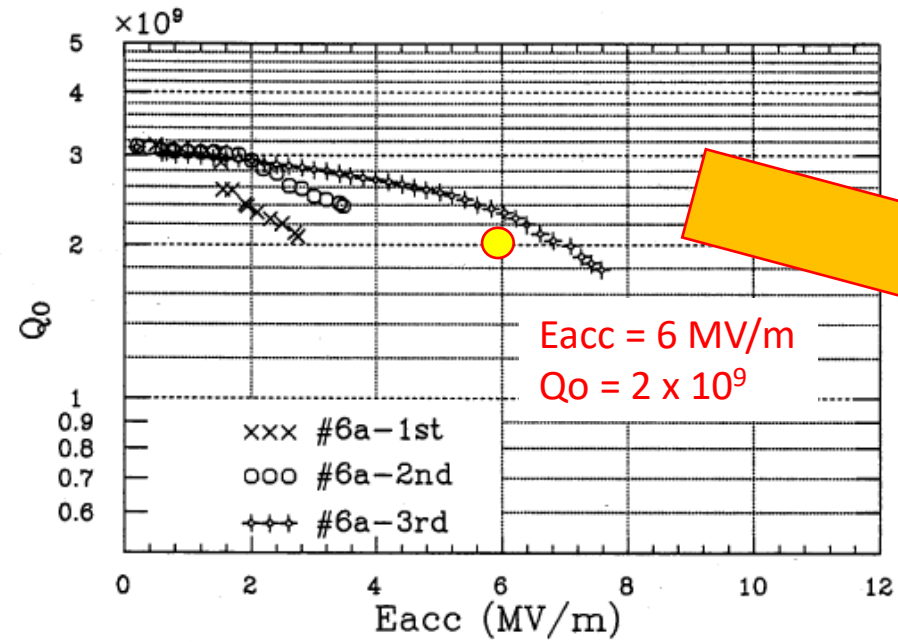


Figure 7: Q_0 and E_{acc} of TRISTAN #6a cavity. [T. Furuya, SRF'89]

STF 1.3GHz 9-cell Cavity



He temperature at 2.0 K
 1 ms, 5 Hz pulsed operation

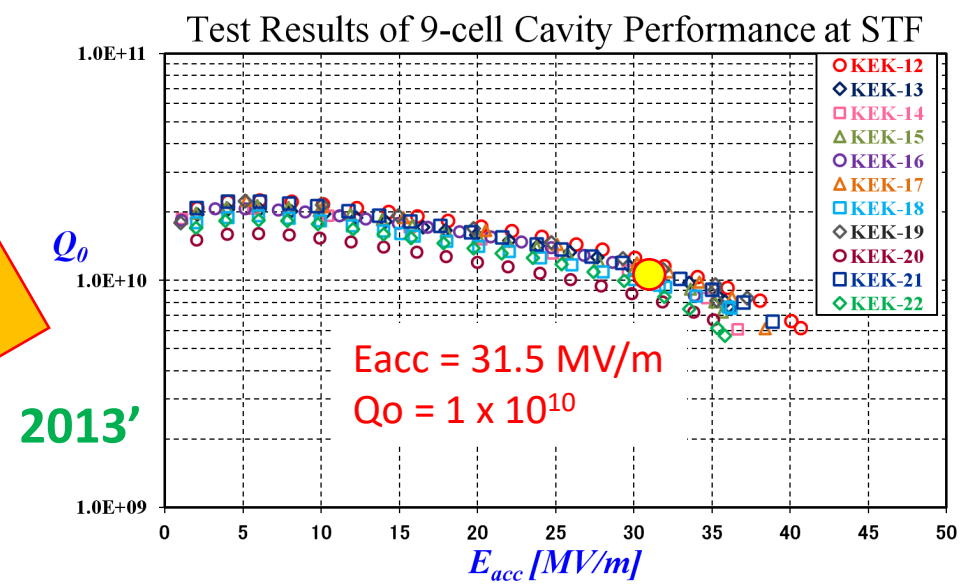
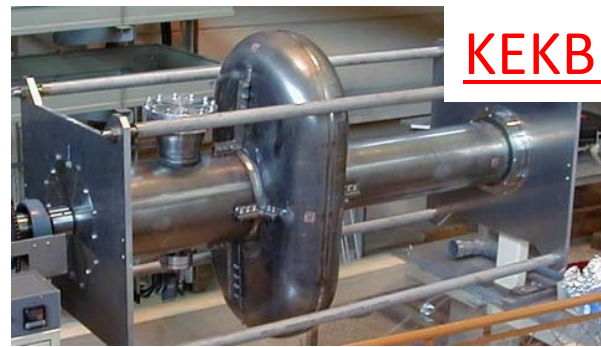


Figure 1: Best Q_0 vs. E_{acc} curves obtained from performance tests for KEK-12 through KEK-22. [Y. Yamamoto, NIM-A (2013)]

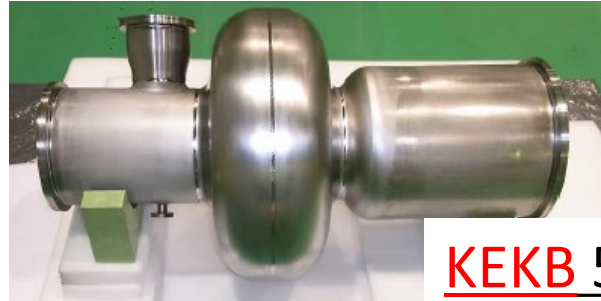
SRF cavities developed at KEK



TRISTAN
508MHz 5-cell Cavity



KEKB 508MHz Crab Cavity



KEKB 508MHz 1-cell Cavity

J-ADS 972MHz
9-cell Cavity
($\beta=0.73$)



cERL Injector
1.3GHz 2-cell Cavity



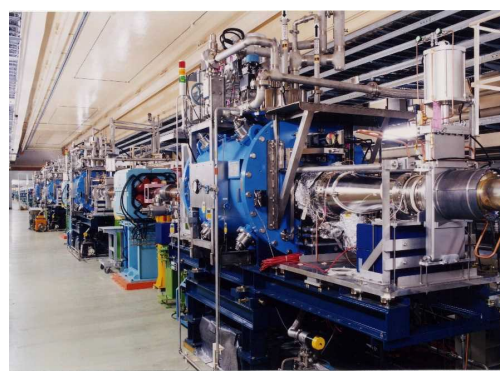
cERL ML 1.3GHz 9-cell Cavity



STF 1.3GHz 9-cell Cavity



TRISTAN 508MHz Cryomodule



KEKB
508MHz Cryomodule

KEKB Crab Cryomodule



J-ADS 972MHz
Cryomodule



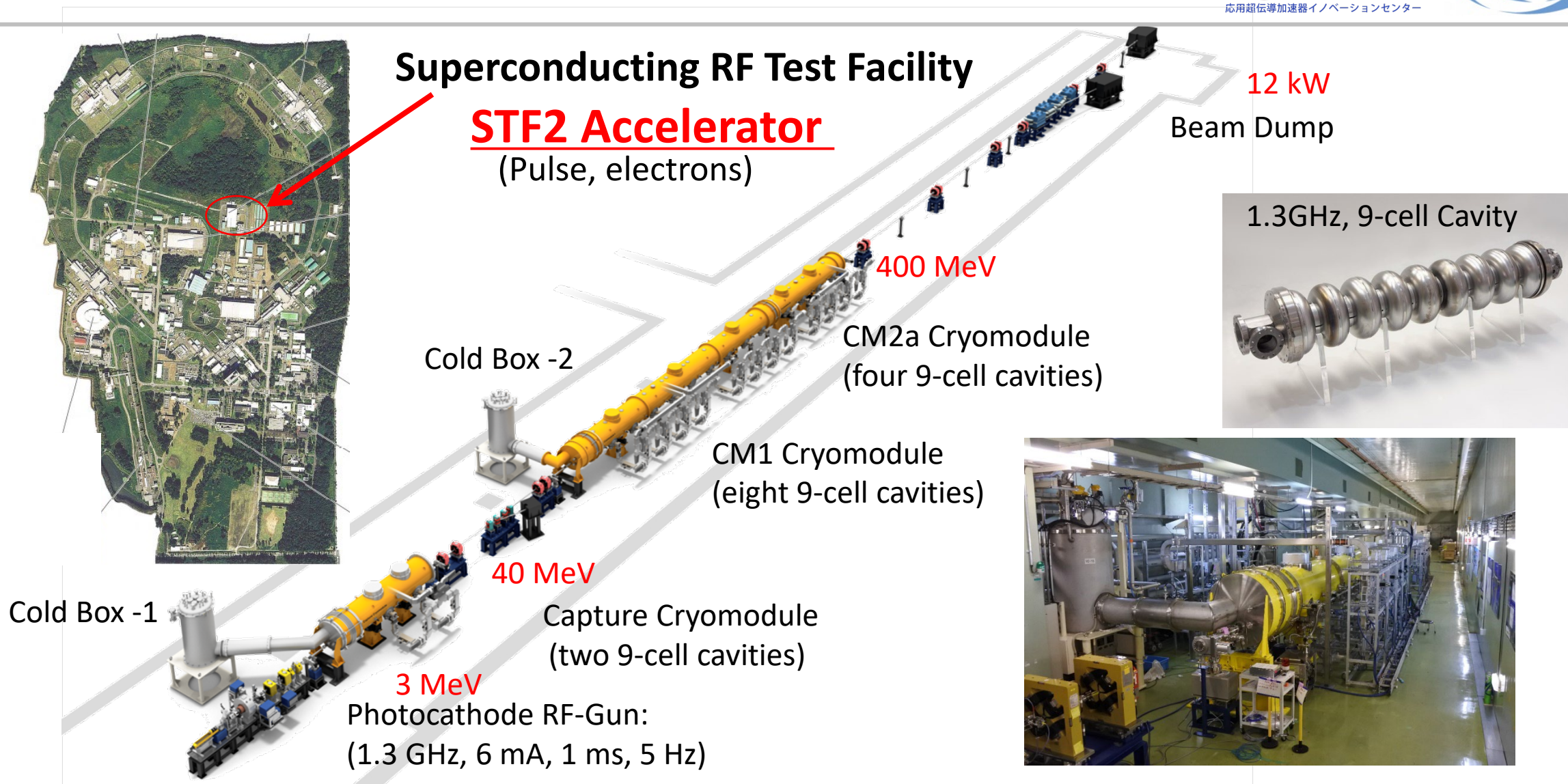
cERL 1.3 GHz
Injector Cryomodule



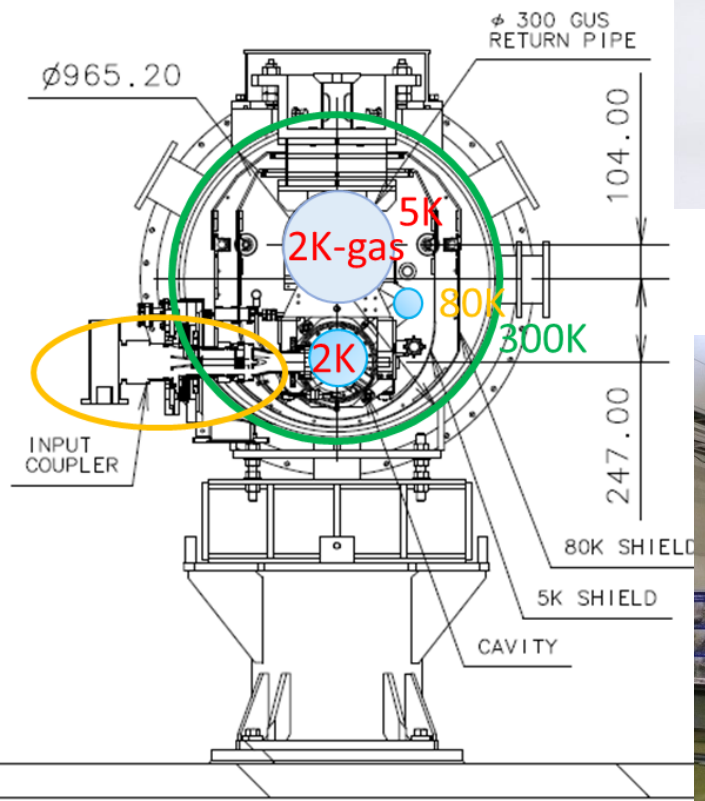
cERL 1.3 GHz
ML Cryomodule



STF 1.3GHz Cryomodule



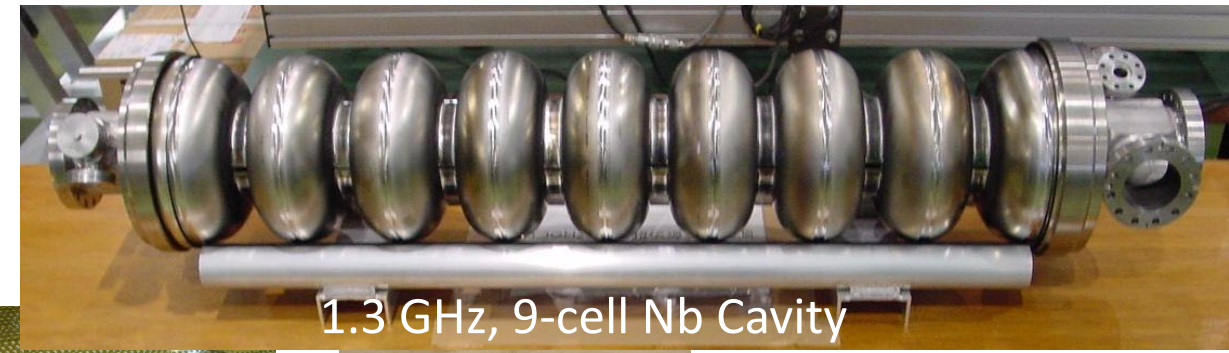
Cryomodule



STF Cryomodule



Input Couplers



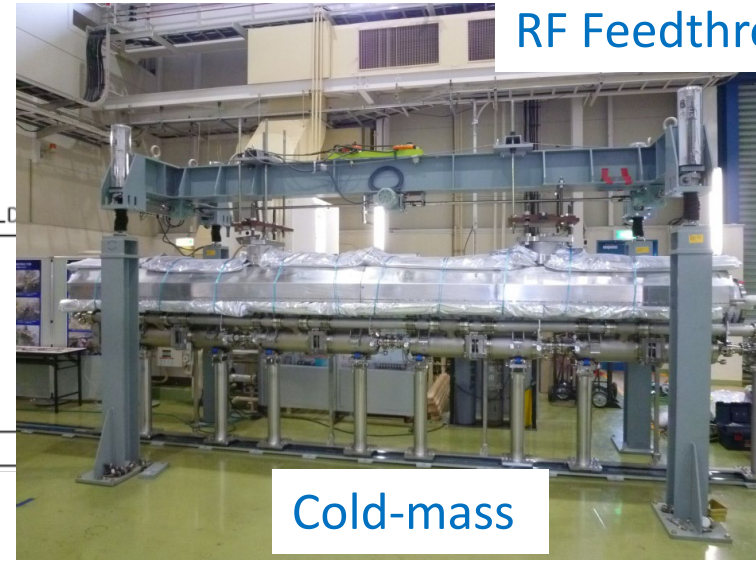
1.3 GHz, 9-cell Nb Cavity



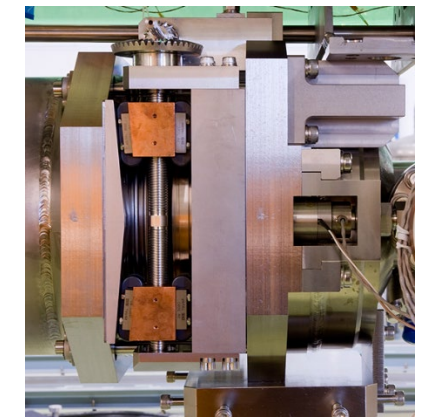
RF Feedthroughs



HOM Couplers



Cold-mass



Slide-Jack Tuner



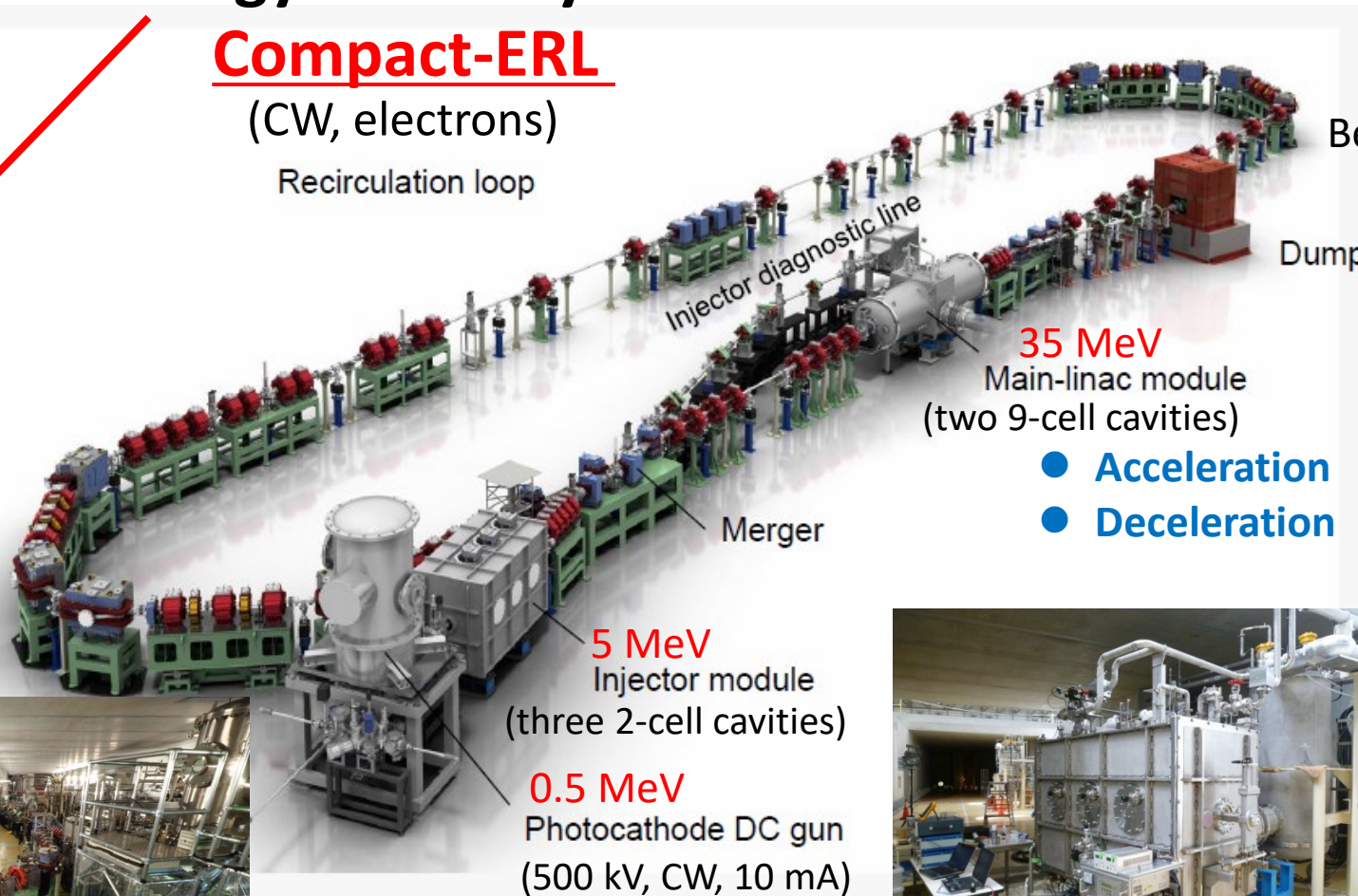
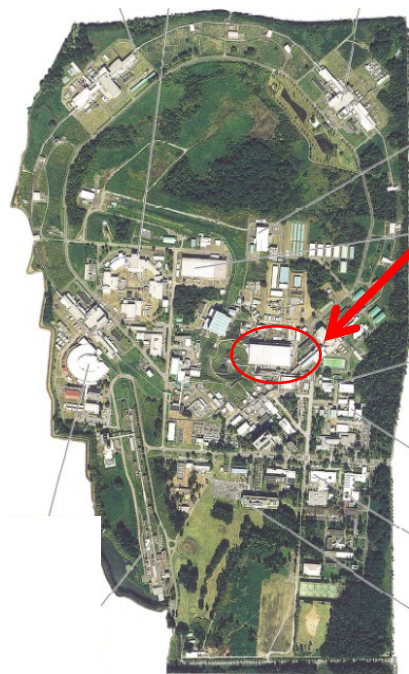
Magnetic Shield & He Jacket (Ti)

Energy Recovery LINAC

Compact-ERL

(CW, electrons)

