

# Review of 3+1D Hydordynamics Evolution

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$t - z$  coordinates  $\rightarrow$   $\tau - \eta$  coordinates

$$\begin{cases} t \text{ ( laboratory time )} \\ z \text{ ( beam direction )} \end{cases} \implies \begin{cases} \tau = \sqrt{t^2 - z^2} \text{ ( longitudinal proper time )} \\ \eta = \tanh^{-1}(z/t) \text{ ( space-time rapidity )} \end{cases}$$

- Puzzling part

*Covariant derivative in curvilinear coordinates*

## Covariant derivative in curvilinear coordinates

A vector  $\mathbf{a}$  expand by the local frame by point  $M(x^1, x^2, \dots, x^n)$  move to another point  $N(x^1 + dx, x^2 + dx^2, \dots, x^n + dx^n)$ , where  $d\mathbf{a} = 0$ , thus

$$\begin{aligned} 0 &= \mathbf{x}_\alpha da^\alpha + a^\alpha d\mathbf{x}_\alpha \\ &= \mathbf{x}_\alpha da^\alpha + a^\beta \frac{\partial^2 \mathbf{x}}{\partial x^\beta \partial x^\gamma} dx^\gamma \end{aligned} \quad (1)$$

we change the dummy index of the second term, and  $a^\beta \frac{\partial^2 \mathbf{x}}{\partial x^\beta \partial x^\gamma}$  can be expanded by the local frame at point  $M$ ,

$$\frac{\partial^2 \mathbf{x}}{\partial x^\beta \partial x^\gamma} = \Gamma_{\beta\gamma}^\alpha \mathbf{x}_\alpha$$

put it into the formula (1)

$$(da^\alpha) \mathbf{x}_\alpha = -(\Gamma_{\beta\gamma}^\alpha a^\beta dx^\gamma) \mathbf{x}_\alpha$$

## Covariant derivative in curvilinear coordinates

as the  $\mathbf{x}_\alpha$  are independent with each other,

$$d\mathbf{a}^\alpha = -\Gamma_{\beta\gamma}^\alpha \mathbf{a}^\beta$$

The Christoffel symbol  $\Gamma_{\beta\gamma}^\alpha$  :

$$\Gamma_{\beta\gamma}^\alpha = \frac{1}{2} \mathbf{g}^{\alpha\lambda} \left( \frac{\partial \mathbf{g}_{\lambda\gamma}}{\partial x^\beta} + \frac{\partial \mathbf{g}_{\beta\lambda}}{\partial x^\gamma} - \frac{\partial \mathbf{g}_{\gamma\beta}}{\partial x^\lambda} \right)$$

Now we can derive the covariant derivative. Consider a vector field  $\mathbf{a}(M)$ , whose covariant components are  $a_\alpha(x^1, x^2, \dots, x^n)$ . When coordinates transform,  $a_\alpha$  changes to,

$$a_{\alpha'} = \frac{\partial x^\alpha}{\partial x^{\alpha'}} a^\alpha$$

take the derivative with respect to  $x^{\beta'}$ ,

$$\frac{\partial a_{\alpha'}}{\partial x^{\beta'}} = \frac{\partial x^\alpha}{\partial x^{\alpha'}} \frac{\partial x^\beta}{\partial x^{\beta'}} \frac{\partial a_\alpha}{\partial x^\beta} + \frac{\partial^2 x^\alpha}{\partial x^{\alpha'} \partial x^{\beta'}} a_\alpha$$

## Covariant derivative in curvilinear coordinates

through some calculation we can derive that

$$\frac{\partial a_{\gamma'}}{\partial x^{\beta'}} - \Gamma_{\beta'\gamma'}^{\alpha'} a_{\alpha'} = \left( \frac{\partial a_{\gamma}}{\partial x^{\beta}} - \Gamma_{\beta\gamma}^{\alpha} a_{\alpha} \right) \frac{\partial x^{\beta}}{\partial x^{\beta'}} \frac{\partial x^{\gamma}}{\partial x^{\gamma'}}$$

from above, we can see that the expression with two freedom index  $\beta\gamma$

$$\frac{\partial a_{\gamma}}{\partial x^{\beta}} - \Gamma_{\beta\gamma}^{\alpha} a_{\alpha} = \left( \frac{\partial}{\partial x^{\beta}} \delta_{\gamma}^{\alpha} - \Gamma_{\beta\gamma}^{\alpha} \right) a_{\alpha}$$

follow the second order covariant tensor's transformational rules. Then we find **Covariant derivative** of the covariant tensor field,

$$\nabla_{\beta} a_{\gamma} = \left( \frac{\partial}{\partial x^{\beta}} \delta_{\gamma}^{\alpha} - \Gamma_{\beta\gamma}^{\alpha} \right) a_{\alpha}$$

where " - " for covariant tensor, " + " for contravariant tensor. This can be generalized to arbitrary high order.