Recirculation loop



50 kW
Beam Dump



35 MeV
Main-linac module
(two 9-cell cavities)

- Acceleration
- Deceleration

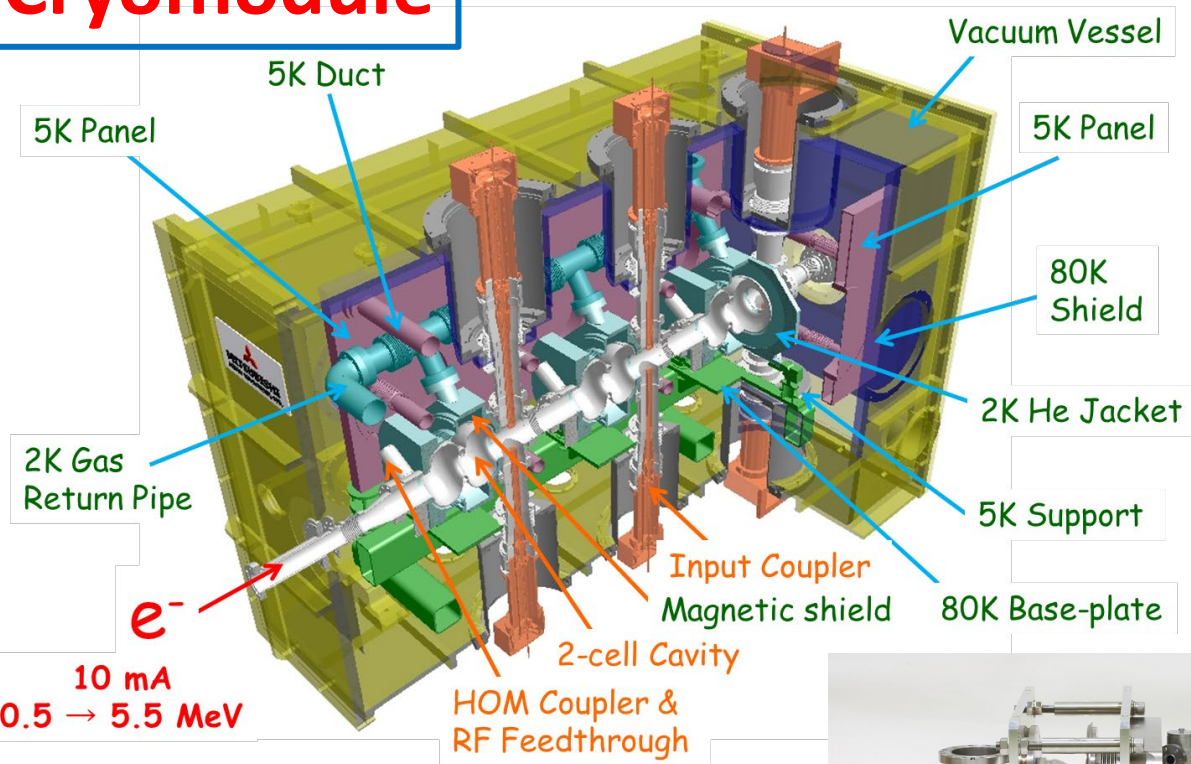
Merger

5 MeV
Injector module
(three 2-cell cavities)

0.5 MeV
Photocathode DC gun
(500 kV, CW, 10 mA)



Cryomodule



10 mA
 0.5 → 5.5 MeV

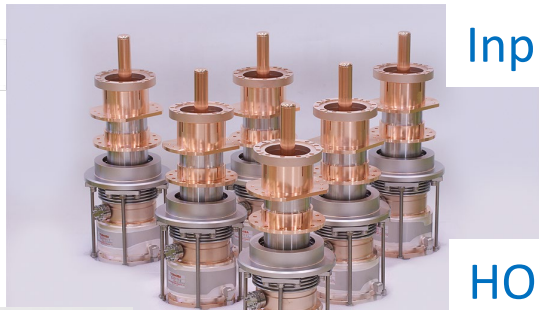
cERL Injector Cryomodule



1.3GHz, 2-cell Cavities



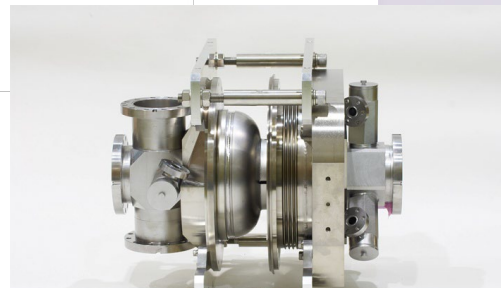
Slide-Jack Tuner



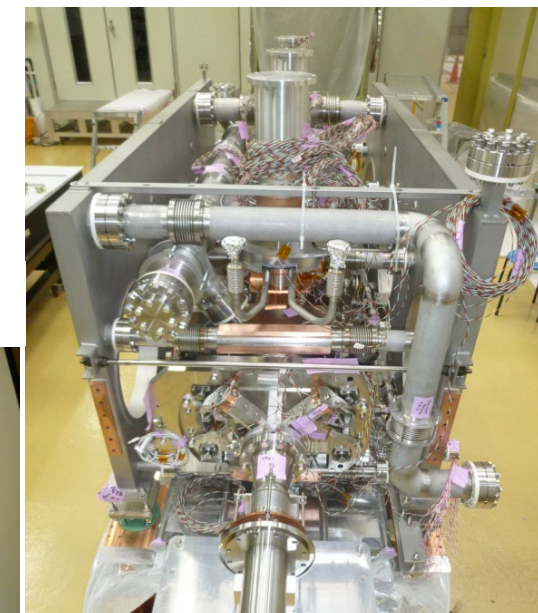
Input Couplers



HOM Couplers

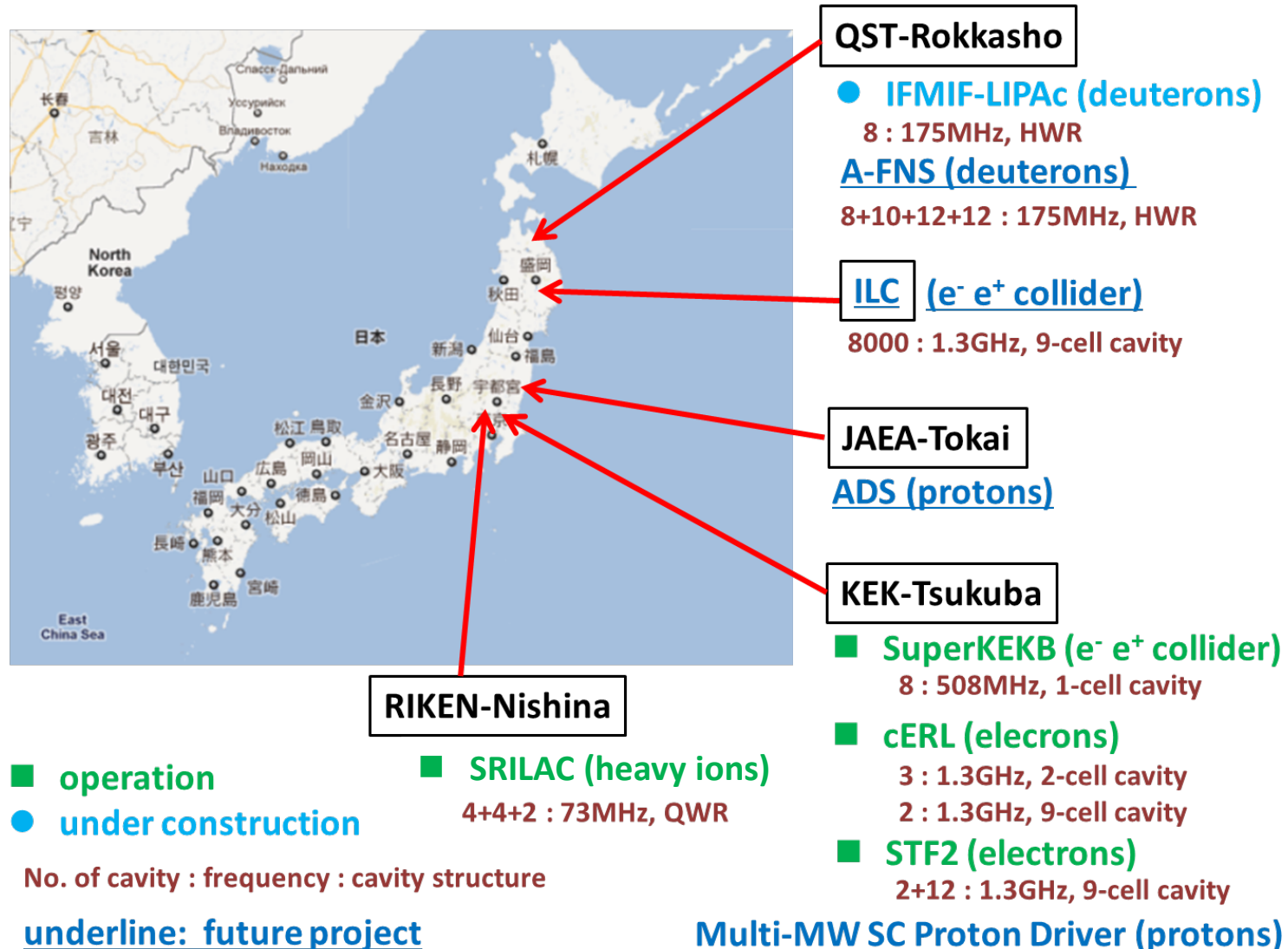


1.3GHz, 2-cell Cavity

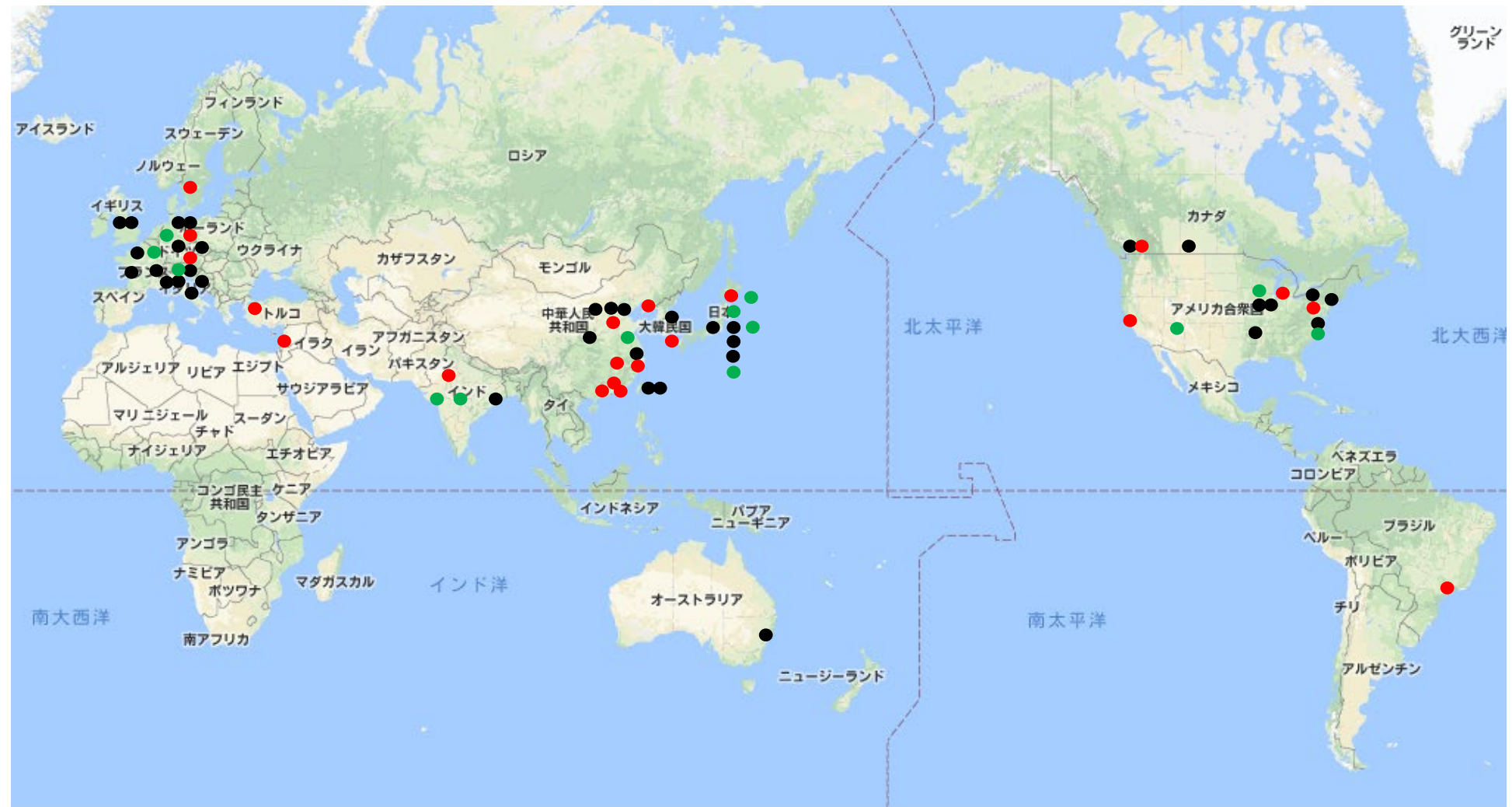


Cold Mass Assembly

Superconducting Accelerator Projects in Japan



Superconducting Accelerator Projects in World

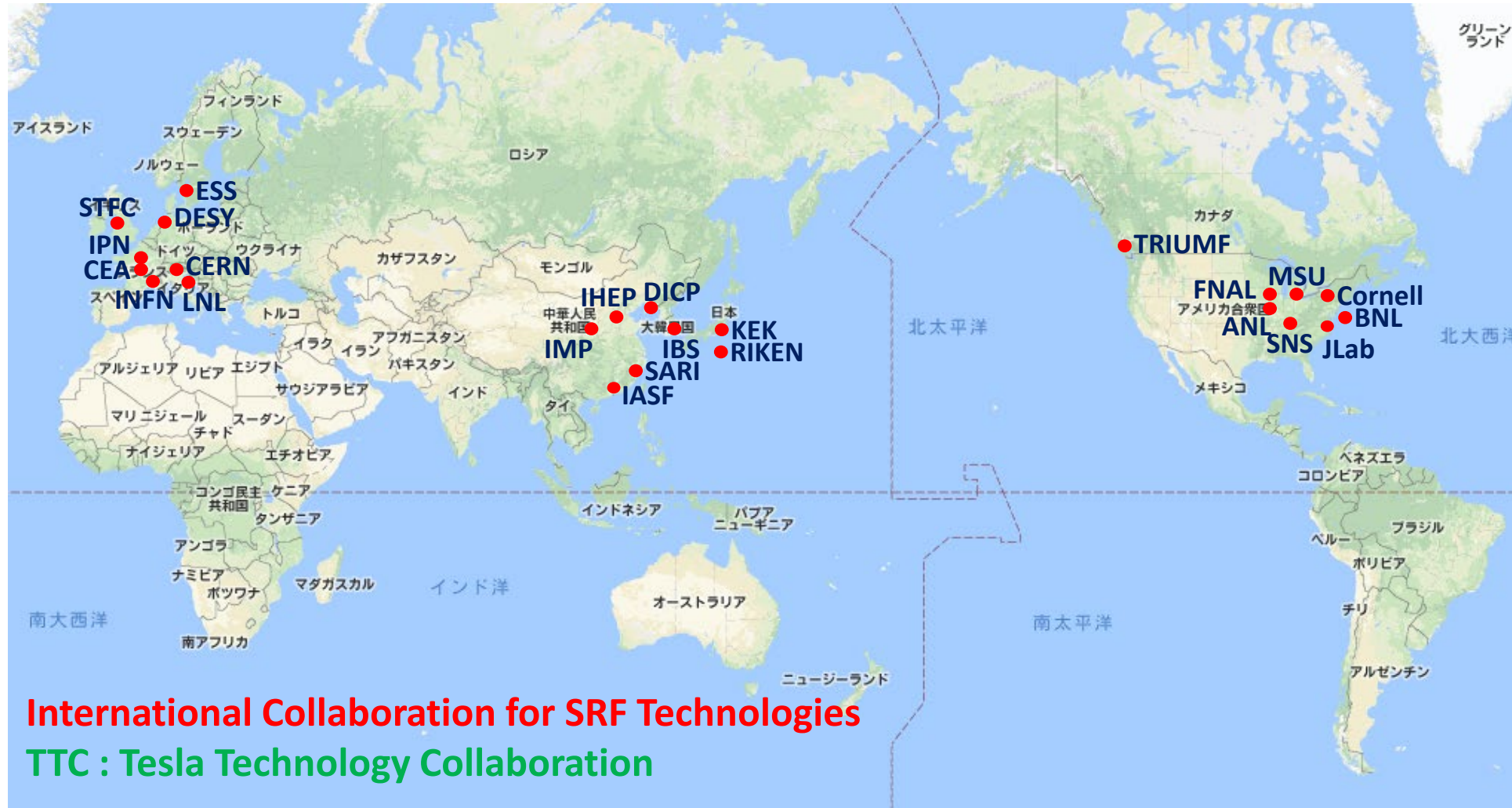


● Operation ● Construction ● Future Plan



- **Elemental Particle Physics:** (S-KEKB, BEPC, LHC, **CEPC, FCC**)
- **Radiation Light Source:** (DIAMOND, CLS, TPS, SLS, PLS, NSLS-II, **HEPS, HALF, SAPS**)
- **LINACs for Nuclear Physics:** (CEBAF, S-DALINAC)
- **LINACs for Free Electron Laser:** (FLASH, E-XFEL, LCLS-II, **SHINE, DALIS, S3FEL**)
- **Energy Recovery LINACs:** (cERL, **bERLinPro**, CBETA, **PERLE**)
- **Proton LINACs for N. Source & ADS:** (SNS, **ESS, CESS, CiADS, MIRROR, J-ADS**)
- **Proton LINACs for Neutrino Experiments :** (**PIP-II, HIPrDr-KEK**)
- **Deuteron LINACs for Nuclear Fusion:** (**IFMIF-LIPAc, A-FNS, DONES**)
- **Heavy Ions LINACs:** (ISAC-II, SPIRAL-2, RILAC, FRIB, **RAON, HIAF**)
- **Linear Colliders for High Energy Physics** (STF, FAST, **ILC**)

Operation
Construction
Future Plan



- Cryogenics (Liq. He)
- Surface preparation
- Vacuum Furnace
- HPR
- Clean room
- VT

Question (3)



***Why our international collaboration is important for
R&D of superconducting cavities?***

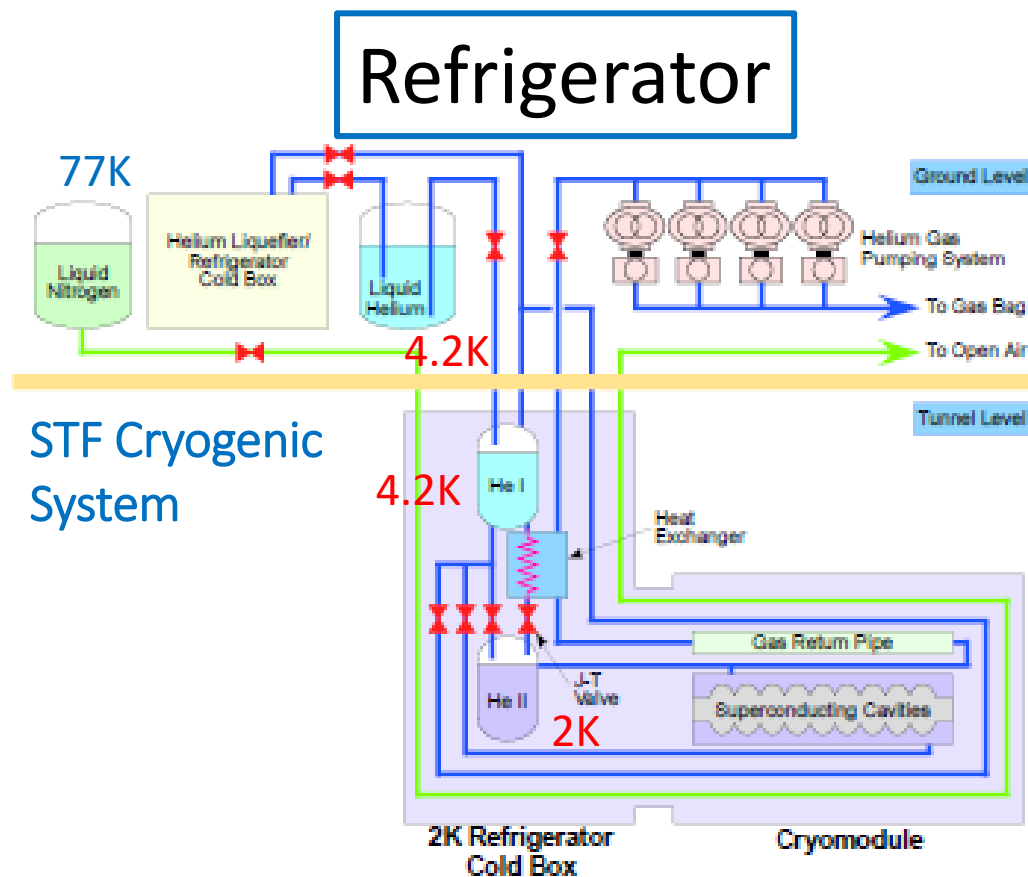


Why our international collaboration is important for R&D of superconducting cavities?

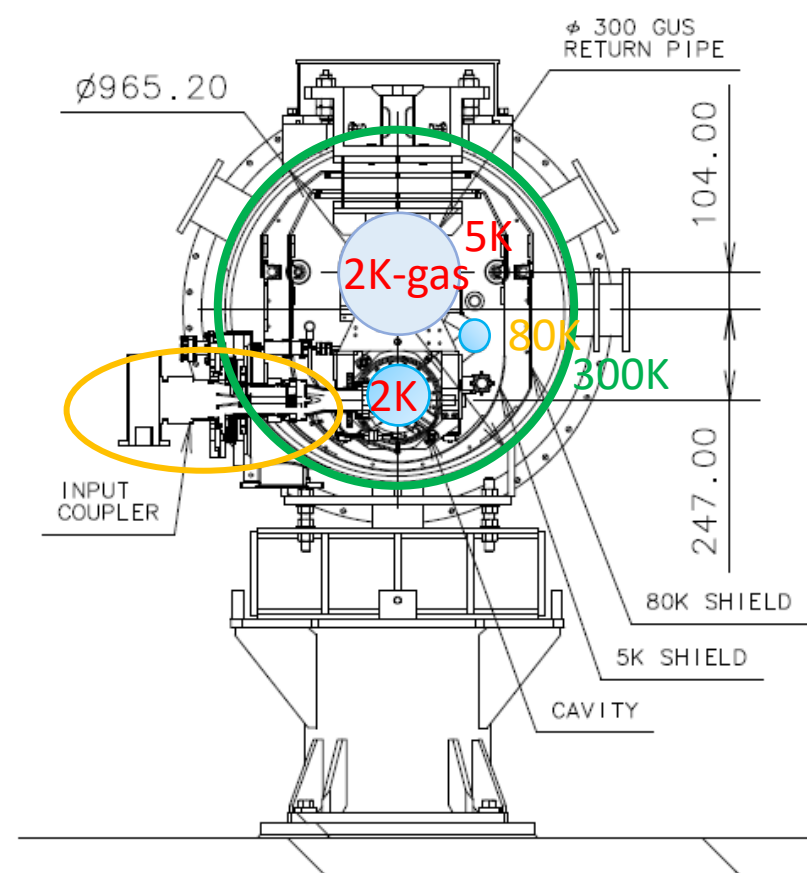
- To advance SRF technology R&D and related accelerator studies across the **broad diversity of scientific applications**.
- To keep open and provide a bridge for **communication** and **sharing** of ideas, developments, and testing across associated projects.
- **Free and open exchange** of scientific and technical knowledge, expertise, engineering designs, and equipment.
- New developments are reported, recent findings are discussed, and **technical issues concluded**.



1. Introduction
2. Fundamental of SRF Cavity
3. Overview of SRF Cavity System
- 4. Fabrication and Surface Preparation**
5. Cavity Performances
6. Summary



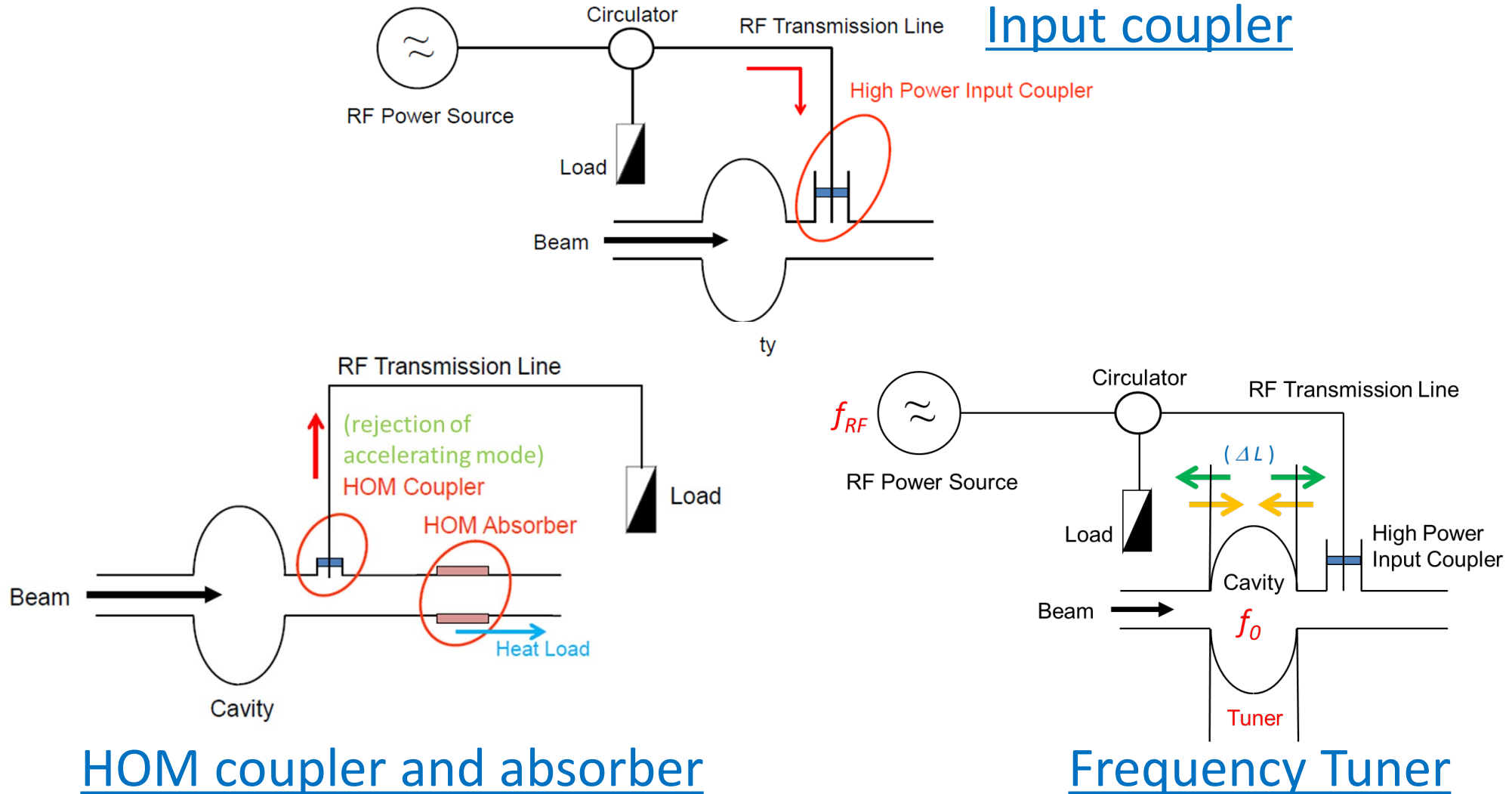
Cryomodule



STF Cryomodule

Cryogenic Efficiency

1 W at 2 K → 4.5 W at 4.2 K, (1 : 4.5)
 3 W at 4.2 K → AC 1 kW, (0.3%)
 ◆ AC 1.0 MW → 3 kW@4.2K, 700 W@2K

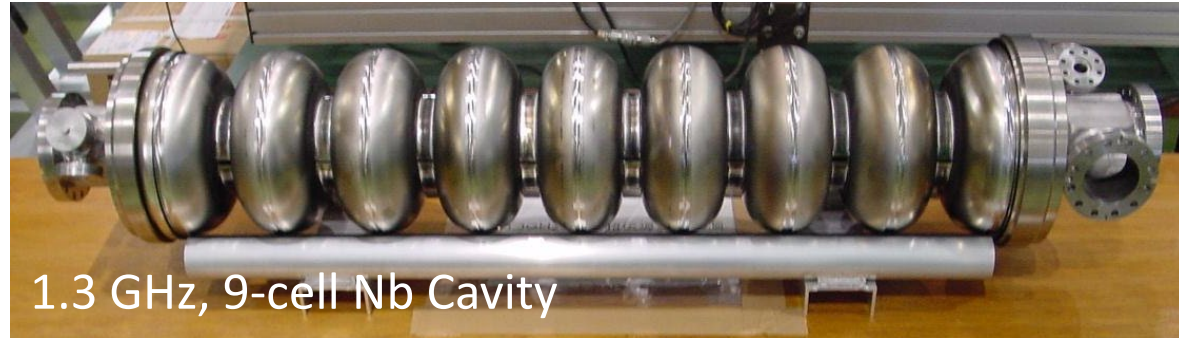


HOM coupler and absorber

Frequency Tuner



Input Coupler



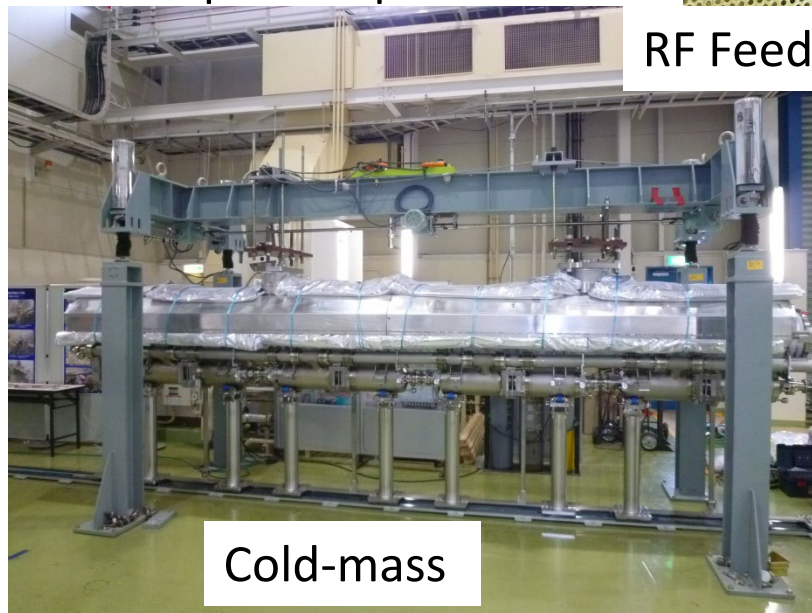
1.3 GHz, 9-cell Nb Cavity



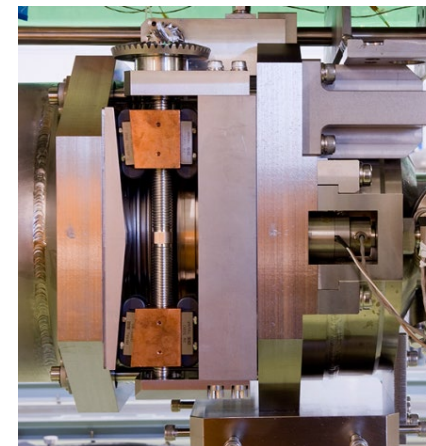
RF Feedthrough



HOM Coupler



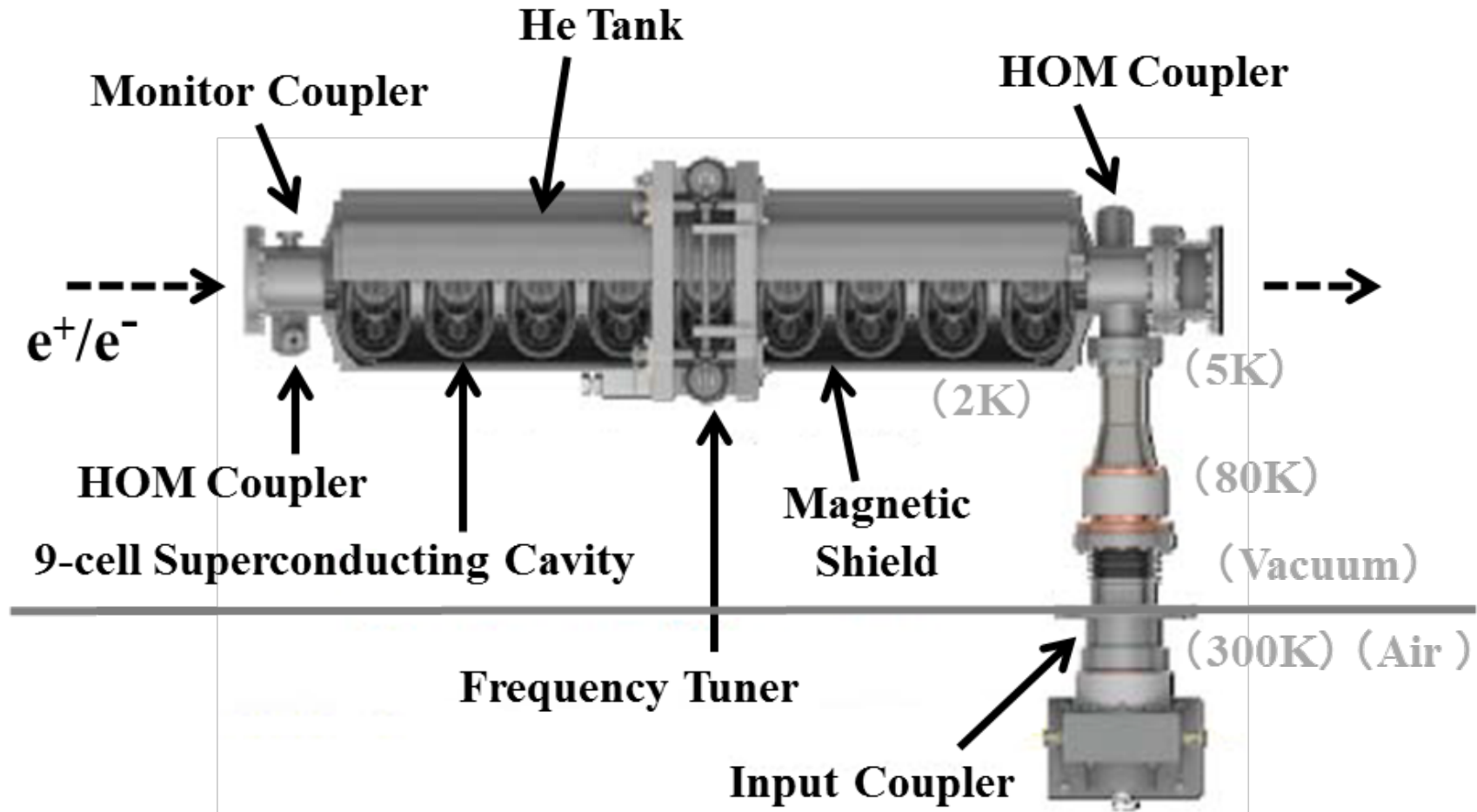
Cold-mass



Slide-Jack Tuner



Magnetic Shield
He Jacket (Ti)



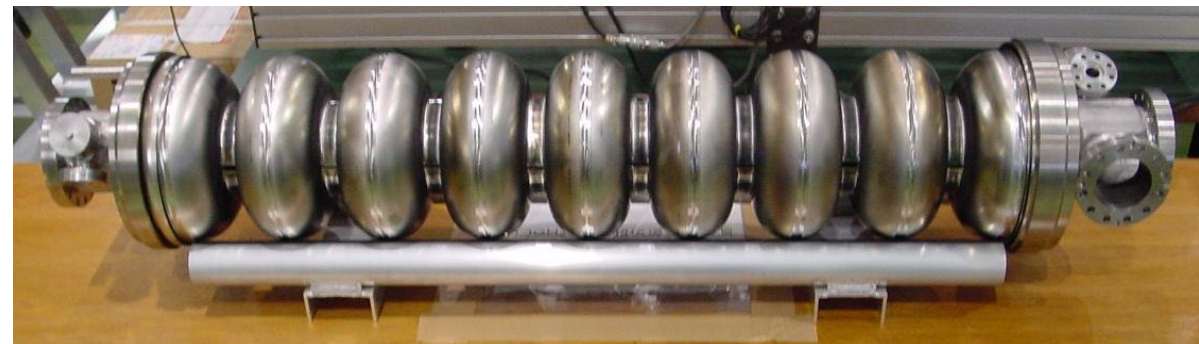
STF 9-cell SRF Cavity Package



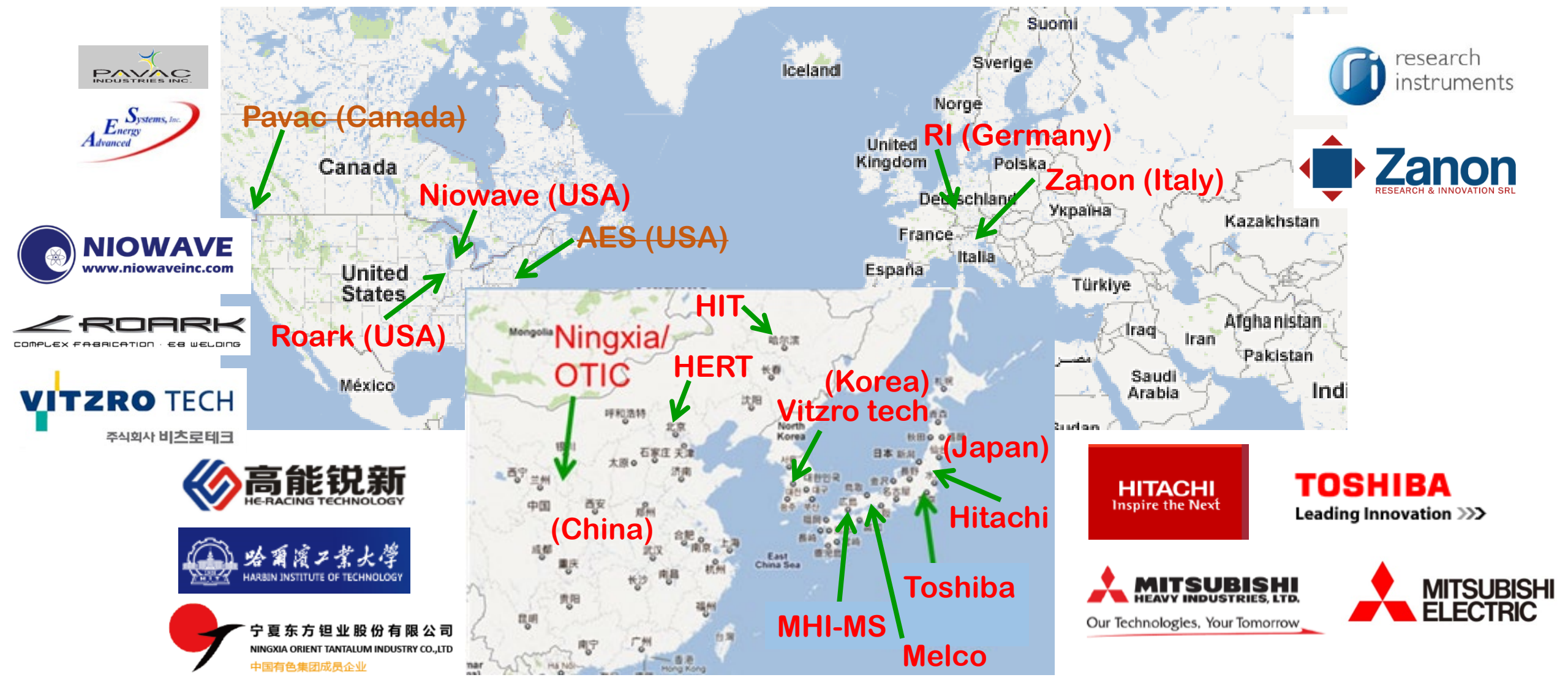
Center-cells (Tokyo Denkai ; RRR~300 Nb)



Forming and joining properties of Nb
(Deep drawing , EBW: electron beam welding)



Cavity fabrication companies in the world





Design

- RF analysis (HFSS, SUPERFISH, CST-MW)
- Mechanical analysis (ANSYS)
- Thermal analysis (ANSYS)
- Elastic-Plastic analysis (Deep-drawing)

Engineering

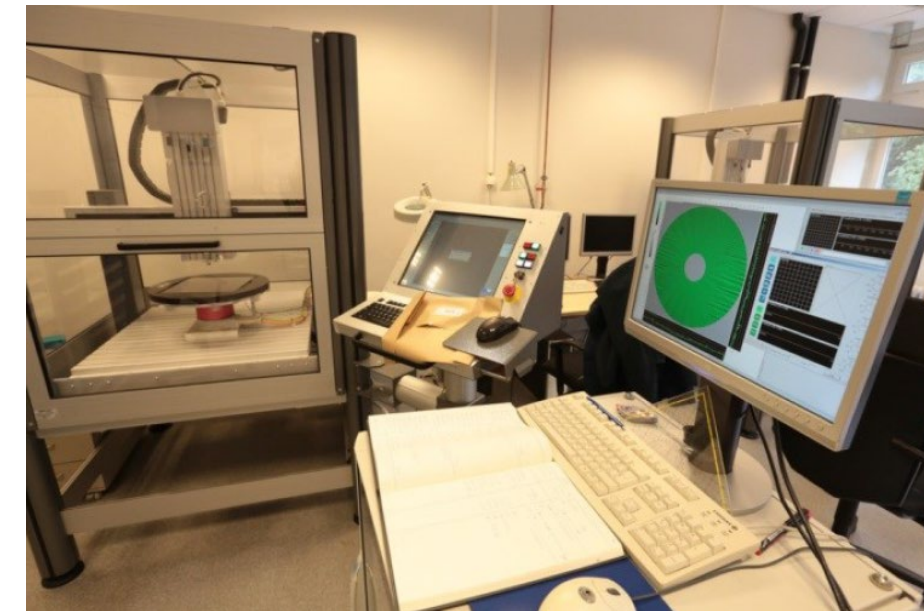
- Pressing
- Machining
- Chemical polishing
- Electron beam welding (EBW)
- Vacuum brazing

Assembly and Inspection

- Fabrication of special jigs
- Vacuum leak check
- Dimensional measurement
- RF measurement
- Frequency tuning
- Precise alignment

Special cavity fabrication tools developed by DESY

TESLA 1.3 GHz 9-cell cavity



Eddy current scan of Nb sheet



Frequency measurement
of half-cell/dumb-bell

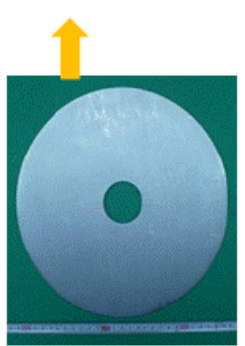
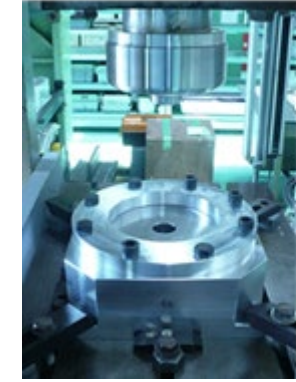
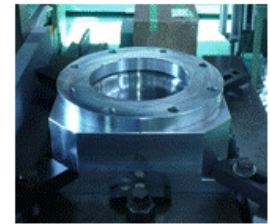
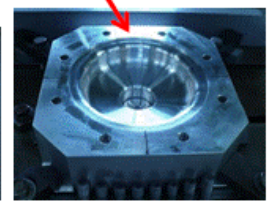
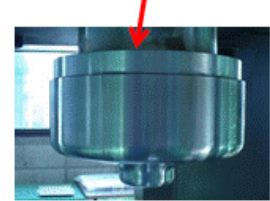