$$\nabla_s T_{ij}^{lk} = \partial_s T_{ij}^{lk} - \Gamma_{is}^r T_{rj}^{lk} - \Gamma_{js}^r T_{ir}^{lk} + \Gamma_{rs}^l T_{ij}^{rk} + \Gamma_{rs}^k T_{ij}^{lr}$$

## The conservation law in the new coordinate system

$$\begin{cases} \partial_{\mu} J^{\mu} = 0 \\ \partial_{\mu} T^{\mu\nu} = 0 \end{cases}$$

transformed into

$$T_{,\tau}^{\tau\tau} + T_{,x}^{\tau x} + T_{,y}^{\tau y} + T_{,\eta}^{\tau\eta} + \frac{1}{\tau} T^{\tau\tau} + \tau T^{\eta\eta} = 0$$

$$T_{,\tau}^{\tau x} + T_{,x}^{xx} + T_{,y}^{xy} + T_{,\eta}^{\eta x} + \frac{1}{\tau} T^{\tau x} = 0$$

$$T_{,\tau}^{\tau y} + T_{,x}^{xy} + T_{,y}^{yy} + T_{,\eta}^{\eta y} + \frac{1}{\tau} T^{\tau y} = 0$$

$$T_{,\tau}^{\tau\eta} + T_{,x}^{\eta x} + T_{,y}^{\eta y} + T_{,\eta}^{\eta\eta} + \frac{3}{\tau} T^{\tau\eta} = 0$$

$$J_{,\tau}^{\tau} + J_{,x}^x + J_{,y}^y + J_{,\eta}^{\eta} + \frac{1}{\tau} J^{\tau} = 0$$

## The conservation law in the new coordinate system

By making use of the relations  $T^{\tau i} = \bar{v}_i T^{\tau\tau} + v_i P$ ,  $T^{\eta\eta} = \frac{P}{\tau^2}$ , the energy-momentum conservation equations turn into

$$\begin{aligned} & T_{,\tau}^{\tau\tau} + (v_x T^{\tau\tau})_{,x} + (v_y T^{\tau\tau})_{,y} + \left(\frac{v_\eta}{\tau} T^{\tau\tau}\right)_{,\eta} + \frac{1}{\tau} T^{\tau\tau} \\ & + (v_x P)_{,x} + (v_y P)_{,y} + \left(\frac{v_\eta}{\tau} P\right)_{,\eta} + \frac{v_\eta^2}{\tau} (T^{\tau\tau} + P) + \frac{P}{\tau} = 0 \\ & T_{,\tau}^{\tau x} + (v_x T^{\tau x})_{,x} + (v_y T^{\tau x})_{,y} + \left(\frac{v_\eta}{\tau} T^{\tau x}\right)_{,\eta} + \frac{1}{\tau} T^{\tau x} + P_{,x} = 0 \\ & T_{,\tau}^{\tau y} + (v_x T^{\tau y})_{,x} + (v_y T^{\tau y})_{,y} + \left(\frac{v_\eta}{\tau} T^{\tau y}\right)_{,\eta} + \frac{1}{\tau} T^{\tau y} + P_{,y} = 0 \\ & T_{,\tau}^{\tau\eta} + (v_x T^{\tau\eta})_{,x} + (v_y T^{\tau\eta})_{,y} + \left(\frac{v_\eta}{\tau} T^{\tau\eta}\right)_{,\eta} + \left(\frac{P}{\tau^2}\right)_{,\eta} + \frac{3}{\tau} T^{\tau\eta} = 0 \\ & J_{,\tau}^{\tau} + (v_x J^{\tau})_{,x} + (v_y J^{\tau})_{,y} + \left(\frac{v_\eta}{\tau} J^{\tau}\right)_{,\eta} + \frac{1}{\tau} J^{\tau} = 0 \end{aligned}$$

# Evolution

- FCT-SHASTA Algorithm

*We can use the SHASTA(SHarp And Smooth Transport Algorithm) algorithm to solve partial differential equations with the form*

$$\partial_t (T) + \partial_i (v_i T) = S$$

*to solve the hydrodynamic equations.*

- Transport stage in SHASTA
- Calculation for Hydrodynamics evolution equations



# Transport stage in SHASTA

$$\partial_t \rho + \partial_x (v\rho) = 0$$

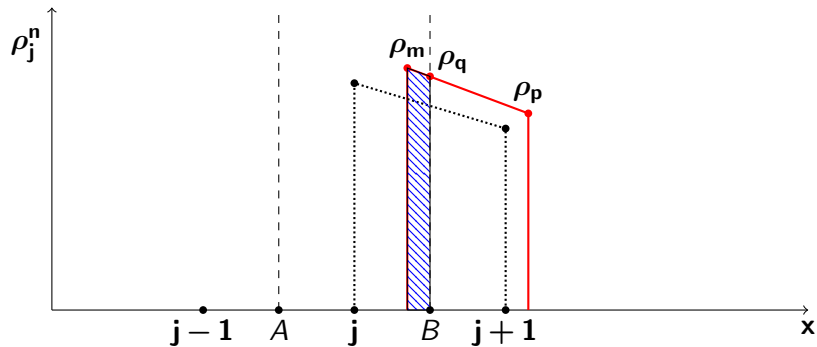
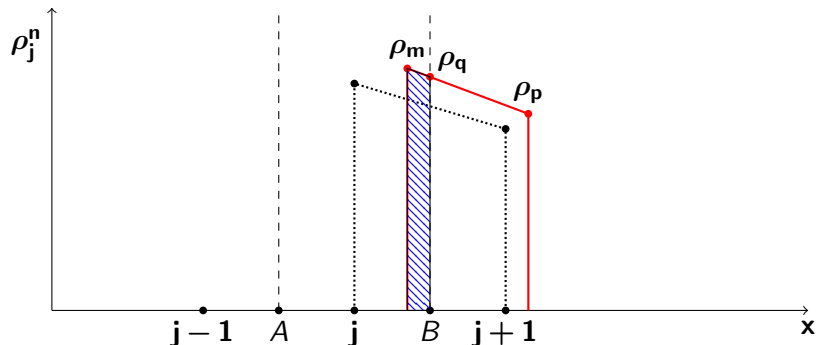


Figure : The geometric explanation of SHASTA algorithm

## Transport stage in SHASTA



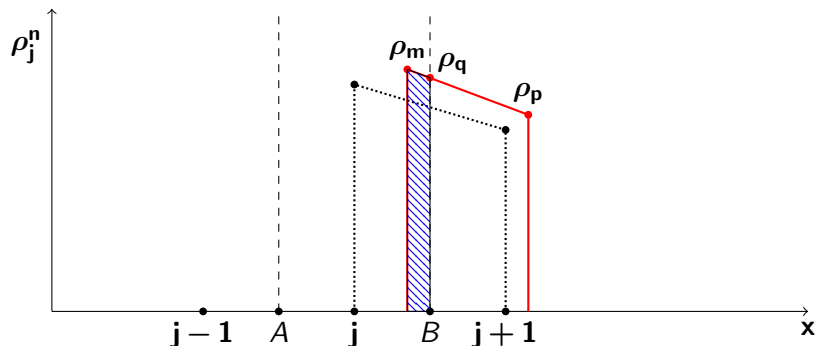
$$\frac{1}{2}(\rho_j^0 + \rho_{j+1}^0)\delta x = \frac{1}{2}(\rho_m + \rho_p) \left[ \delta x + (v_{j+1}^{1/2} - v_j^{1/2}) \delta t \right]$$

If we consider the two sides if the solid trapezoid vary in the same rate, we get

$$\rho_p = \rho_{j+1}^0 \delta x / \left[ \delta x + (v_{j+1}^{1/2} - v_j^{1/2}) \delta t \right]$$

$$\rho_m = \rho_j^0 \delta x \left[ \delta x + (v_{j+1}^{1/2} - v_j^{1/2}) \delta t \right]$$

## Transport stage in SHASTA

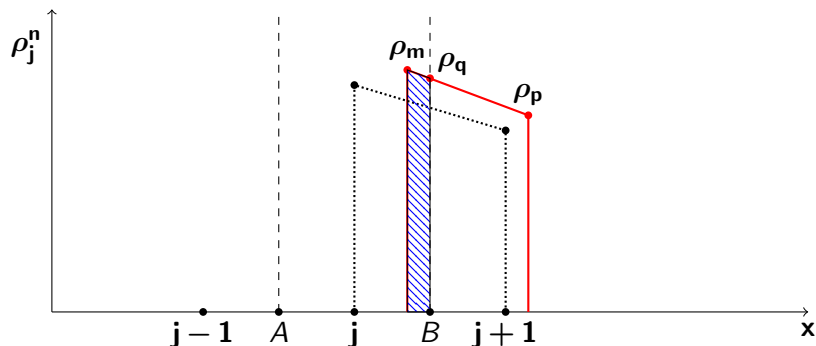


$$\rho_q = \rho_p + (\rho_m - \rho_p) \left( \delta x / 2 + v_{j+1}^{1/2} \delta t \right) \left[ \delta x + \left( v_{j+1}^{1/2} - v_j^{1/2} \right) \delta t \right]$$