Automatic pre-tuning machine

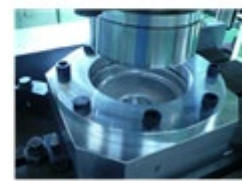
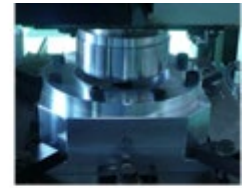
1. MHI's work for ERL (SRF Electron Gun)

Procedure of press of half-cells

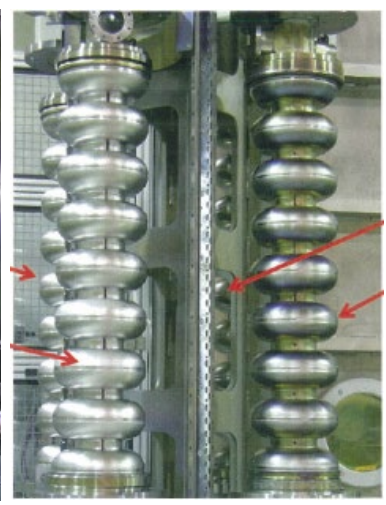
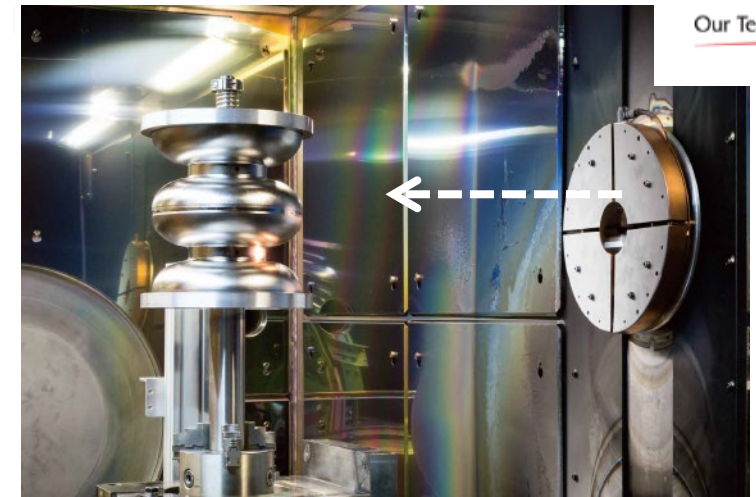
Before press
Deep Drawing
 (press forming)
 ↓
Trimming
 (machining)
 CP
 ↓
Joining
 (EBW)



In the middle of press



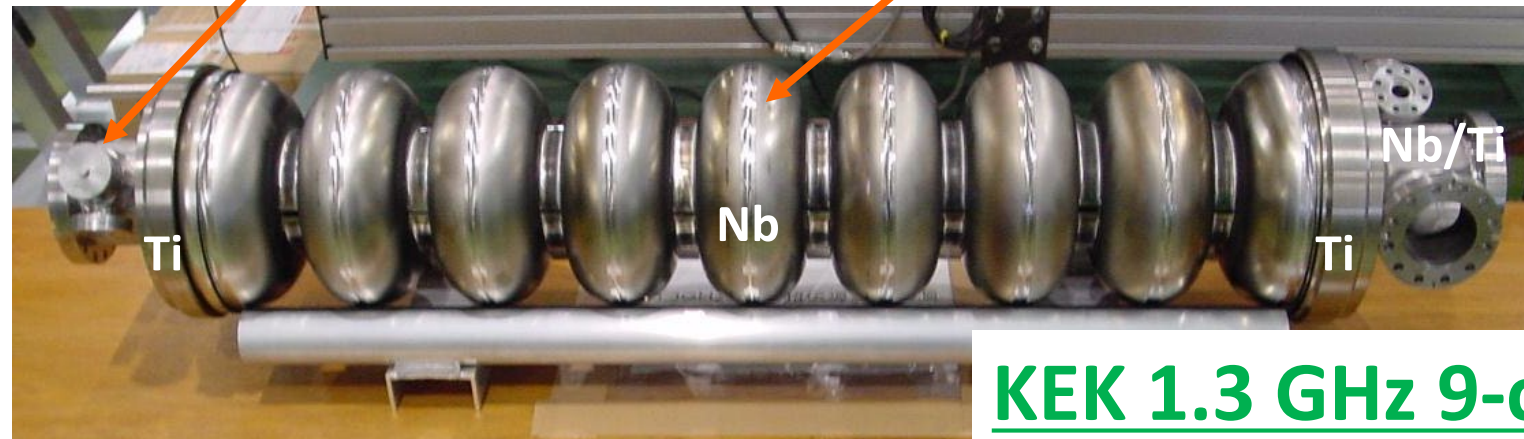
Electron Beam Welding (EBW)



by K. Sennyu (MHI-MS)

Special Technology
 4 x 9-cell cavities
 (all 36 EBW seams)
 per
 1 vac. Pumping
 at MHI-MS

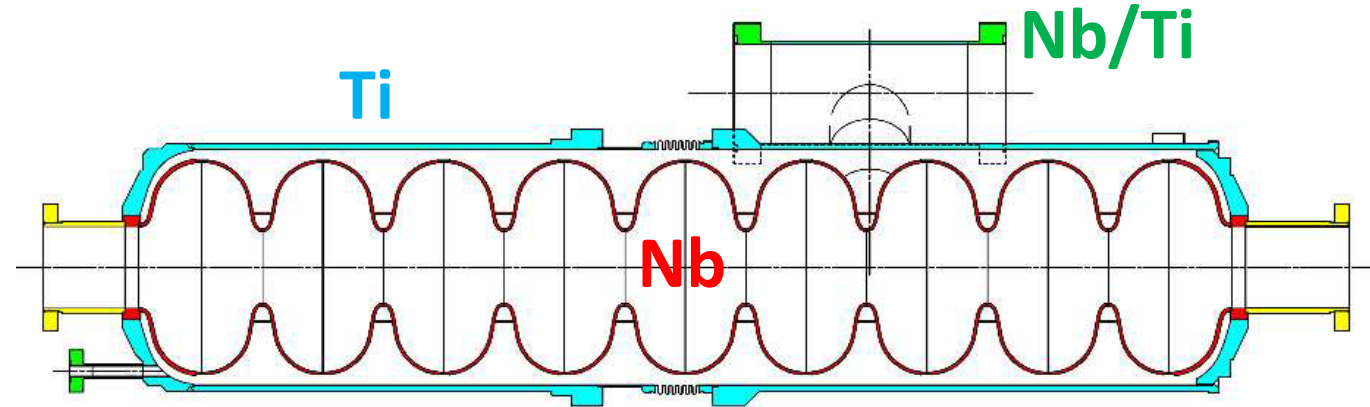
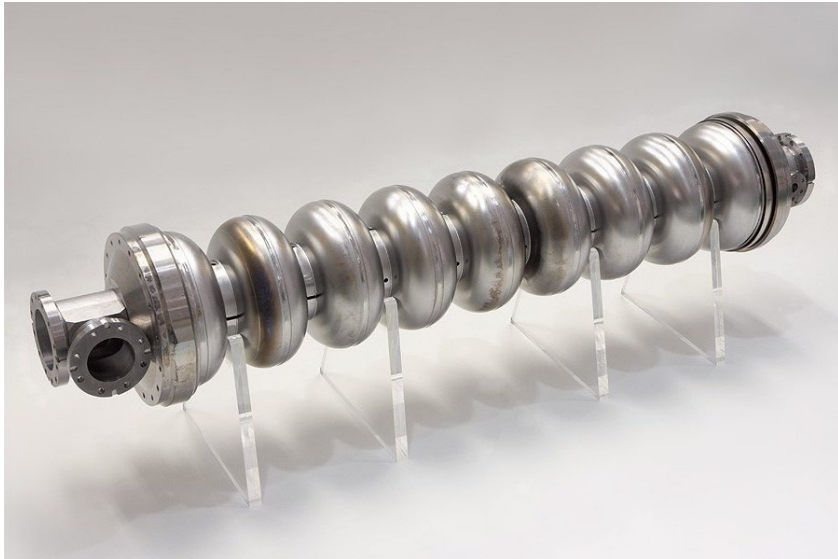
Cavity fabrication (EBW: electron beam welding)



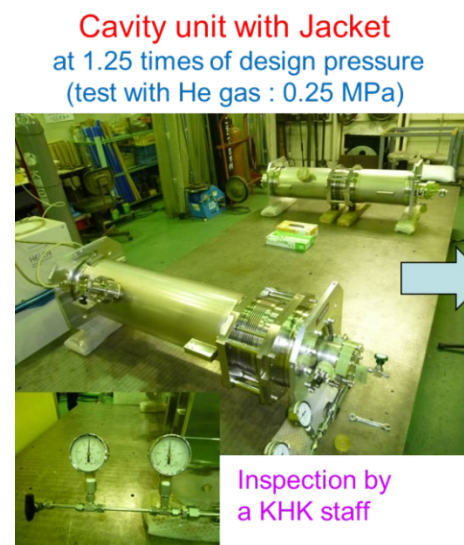
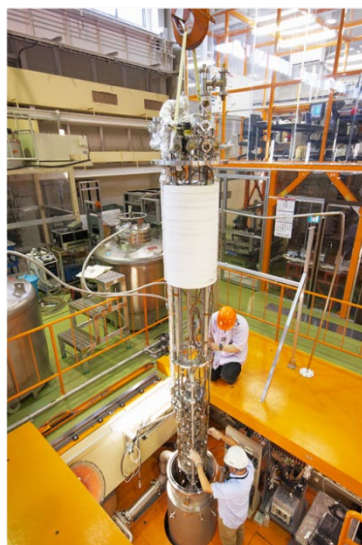
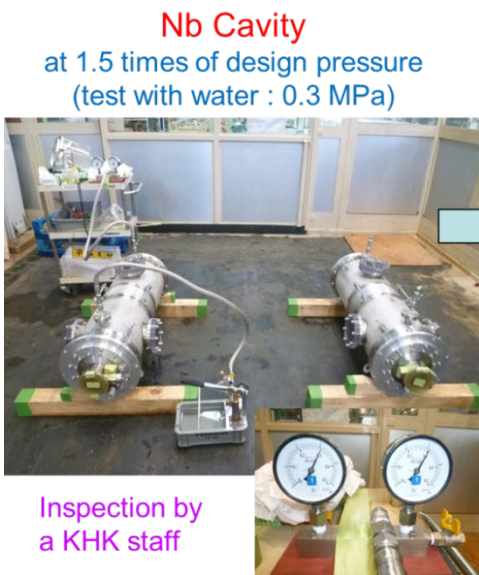
KEK 1.3 GHz 9-cell cavity



KEK 1.3 GHz 9-cell cavity



Materials	Joining Methods
Nb	(Cavity cells)
Ti	(He Tank)
Nb/Ti	(Flanges)
Nb - Nb Joining	EBW, LBW
Nb - Ti Joining	EBW
Ti - Ti Joining	TIG
Nb/Ti - Ti Joining	TIG
Nb/Ti - Nb Joining	EBW, LBW



Mechanical properties of Nb, Ti and Nb/Ti (EBW-joints)

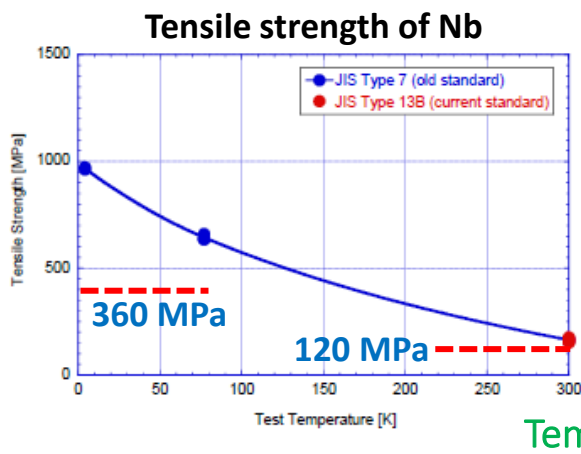


Fig. (5)a Tensile strength of Nb.

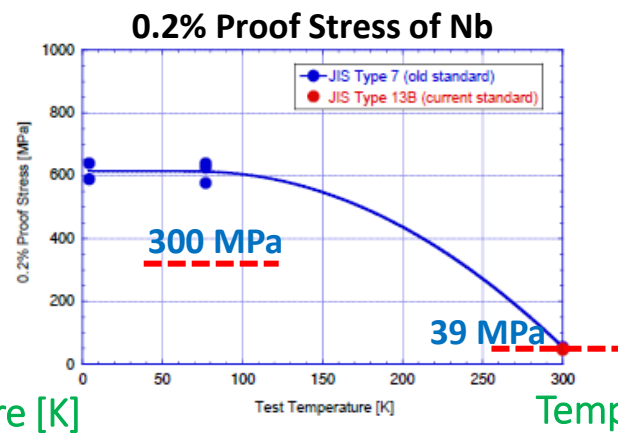


Fig. (5)b 0.2% proof stress of Nb.

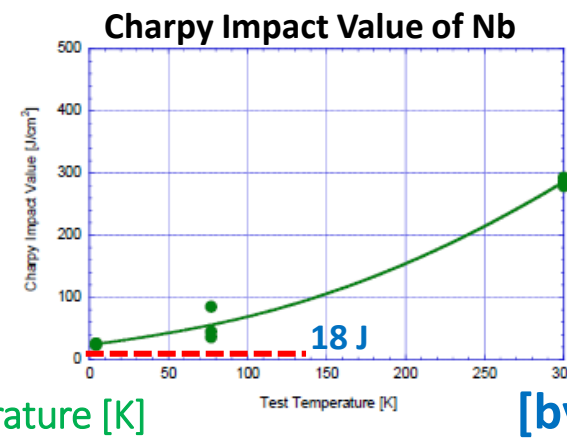


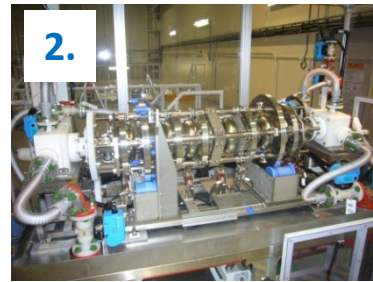
Fig. 5(b) Charpy impact value of Nb (10 mm wide).

[by H. Nakai (KEK)]

Surface treatment (smooth and clean)



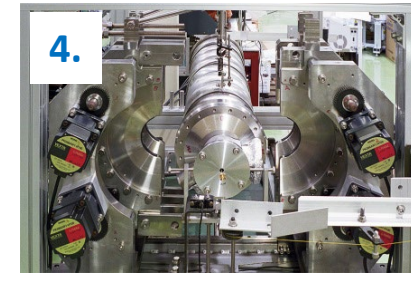
1. Inspection of inner surface



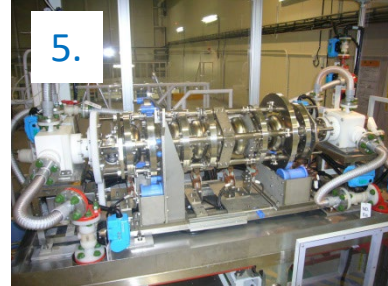
2. Pre-EP + EP-I (5+100 μm)



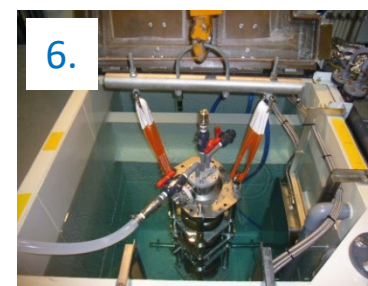
3. Anneal (750°C, 3h)



4. Pre-tuning (flatness, f_0)



5. EP-II (5~20 μm)



6. Hot bath rinsing with ultra-sonic



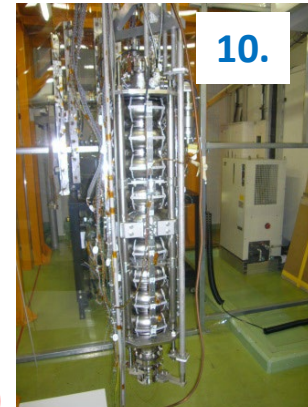
7. HPR



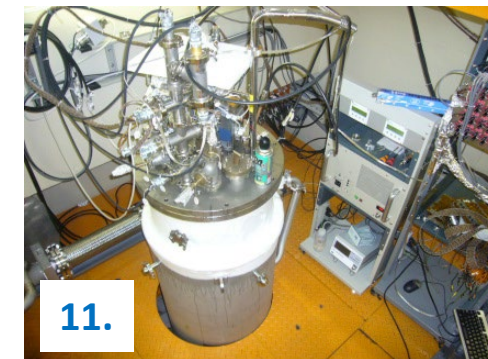
8. Assembly (Class 10)



9. Baking (120°C, 48h)



10. Hanging stand with T-map

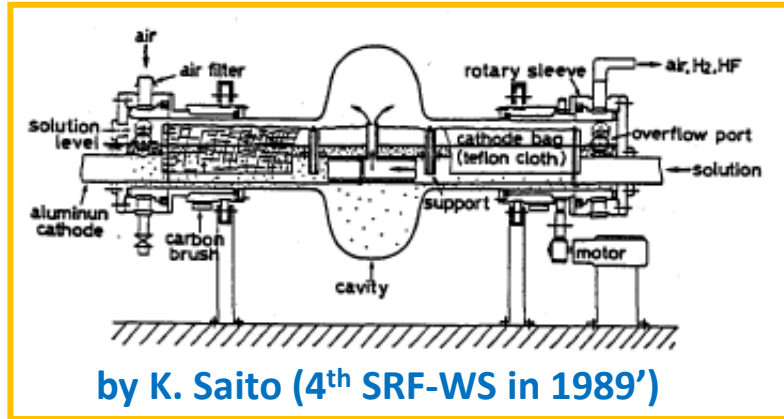


11. Vertical Test

Electro-polishing: EP



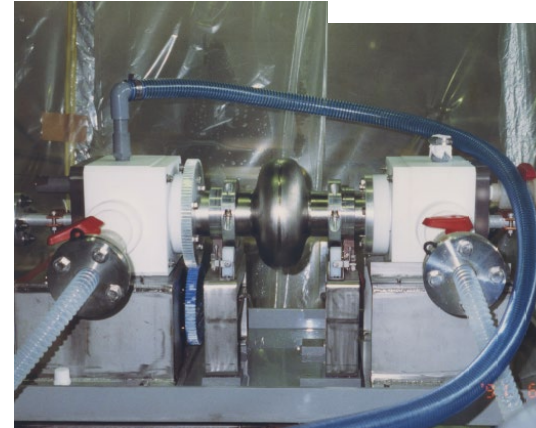
Electro-polishing Device



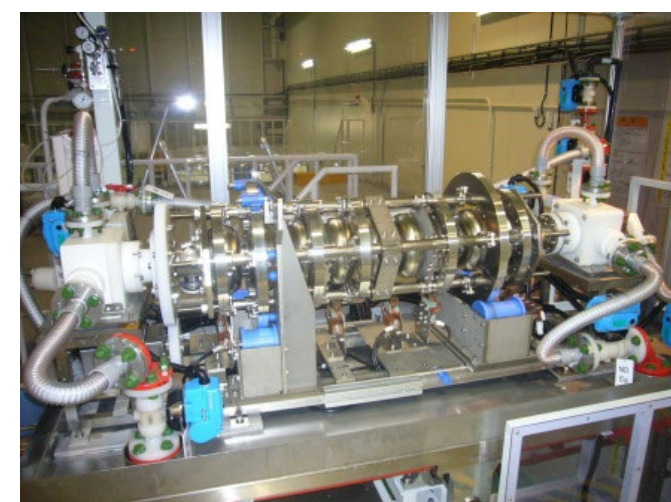
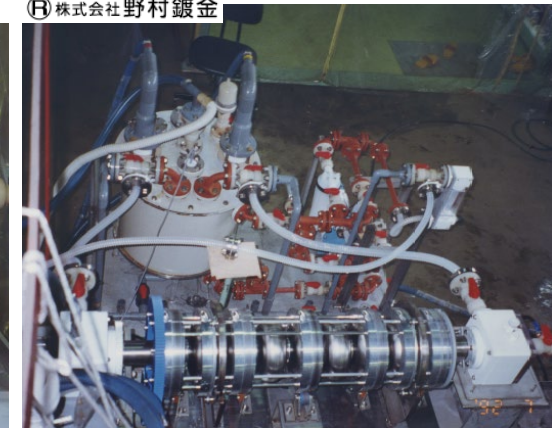
1993'

NOMURA PLATING

1998'

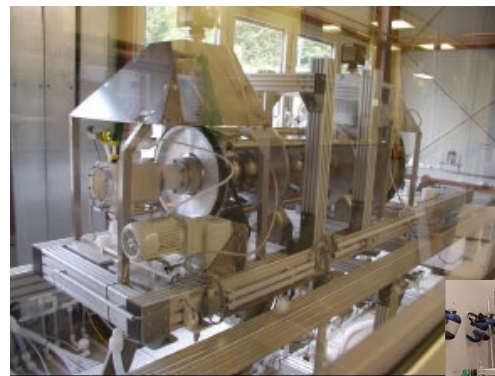


株式会社野村鍍金



2006'

STF/KEK

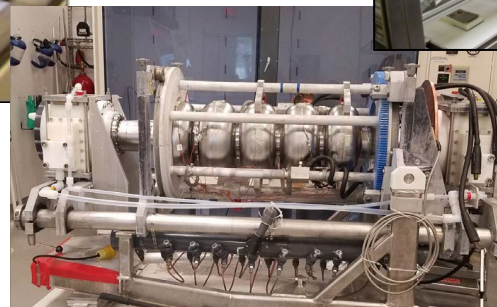


DESY

ANL/
FANL



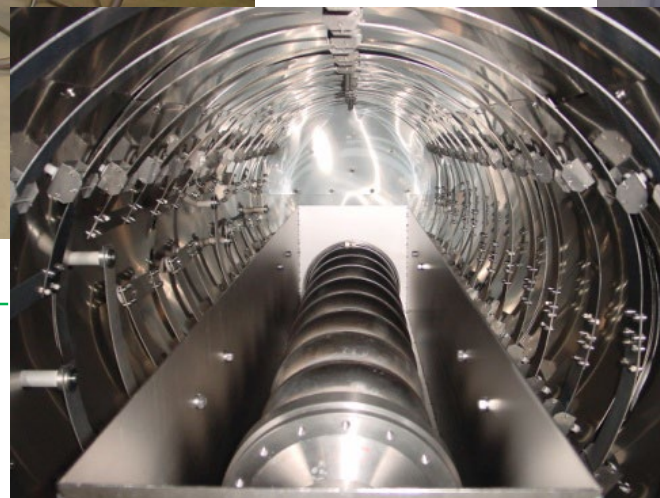
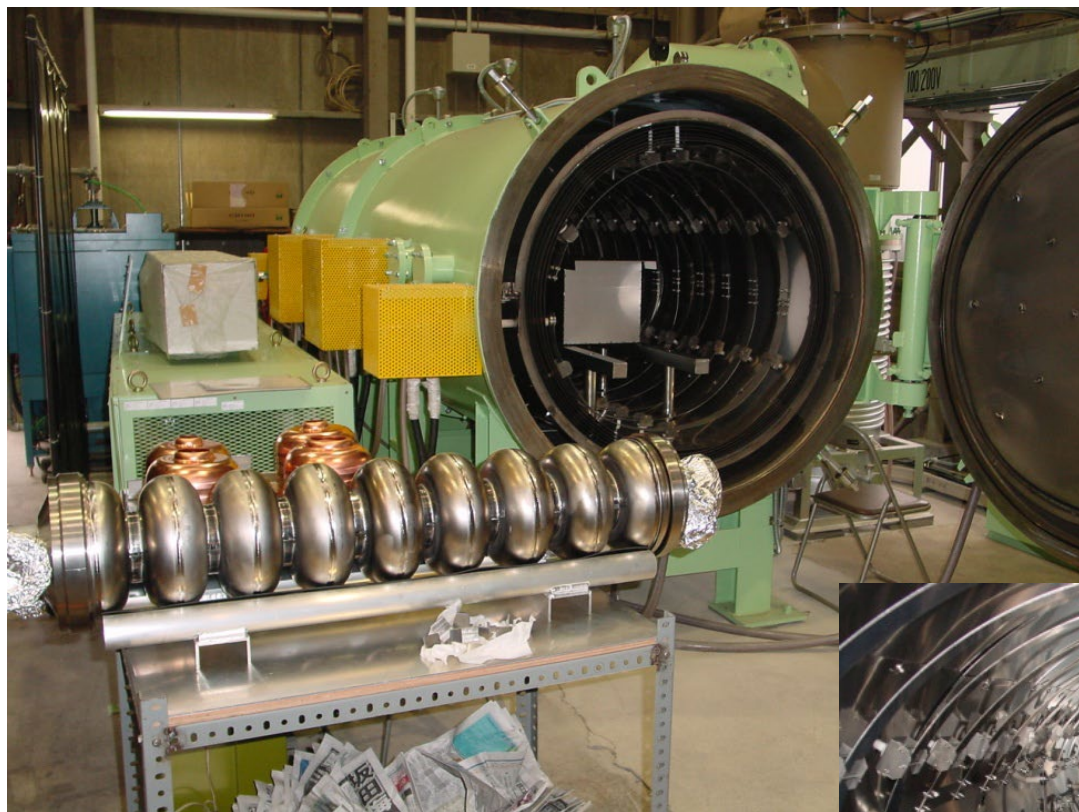
E. ZANON/DESY
 Ningxia/IHEP
 Wuxi/SINAP



JLab

RI/
DESY





Vacuum furnace with diffusion-pump
for hydrogen degassing:
max. temp. = 800 °C
1. x10⁻⁴ Pa at RT

New clean vacuum furnace with cryopump
for N-doping and N-infusion:
max. temp. = 1200 °C
1. x10⁻⁶ Pa at RT

High pressure rinsing: HPR



HPR-1 at STF



HPR-2 at COI

Nozzle: fixed
Cavity: rotation, up/down

Nozzle: rotation
Cavity: up/down

Pressure = 8 MPa
Purity = 18 MΩ · cm

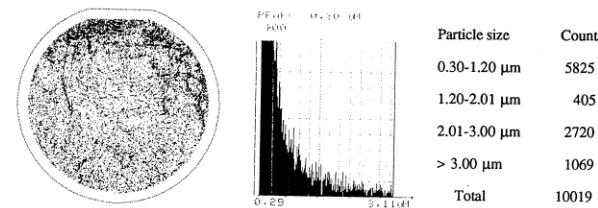


Fig. 6 Residual particles on a wafer surface after the TRISTAN final rinsing.

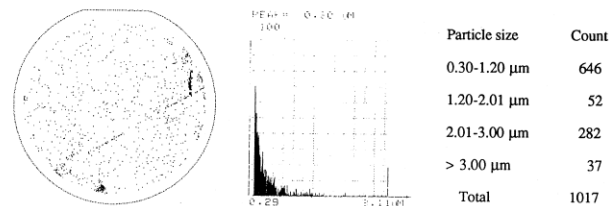


Fig. 7 Residual particle on a wafer surface after HPR. **by K. Saito (SRF91')**

Cleanroom Assembly (class-10, ISO-4)



- Parts cleaning
- UPW rinsing
- Ultra-sonic bath
- Ionized gun
- Particle counter
- Ar gas flow

Question (4)



What is the essential technologies for achieving higher cavity performance?



What is the essential technologies for achieving higher cavity performance?

Essential technologies for higher performance:

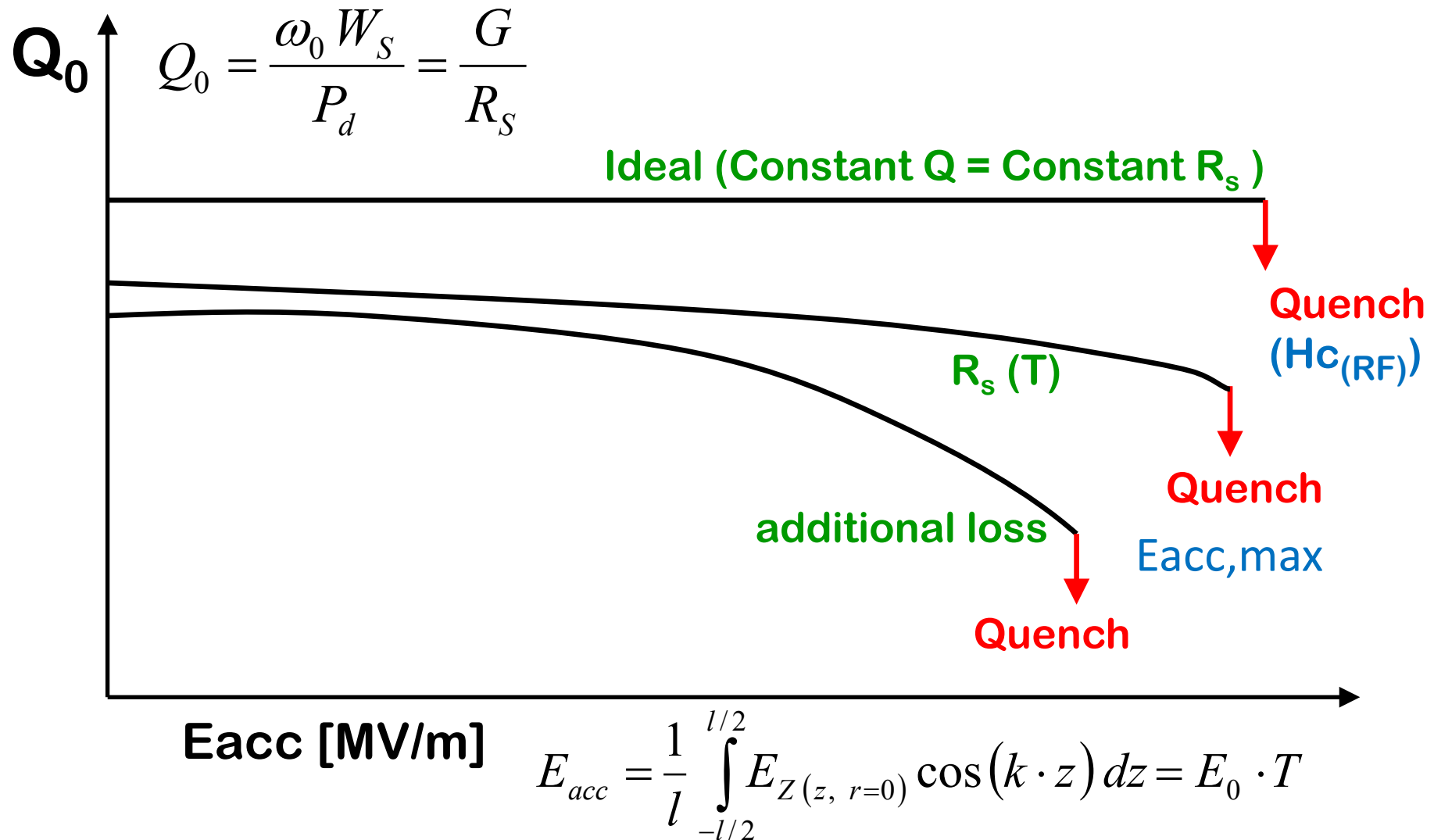
- **Smooth Surface**
- **Clean Surface**
- **Clean Environment**

To achieve higher performance

- avoid **Thermal Quench** caused by surface defects
- suppress **Field Emission** due to dust contamination

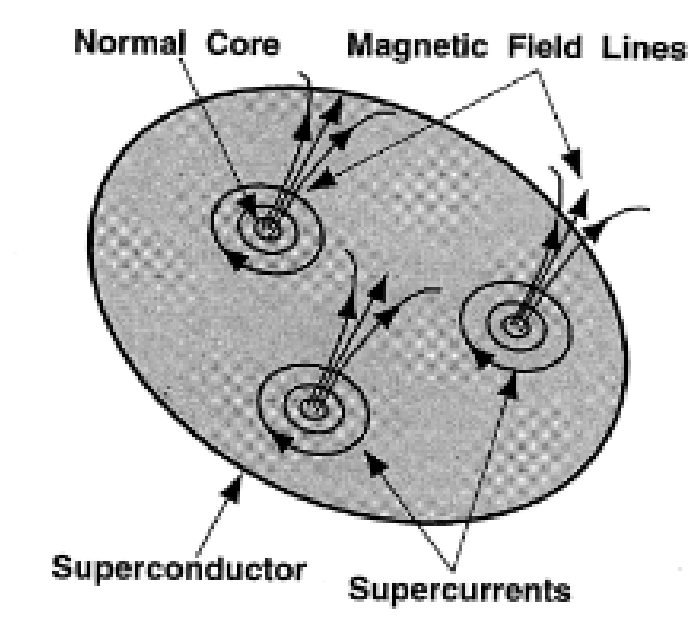


1. Introduction
2. Fundamental of SRF Cavity
3. Overview of SRF Cavity System
4. Fabrication and Surface Preparation
- 5. Cavity Performances**
6. Summary





- High purity Nb material (Fine-grain, Large-grain)
- Forming (Hydroforming, Deep drawing, Spinning)
- Joining (EBW, TIG, LBW, Brazing,)
- Surface removal treatment (CP, EP)
- Rinsing (Detergent, Ultra-pure water, US, HPR)
- Clean room environment
- Assembly procedure



Experiment to investigate shielding
effect of residual magnetic field

(0.3 nΩ / mGauss)

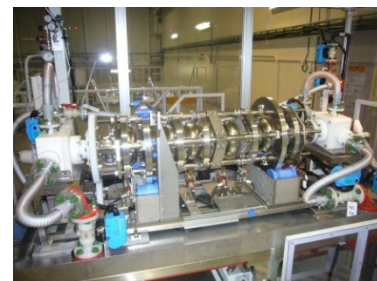
This sensitivity is strongly dependent
on the surface condition.

Residual magnetic field is one of main causes of residual surface resistance, because magnetic fluxes in a normal conducting state are trapped when a transition to superconducting state occurs in a niobium cavity.

Surface preparation : indispensable preparation



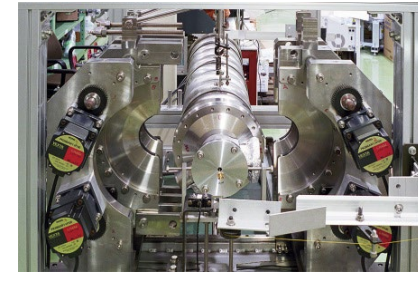
Inspection of inner surface



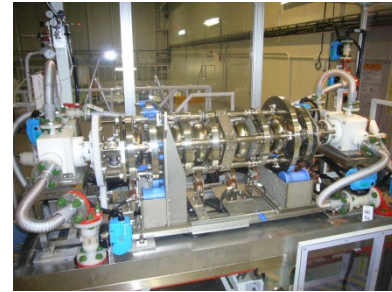
Pre-EP + EP-I (5+100 mm)



Anneal (750°C, 3h)



Hot bath rinsing by ultra-sonic agitation with ultra-pure water



EP-II (5~20 mm)



Suppression of Field Emission

- Rinsing by ultra-pure water
- Assembly in class-10 clean room



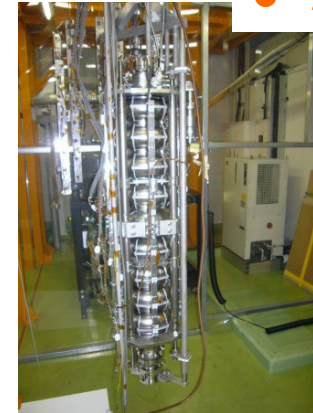
HPR



Assembly (Class 10)



Baking (120°C, 48h) (Class 1000)

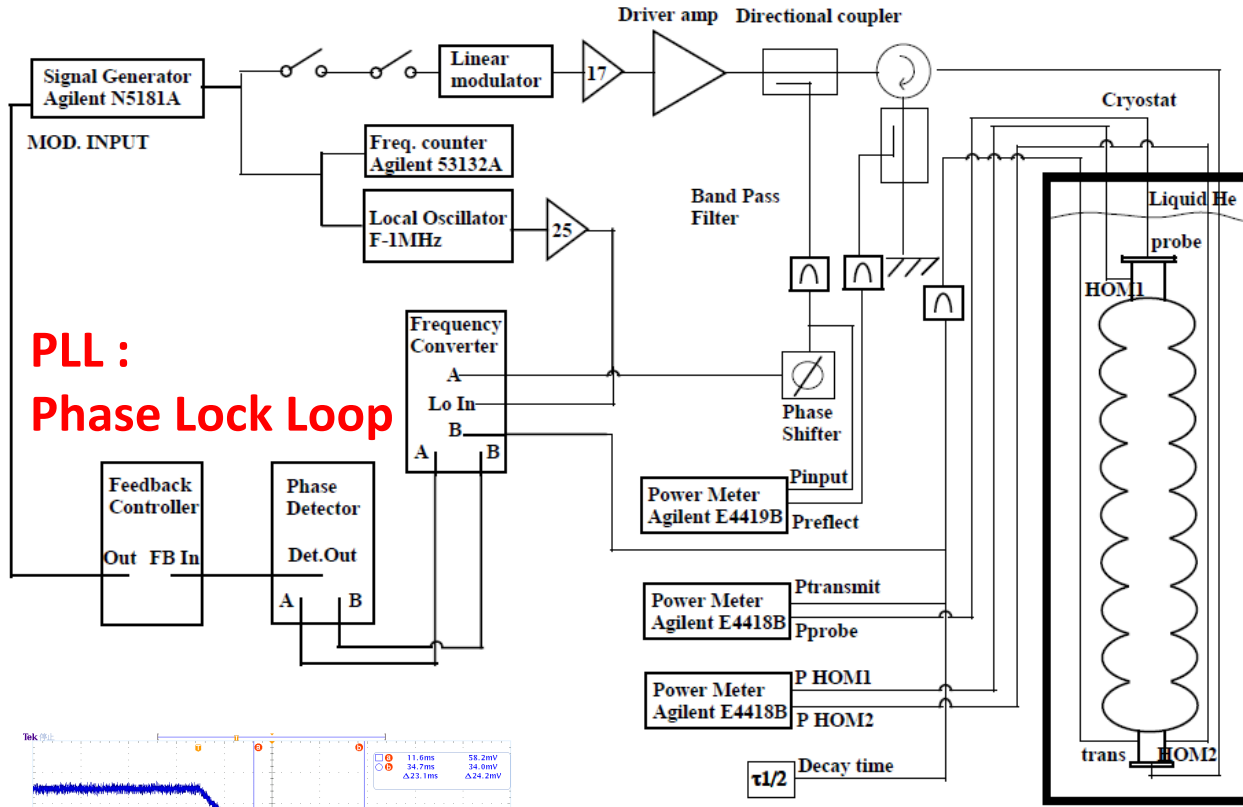


Hanging stand with T-map

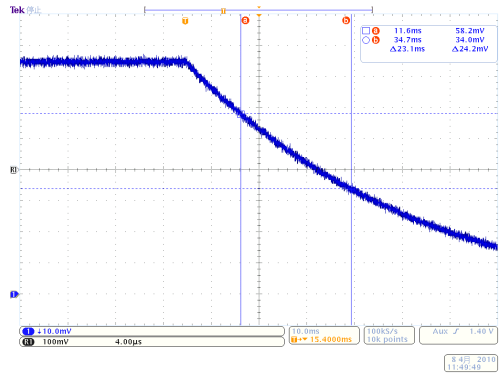


Vertical Test

RF system for Vertical Tests : VT

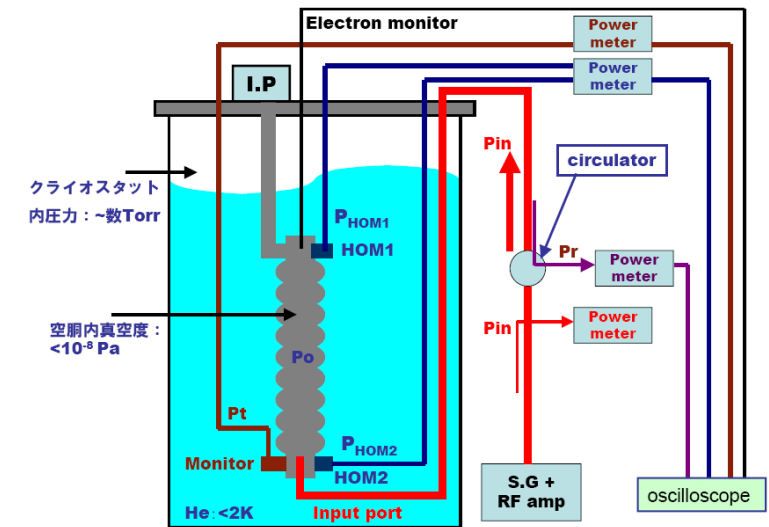


**PLL :
Phase Lock Loop**



$$Q_L = 2 \pi f_o \cdot \tau_{1/2} / \log_e 2$$

($\tau_{1/2}$: decay time of P_t)



$$P_o = P_{in} - P_{ref} - P_{ext}$$

$$\beta^* = \frac{1 \pm \sqrt{P_{ref}/P_{in}}}{1 \mp \sqrt{P_{ref}/P_{in}}}$$

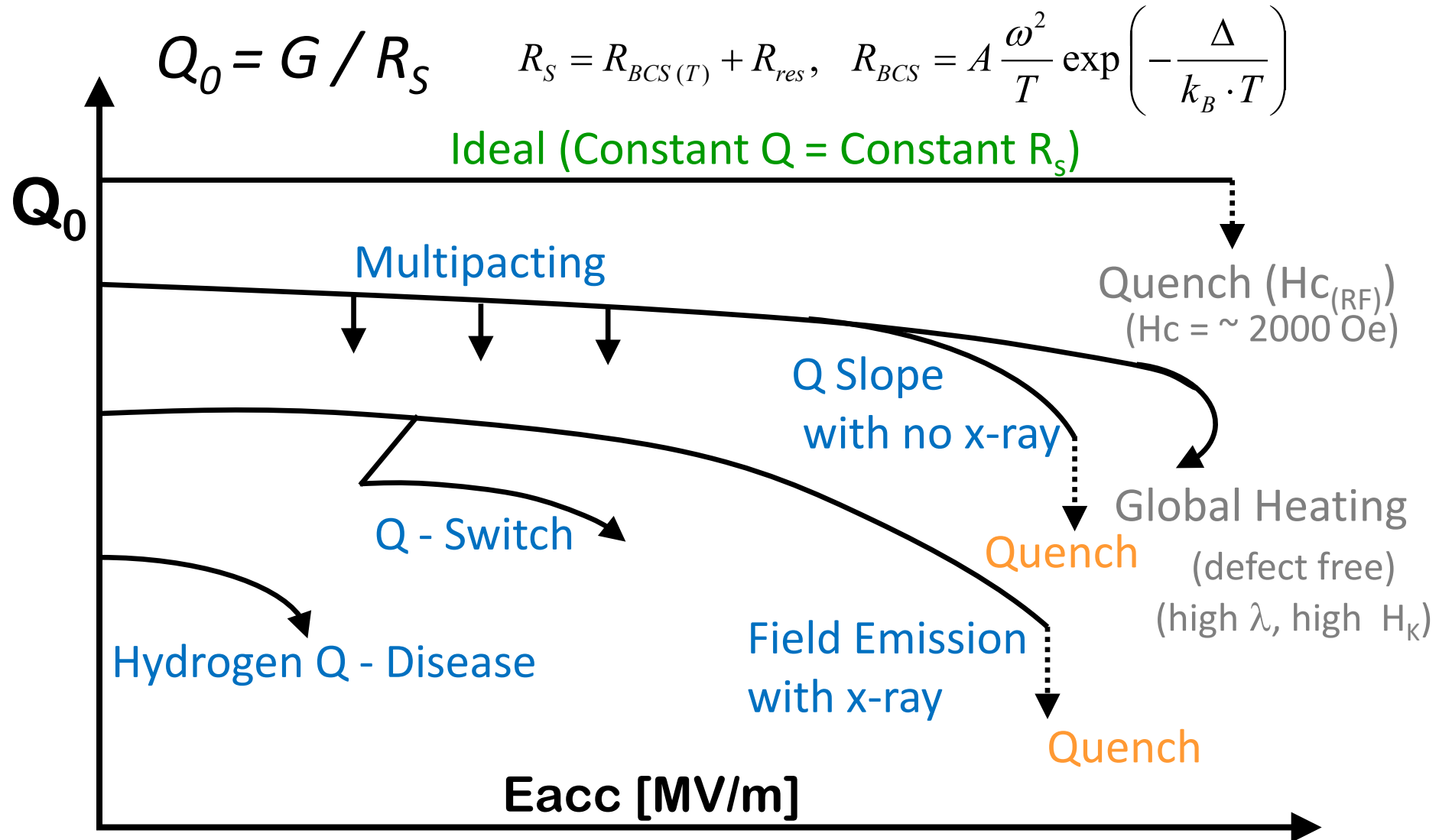
$$\beta_{in} = \beta^* \cdot (1 + \beta_{ext})$$

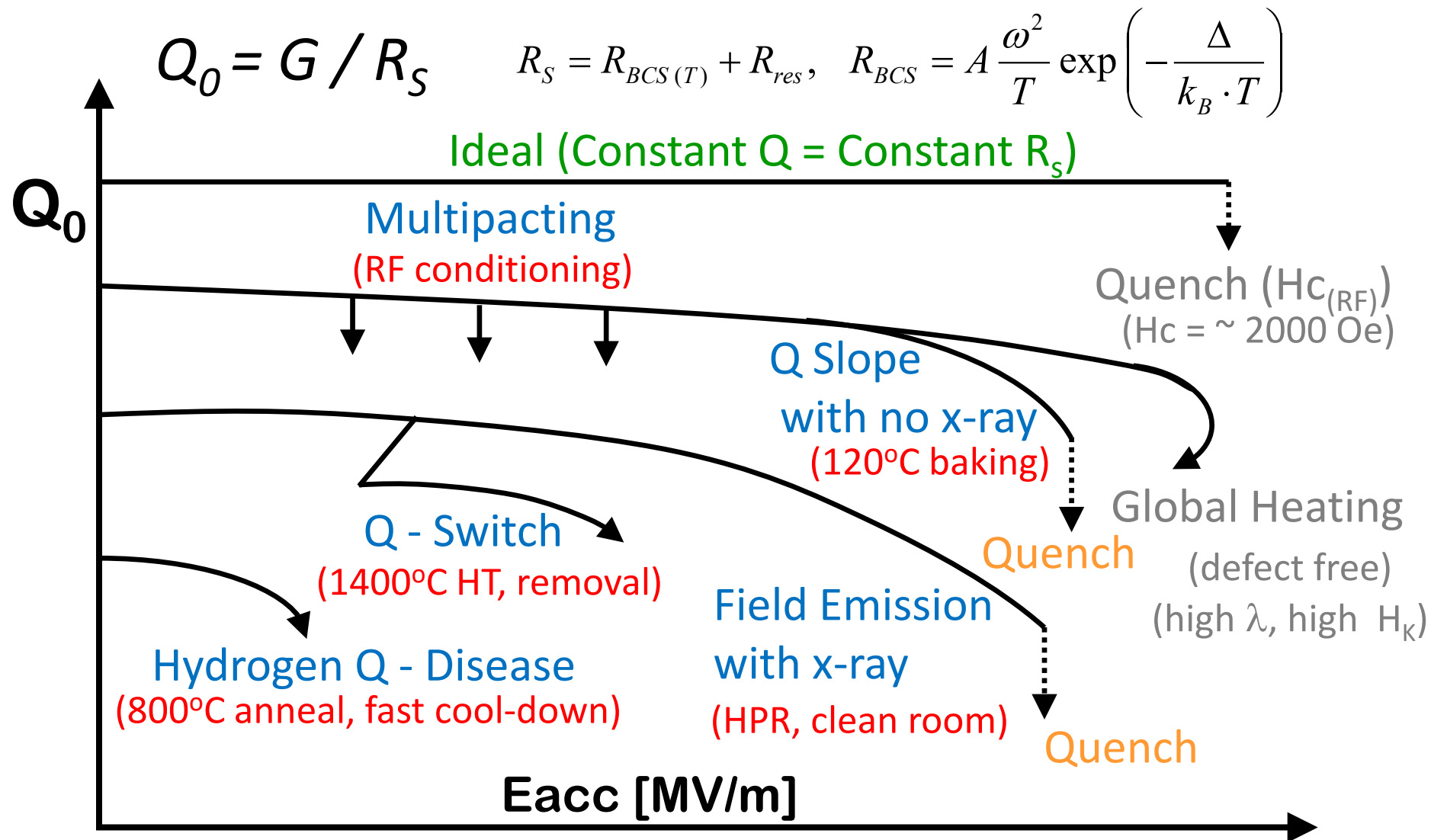
$$\beta_{ext} = P_{ext} / P_o$$

$$Q_o = Q_L \cdot (1 + \beta_{in} + \beta_{ext})$$

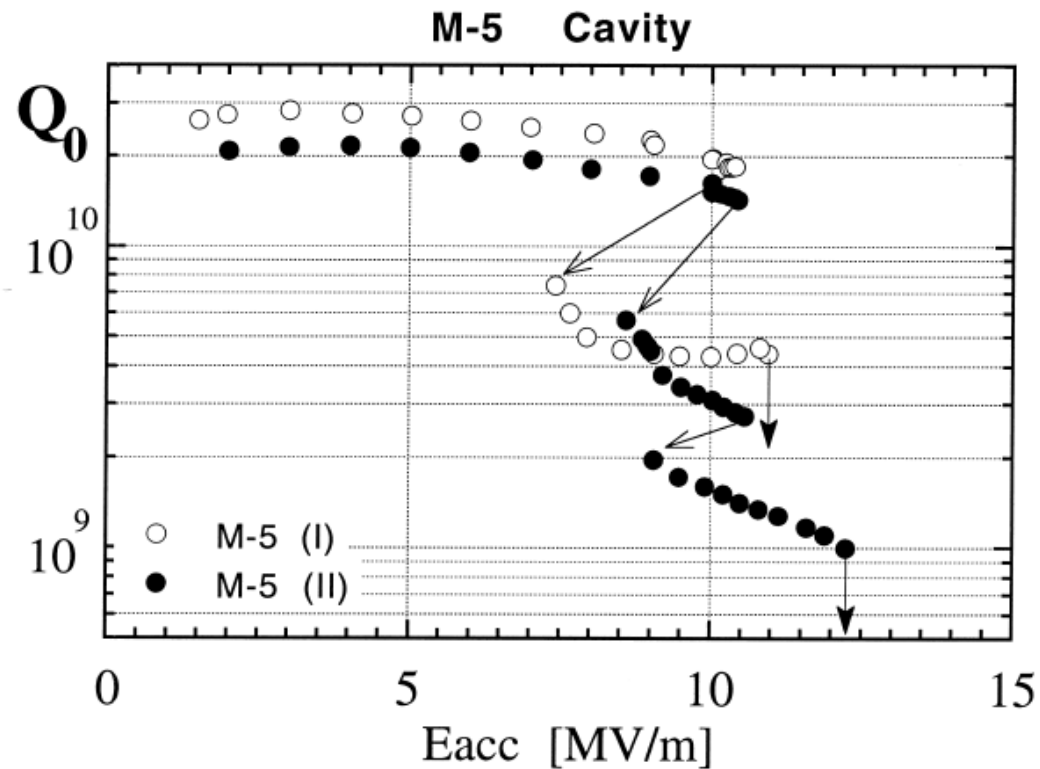
$$Q_{ext} = P_o \cdot Q_o / P_{ext}$$

Phenomena limiting cavity performance





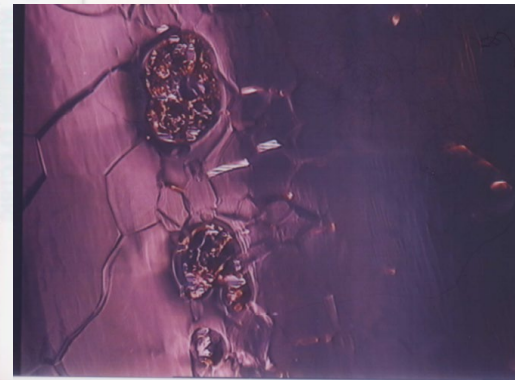
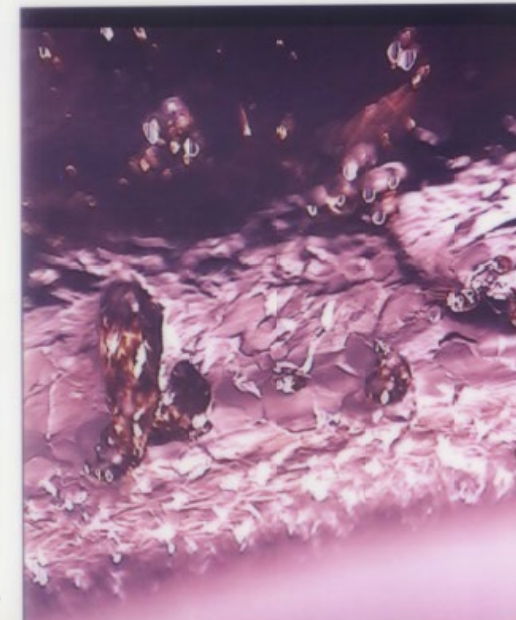
Q - Switch



The Q-Switch is caused by heating due to the transition from an SC state to a NC state at **thermally isolated defects**.

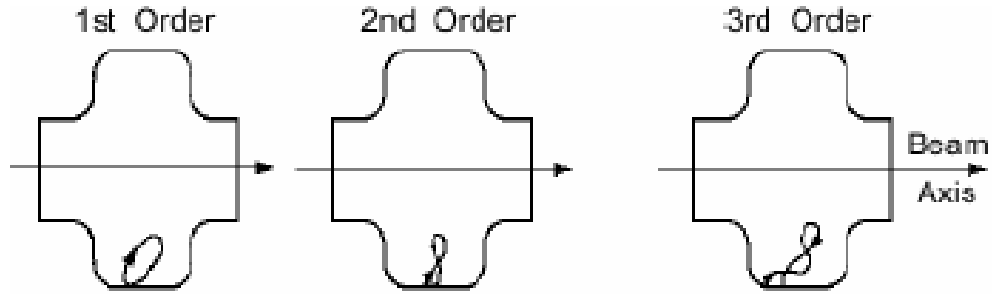
Typically, around iris region, where surface currents are lower.

M - 5 Cavity ; Quench Location
EBW seam at lower Iris
Sputtering balls / welding imperfections



← 1 2 3 4 [mm] →

C-1 Cavity ; iris EBW ($\theta = 30^\circ$)

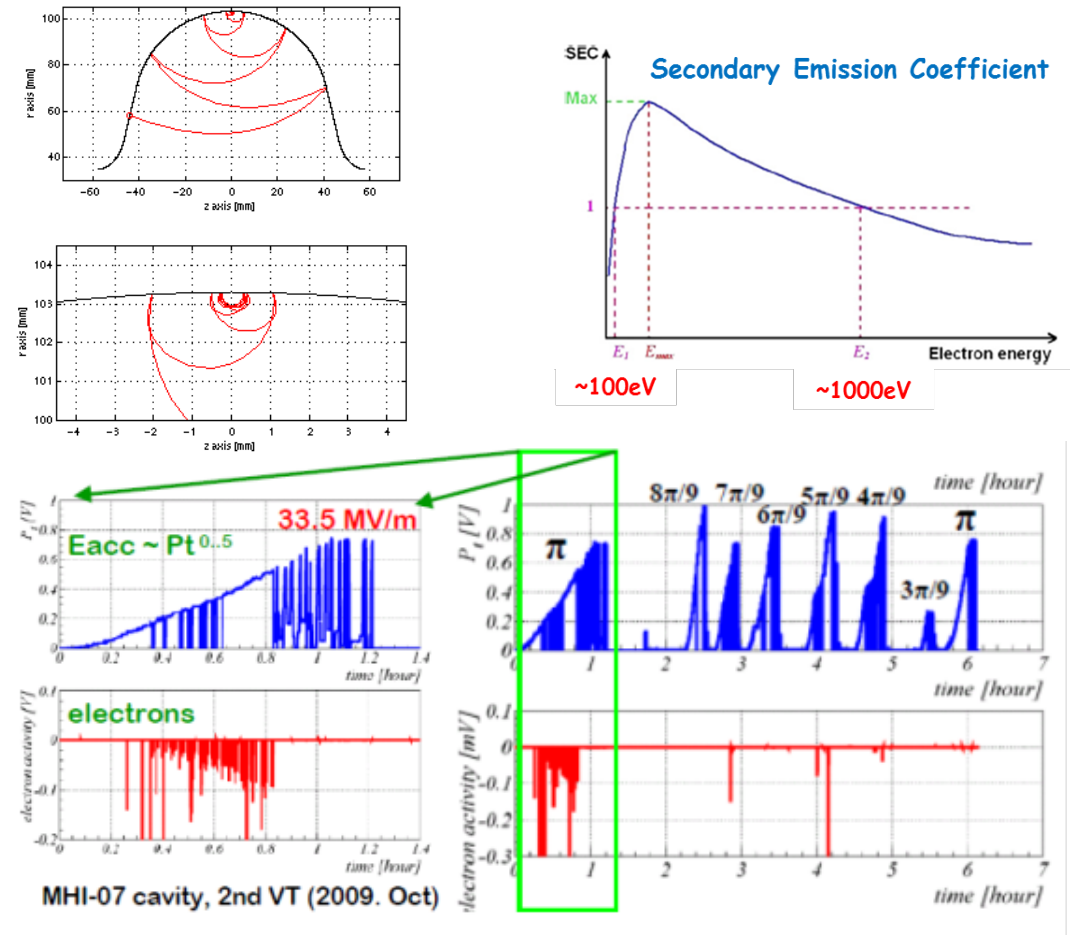


Multipacting at equator region

Multipacting is a low RF power, **electron multiplication based on resonance breakdown** phenomenon in vacuum. For a cavity shape such as a pill-box cavity, the cavity performance is frequently limited by a multipacting phenomenon around the equator region. A spherical cell shape is usually used for actual SRF cavities to suppress the multipacting phenomenon by **eliminating a flat region** around the equator. In the design of the cell shape, the ease of forming processes and rinsing procedures for cleaning should also be considered.

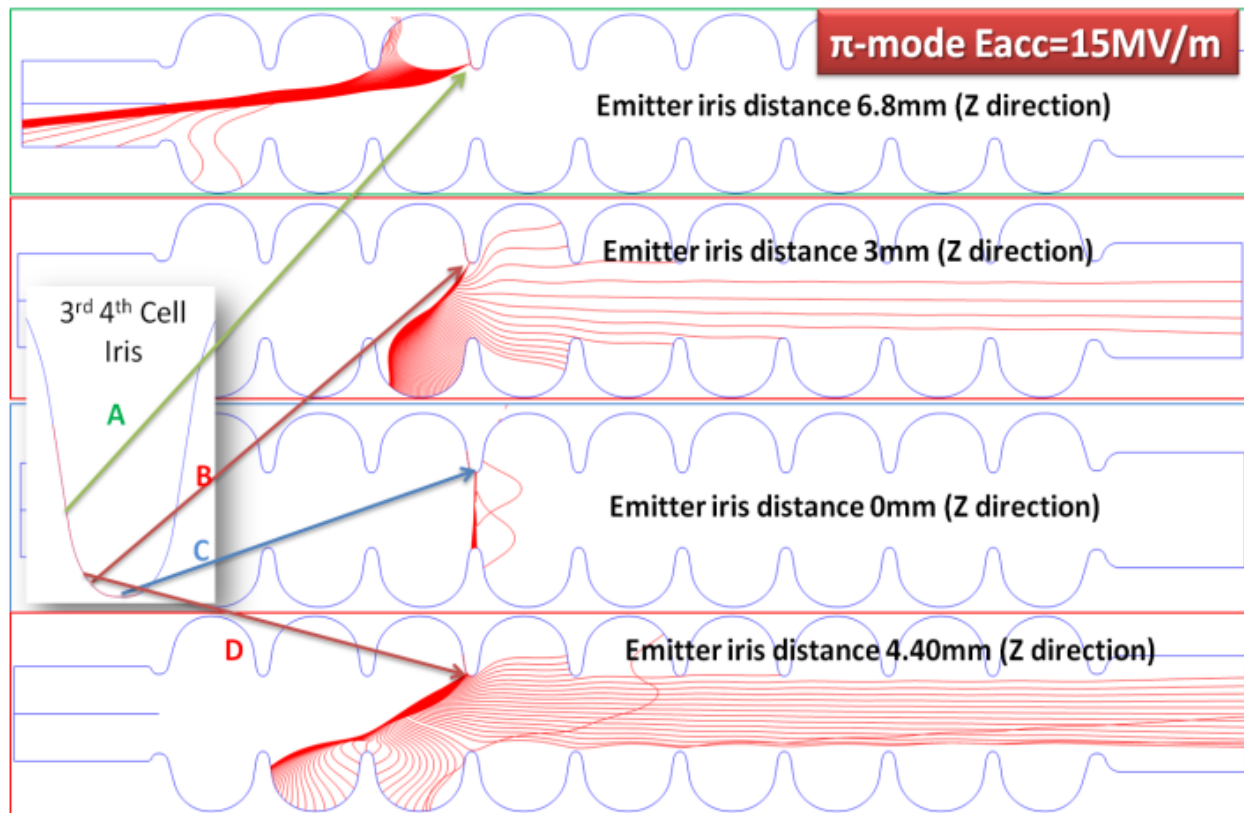
Multipacting (Clean surface is essential.)

Multipacting is usually processed-out by RF conditioning.





TM010-mode



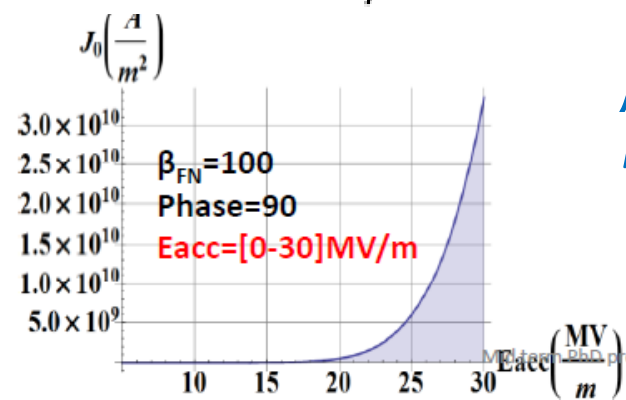
[Thesis by E. Cenri (KEK)]

Source of field emitted electrons

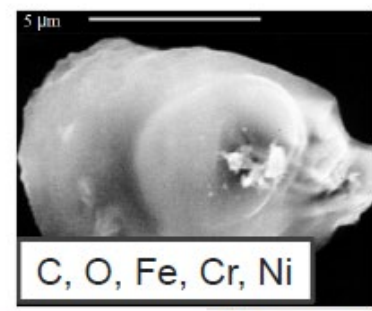
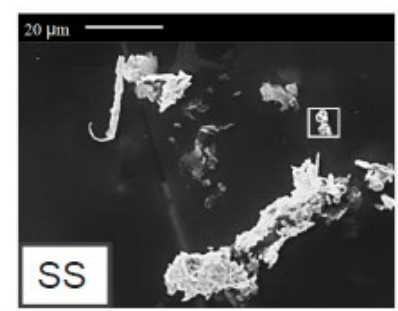
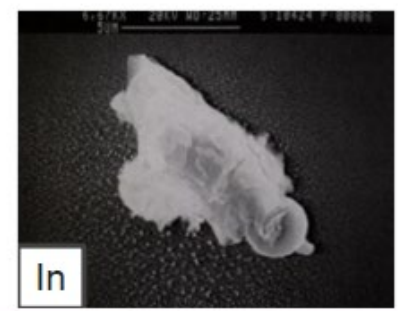
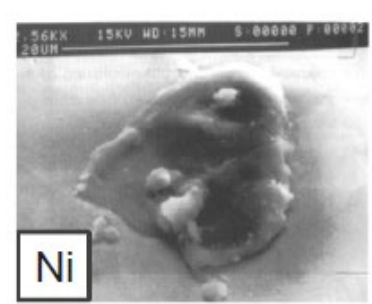
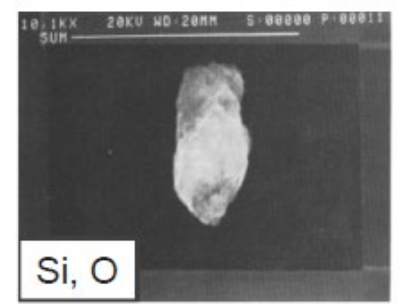
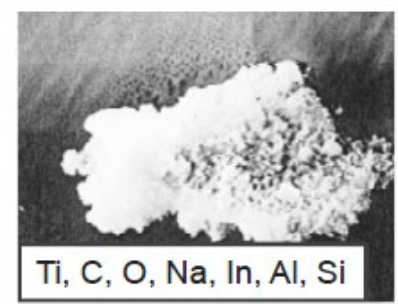
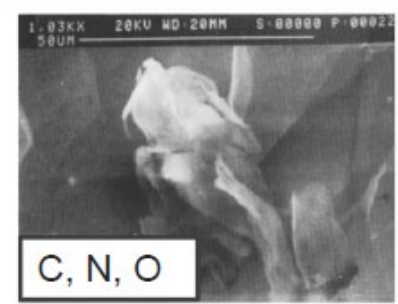
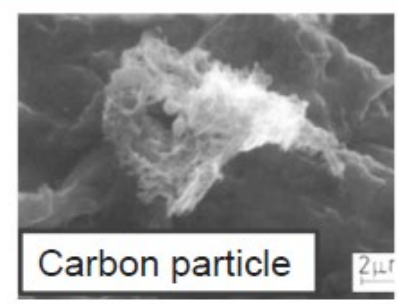


Fowler – Nordheim Equation

$$J = \frac{A_{FN} (\beta_{FN} E_{surf}(t))^2}{\phi} e^{\frac{-B_{FN} \phi^{1.5}}{(\beta_{FN} E_{surf}(t))}} \left[\frac{A}{m^2} \right]$$



β_{FN} : field enhancement factor
 E_{surf} : surface electric field
 ϕ : work function of Nb



[by M. Martinello (FNAL)]

5/18/2017 Martina Martinello | IPAC 2017



Application from semiconductor industries to accelerator technologies.

The Evolution of Silicon Wafer Cleaning Technology

Werner Kern*

Lam Research Corporation, Advanced Research Center, San Diego, California 92126

J. Electrochem. Soc., Vol. 137, No. 6, June 1990 © The Electrochemical Society, Inc.

High-pressure fluid jet cleaning consists of a high-velocity jet of liquid sweeping over the surface at pressures of up to 4000 psi (55, 56). The liquid can be DI water or organic solvents. The shear forces effectively dislodge submicron particles and penetrate into dense topography, but damage to the wafer can result with improperly adjusted pressure (18).

[Ph. Bernard, EPAC'92 at Berlin]

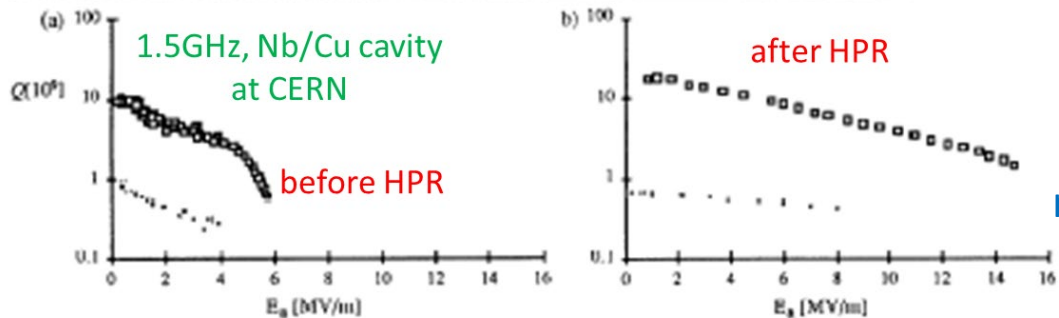


Figure 1. Q-value vs accelerating field for the fundamental mode at 4.2 K (lower) and 1.6 K (upper), a) before and b) after high-pressure water rinsing.

[P. Kneisel, SRF'93 at JLab]

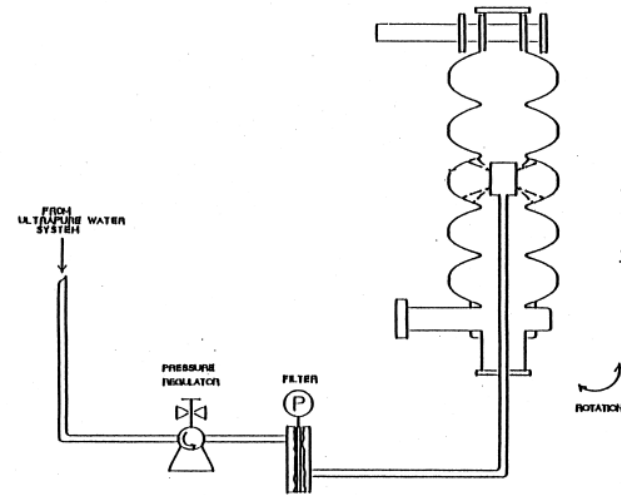


Figure 1 : Schematic of High Pressure Rinsing System

Experimental results of performance recovery by high pressure water rinsing
Demonstration of the effectiveness of HPR

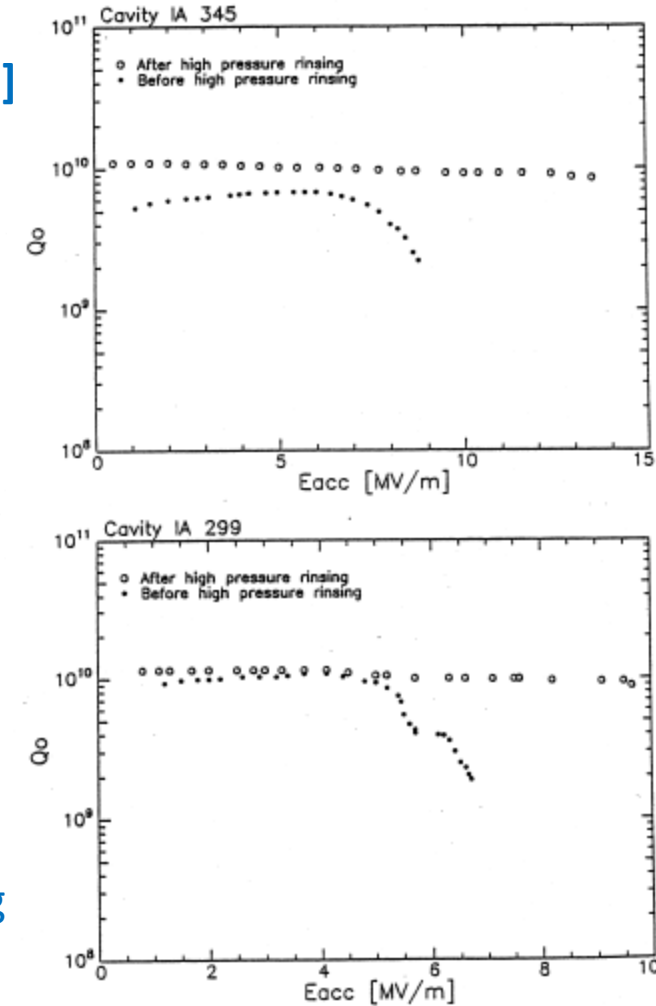
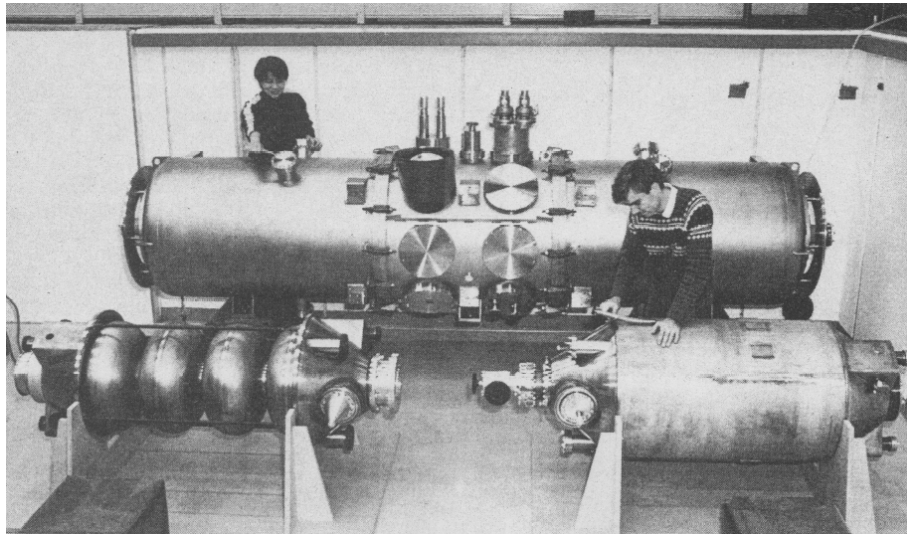


Figure 3 : Results of Production Cavity Pair IA345/IA299 before and after High Pressure Rinsing (measurements have been



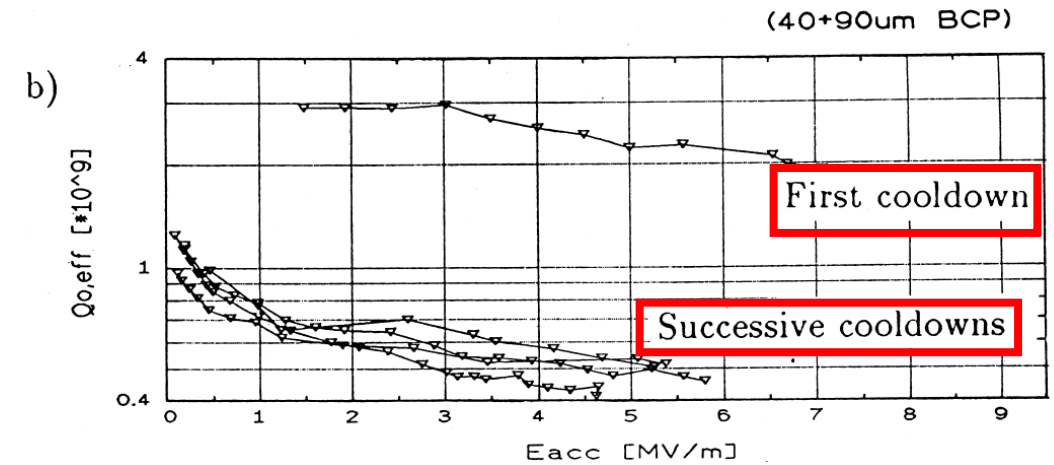
HERA cavities and cryomodule (in 1991 at DESY)

Heat capacity in the cryomodule is large, so that the fast cooling like vertical tests is very difficult.

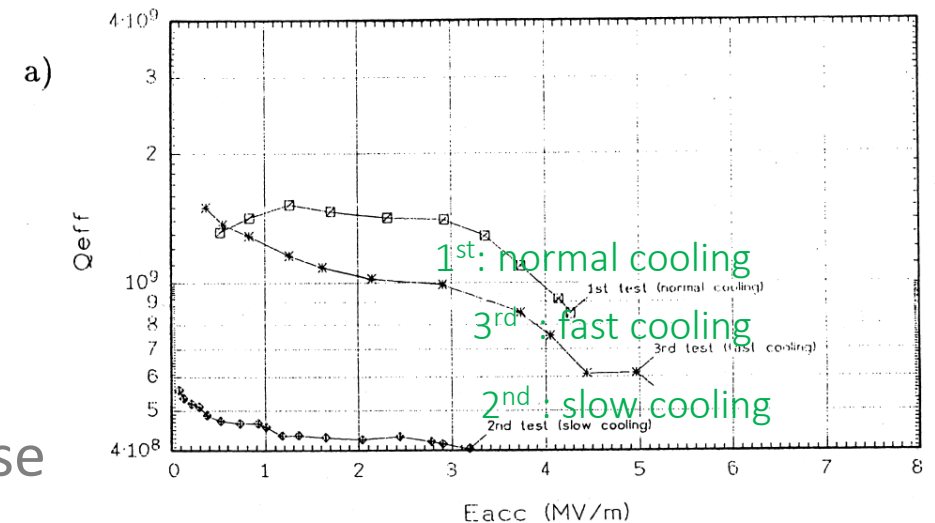
Therefore, hydrogen Q-disease was observed in this condition.

HERA cavities (DESY) : BCP + no Anneal → Q-disease

TRISTAN cavities (KEK) : EP + 800°C Anneal → no Q-disease

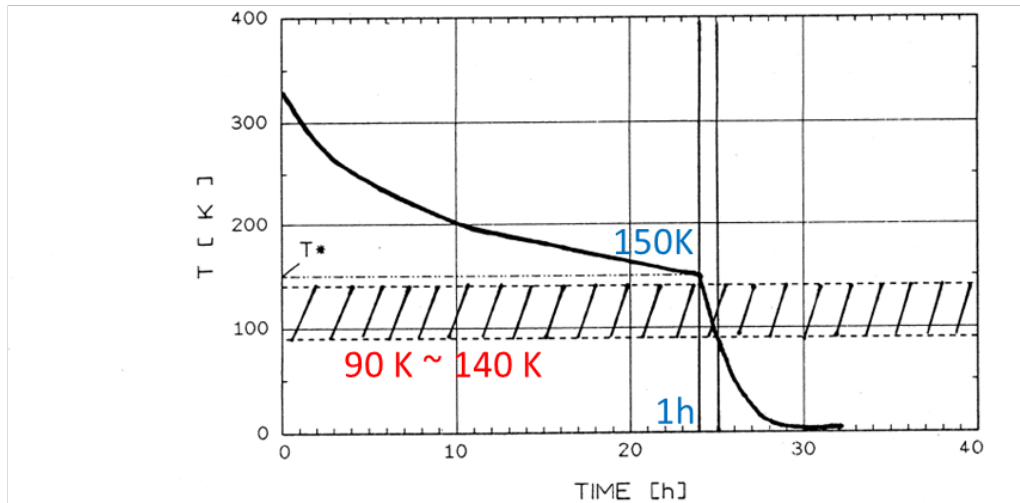


[SRF'91 at DESY]





Cool-down condition in Cryomodule



[SRF'91 at DESY]

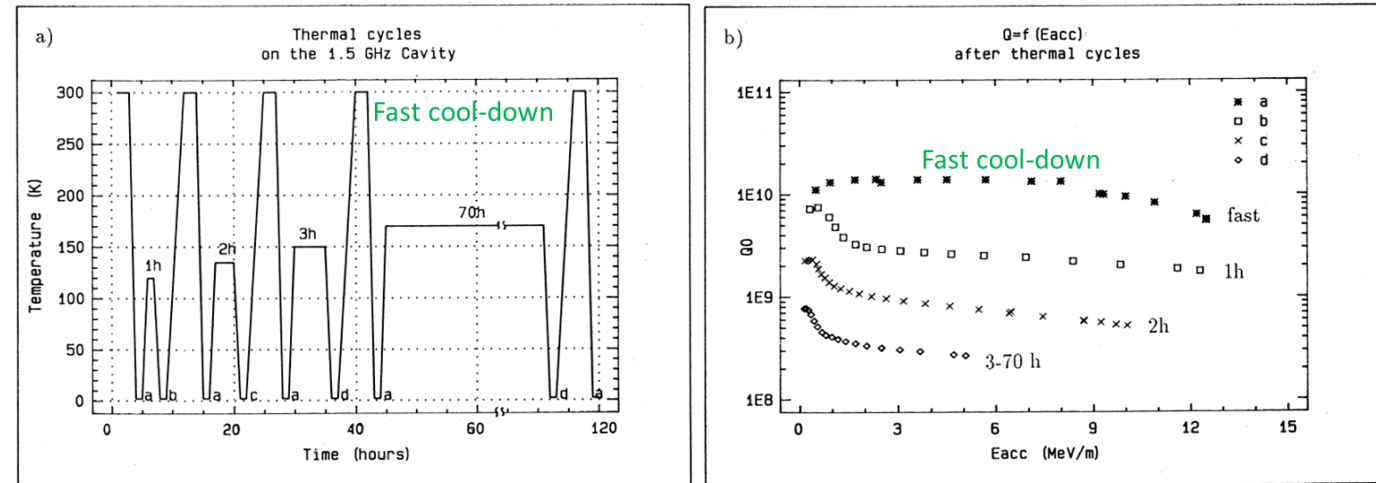
Fig. 4: Cooldown conditions to reduce the effect of the Q disease.

Experimental results on Q-disease at DESY :

A cure method by **fast cooling** around dangerous temperature region from **140K to 90K**

Hydrogen dissolved in a bulk niobium is precipitated on the surface layer and formed niobium-hydride composition.

1.5 GHz Nb 1-cell Cavity at Saclay

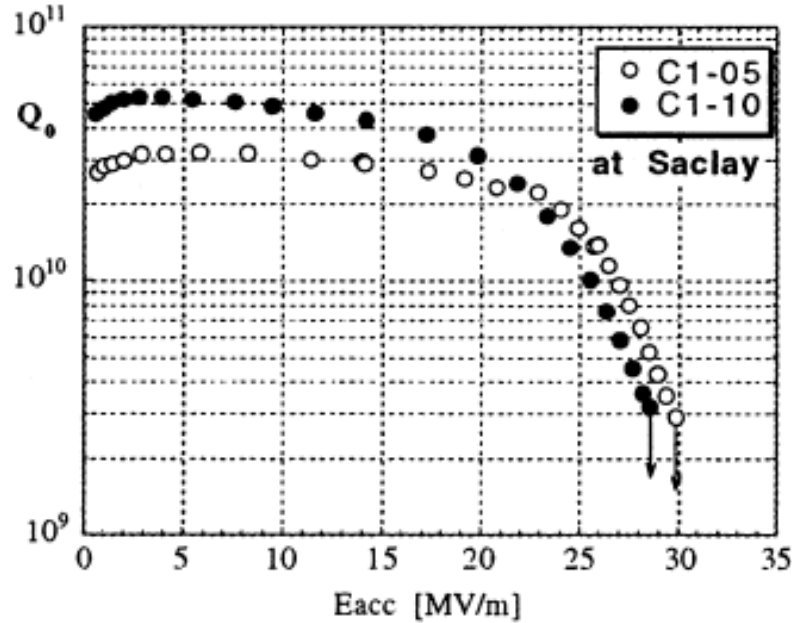


Experimental results on Q-disease at CEA-Saclay :

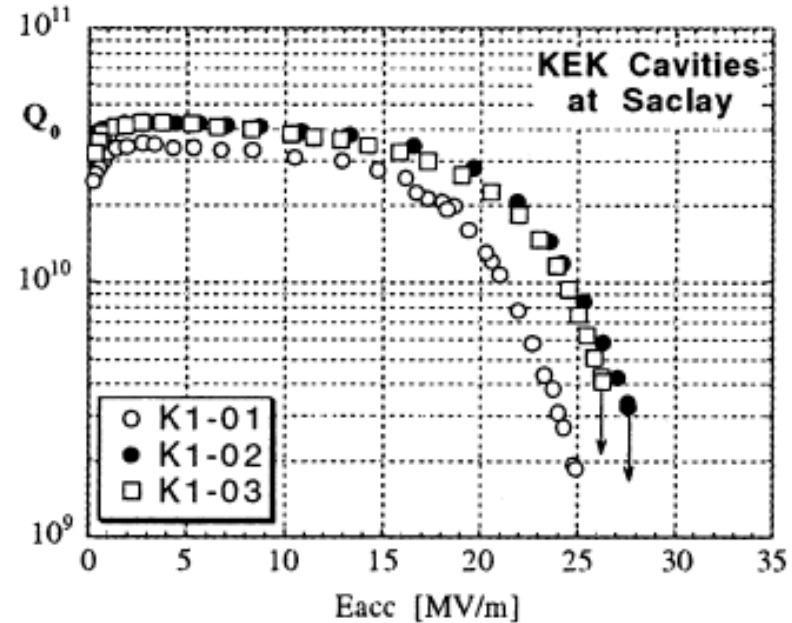
Another cure method is an **annealing at 800°C** of Nb cavities for hydrogen degassing.



2 Saclay cavities tested at Saclay



3 KEK cavities tested at Saclay



[by E. Kako : SRF'97]

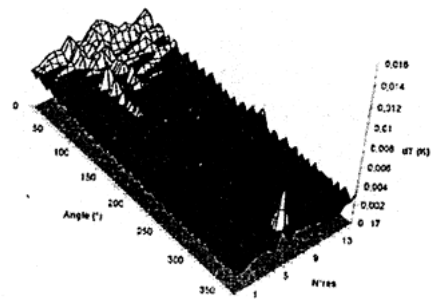


図5. C1-10空洞の表面温度分布(Eacc=29MV/m)

Q- Slope without x-ray

Reproducible observation.
 Temperature rises at whole cavity surface were observed by a temperature mapping system.
 (No Field Emission)

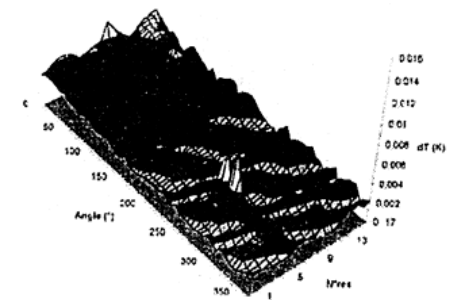
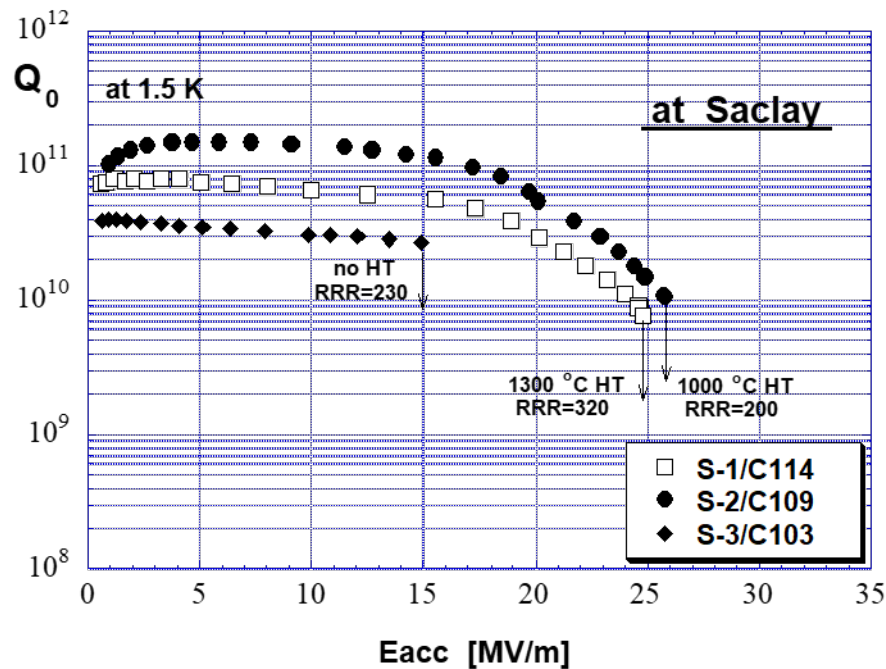


図6. K1-02空洞の表面温度分布(Eacc=28MV/m)

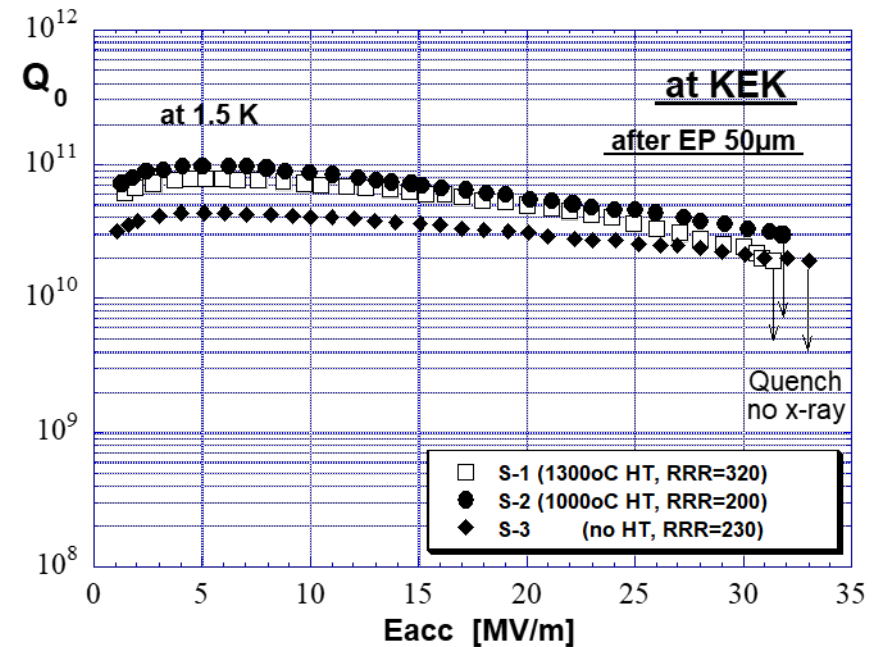


Study on 1-cell cavities at KEK

Improvement of cavity performance by EP



CP cavity @ Saclay



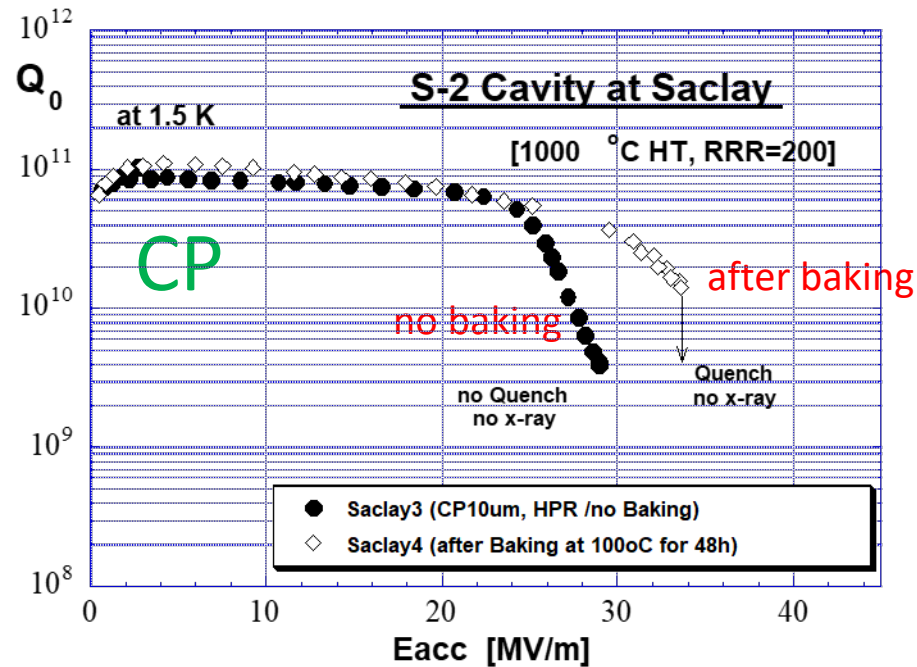
After EP @ KEK

[by E. Kako : SRF'99 at Santa Fe]

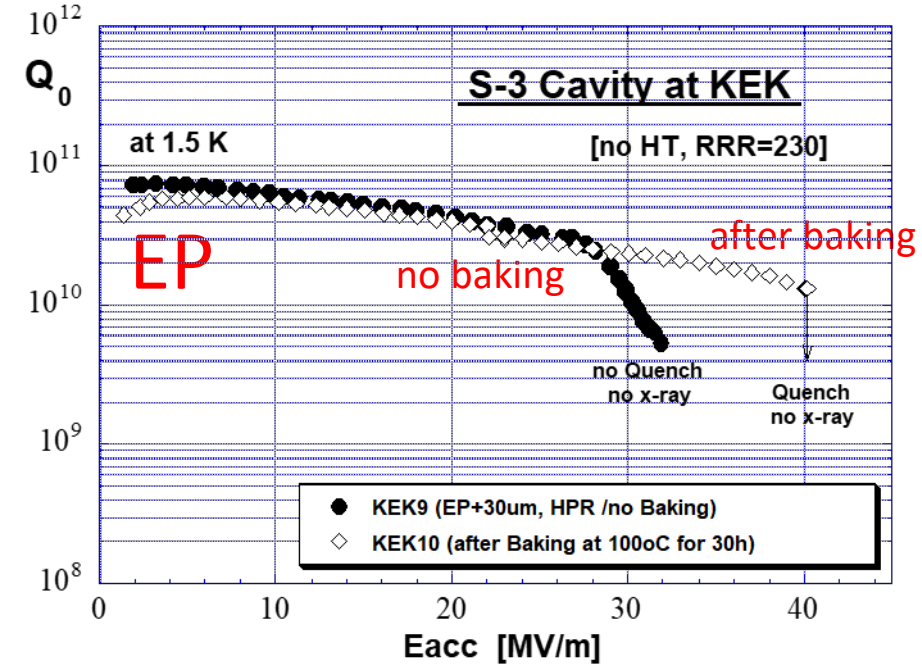


Study on 1-cell cavities at KEK

Effectiveness of baking at 120°C



CP cavity + Natural Drying @ Saclay



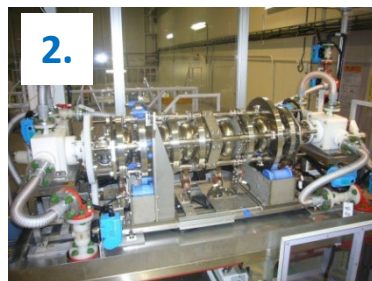
EP cavity + Pumping & Baking @ KEK

EP+120°C Baking is an indispensable procedure to achieve >30 MV/m

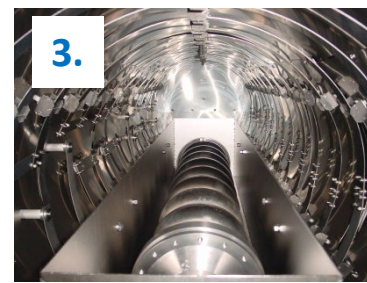
(The initial purpose of baking at KEK was a drying in vacuum for a wet cavity after EP.)



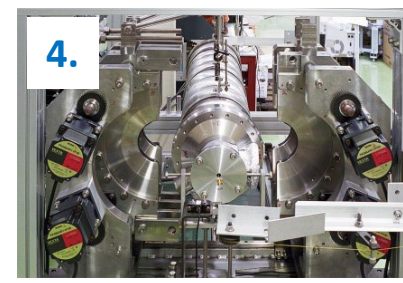
1. Inspection of inner surface



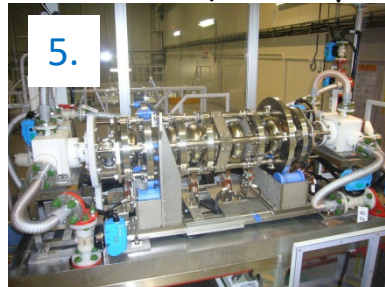
2. Pre-EP + EP-I (5+100 μm)



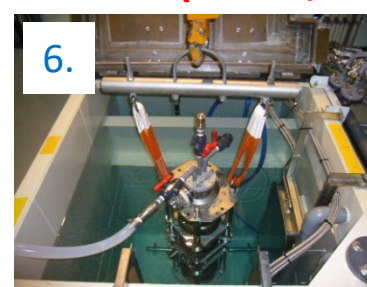
3. Anneal (750°C, 3h)



4. Pre-tuning (flatness, f_0)



5. EP-II (5~20 μm)



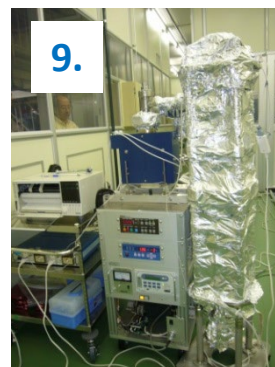
6. Hot bath rinsing with ultra-sonic



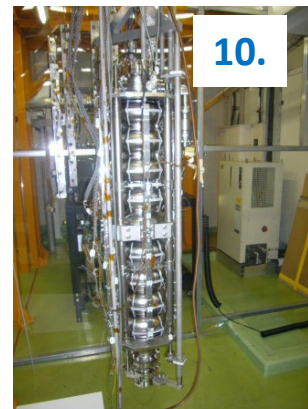
7. HPR



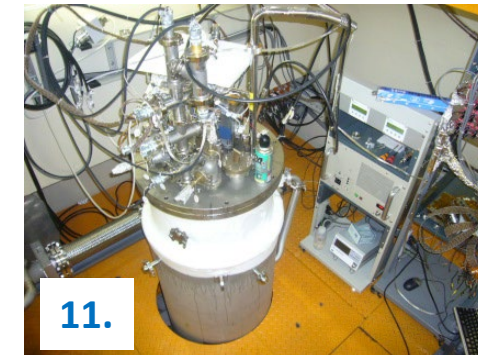
8. Assembly (Class 10)



9. Baking (120°C, 48h) (Class 1000)



10. Hanging stand with T-map



11. Vertical Test

Question (5)



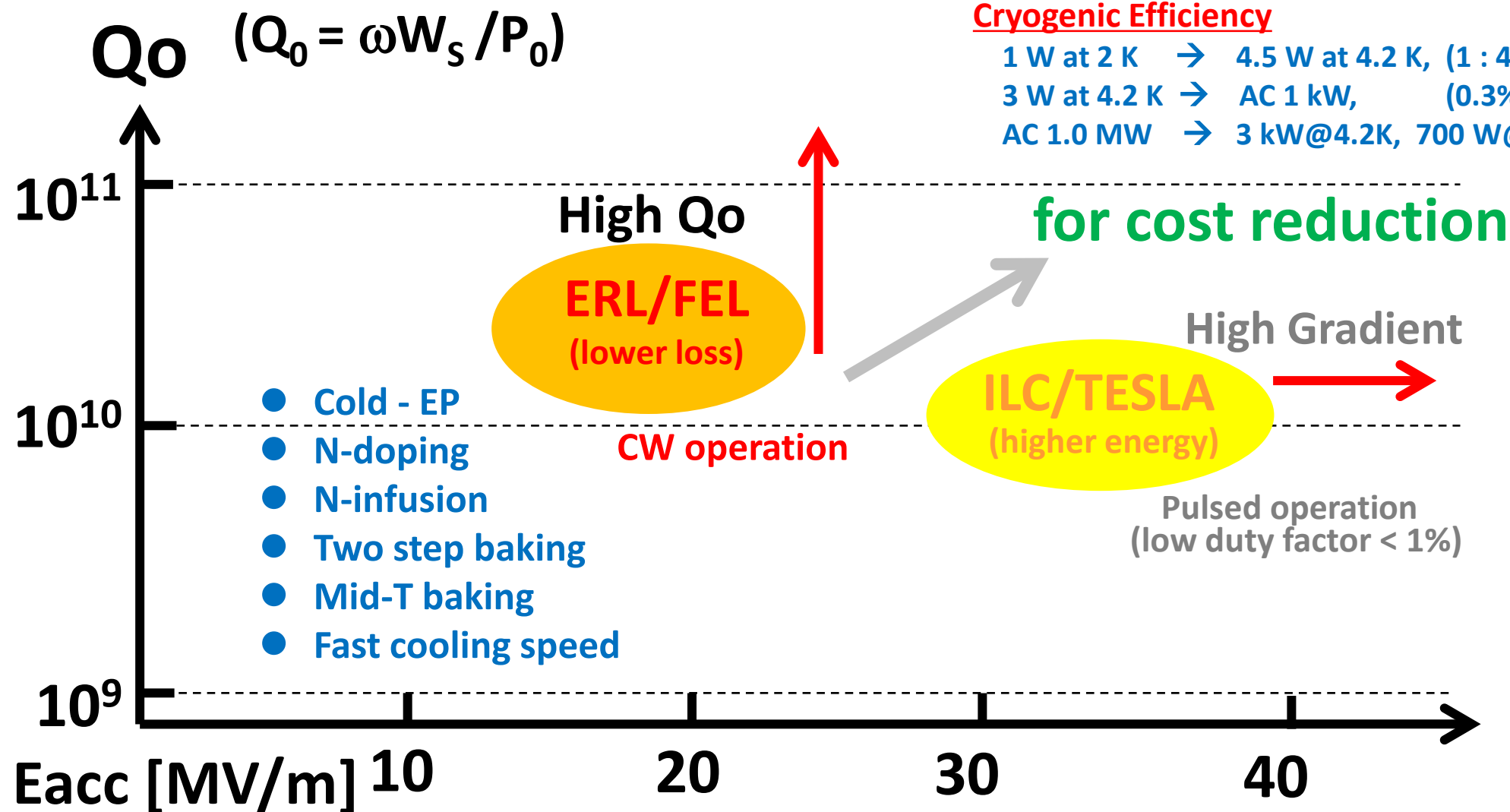
What is the essential surface preparation procedures as a current standard?

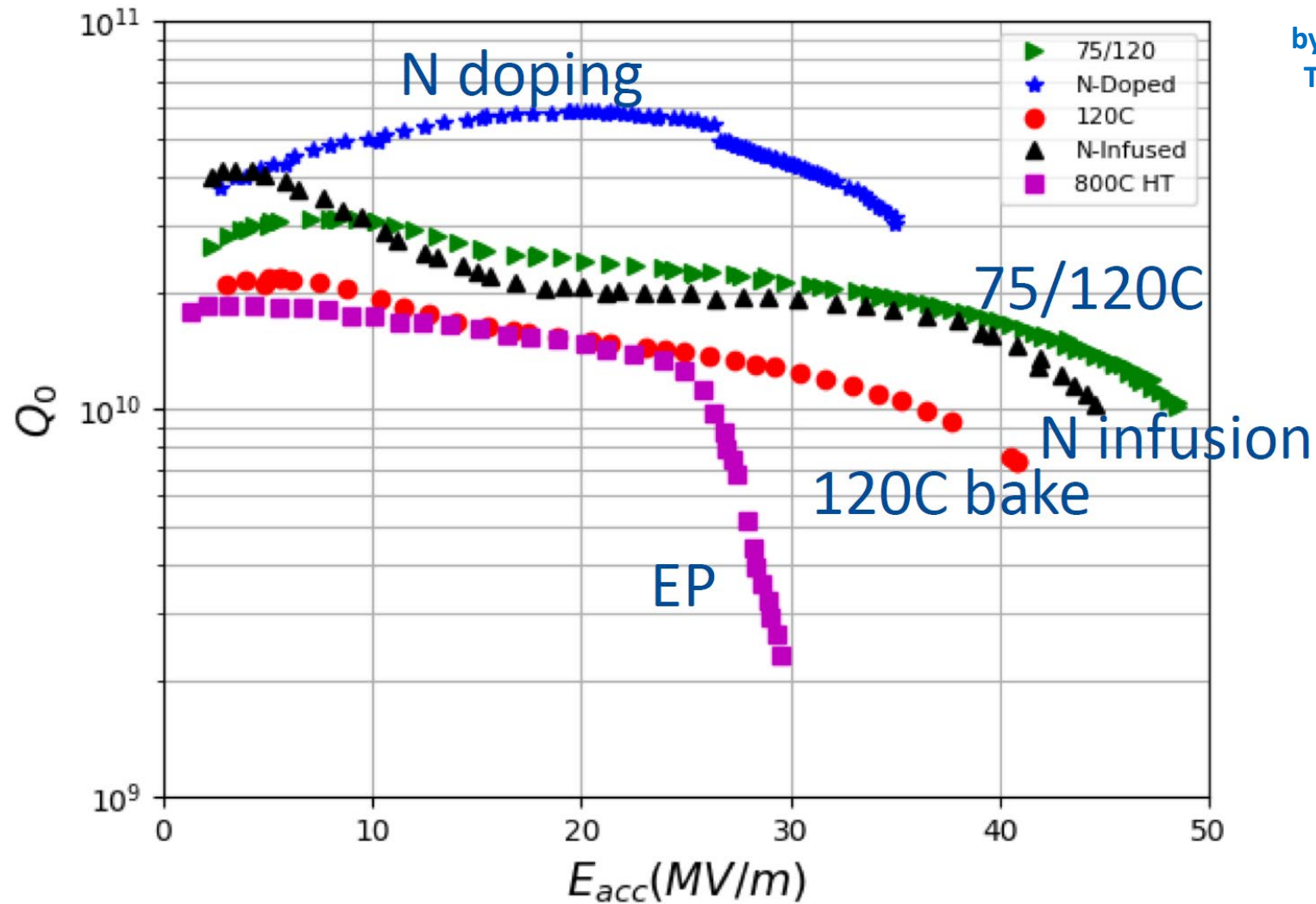


What is the essential surface preparation procedures as a current standard?

Established as an essentially important surface processing :

1. Electro-polishing: **EP**
2. Annealing at 800°C for **hydrogen degassing**
3. High pressure water rinsing: **HPR**
4. Assembly in **class-10** clean room
5. Baking at **120°C**
6. **Clean assembling** procedure to suppress field emission





by A. Grassellino (FNAL)
 TTC meeting at TRIUMF
 2019 February 05



1. Reliable operation at higher gradient (**High-G**)
 - Improvement of clean environment to suppress field emission:
 - a. Development of **slow pumping/venting** system
 - b. Development of local clean booth
 - Performance recovery of degraded cavity:
 - a. Surface cleaning by **He-processing** at low temperature
 - b. Surface cleaning by **plasma processing** using glow discharge
 - c. High power pulsed RF conditioning
2. **High-Q** technology for reducing cryogenic losses
 - **Nitrogen doping** at 800 °C + EP
 - **Nitrogen infusion** at 800+120 °C + (no EP)
 - Development of lower residual magnetic field components
3. Possible operation at **4.2K**
 - **Nb₃Sn** thin film on Nb cavity with higher T_c and higher H_c



1. Introduction
2. Fundamental of SRF Cavity
3. Overview of SRF Cavity System
4. Fabrication and Surface Preparation
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- 6. Summary**

Summary



- Fundamental knowledge of **RF electromagnetic fields** in the SRF cavities is absolutely important in the first step of R&D in SRF technologies.
- Essential surface preparations including **EP, 800°C HT, HPR, 120°C baking** and **clean assembly** was confirmed in many 1.3 GHz 1-cell/9-cell cavities.
- **High power input couplers** and **HOM couplers/absorbers** are one of the most critical components of an SRF cavity system and include varieties of key technologies in design, fabrication, conditioning and operation.
- **International collaboration** is essentially important for R&D of superconducting cavities.

Thank you for your attention.



I believe you are interested in SRF cavity developments.
We welcome your visit to KEK.



Emeritus Prof. Eiji Kako

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KEK, Japan

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email: eiji.kako@kek.jp

Thank you!



Questions !

Superconducting RF (SRF) Cavity



Superconducting RF (SRF) Cavity