The residual mass is given by the the blue shadow area,

$$\begin{aligned} \Delta m_{re,j}^n &= (\rho_m + \rho_q) (\delta x / 2 - v_j^{1/2} \delta t) \\ &= \delta x \left[ \frac{1}{2} Q_+^2 (\rho_{j+1}^n - \rho_j^n) + Q_+ \rho_j^n \right] \end{aligned}$$

## Transport stage in SHASTA

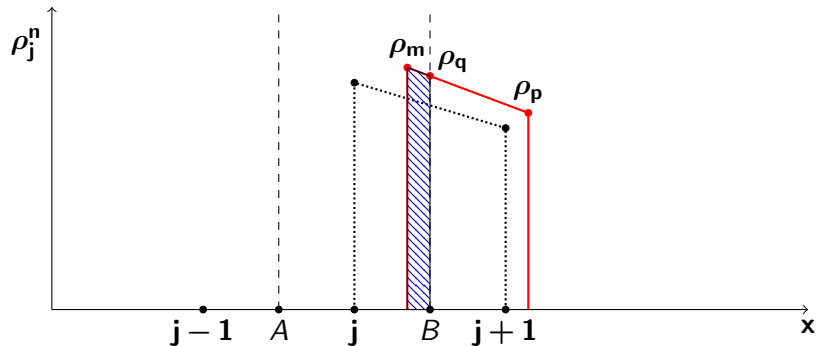


The another part of the element's mass (in cell  $j+1$ ) is  $\Delta m_{an,j}^n$ , we can easily calculate

$$\Delta m_{an,j-1}^n = \delta x \left[ \frac{1}{2} Q_-^2 (\rho_{j-1}^n - \rho_j^n) + Q_- \rho_j^n \right]$$

$$Q_{\pm} = \left( 1/2 \mp v_j^{1/2} \delta t / \delta x \right) / \left[ 1 \pm \left( v_{j\pm 1}^{1/2} - v_j^{1/2} \right) \delta t / \delta x \right]$$

## Transport stage in SHASTA



The mass density at grid point  $j$  and time step  $n + 1$  is

$$\begin{aligned} \rho_j^{n+1} &= (\Delta m_{an,j-1}^n + \Delta m_{re,j}^n) / \delta x \\ &= \frac{1}{2} Q_-^2 (\rho_{j-1}^n - \rho_j^n) + \frac{1}{2} Q_+^2 (\rho_{j+1}^n - \rho_j^n) + (Q_+ + Q_-) \rho_j^n \end{aligned}$$

## Transport stage in SHASTA

If we consider a uniform velocity, the above equation will be simplified to

$$\rho_j^{n+1} = \rho_j^n - \frac{\varepsilon}{2} (\rho_{j+1}^n - \rho_{j-1}^n) + \left( \frac{1}{8} + \frac{\varepsilon^2}{2} \right) (\rho_{j+1}^n - 2\rho_j^n + \rho_{j-1}^n)$$

where  $\varepsilon = v\delta t/\delta x$ . If  $v = 0$ ,

$$\rho_j^{n+1} = \frac{1}{8} (\rho_{j+1}^n - 2\rho_j^n + \rho_{j-1}^n)$$

## Anti-diffusion stage

Now, we can see that the solution is conservative and positivity but has a large zero order diffusion. To correct the diffusion, we used an anti-diffusion form

$$\bar{\rho}_j^{n+1} = \frac{1}{8} \left( \rho_{j+1}^{n+1} - 2\rho_j^{n+1} + \rho_{j-1}^{n+1} \right)$$

but it will destroy the positivity. So the anti-diffusion terms are written in mass flux form

$$\bar{\rho}_j^{n+1} = \rho_j^{n+1} - f_{j+1/2}^{n+1} + f_{j-1/2}^{n+1}$$

where the mass flux is

$$f_{j\pm 1/2}^{n+1} = \pm \frac{1}{8} \left( \rho_{j\pm 1}^{n+1} - \rho_j^{n+1} \right)$$

## Anti-diffusion stage

and the flux is corrected as

$$f_{j+1/2}^{(c)n+1} = \sigma \max \left\{ 0, \min \left\{ \sigma \Delta_{j-1/2}, \frac{1}{8} \Delta_{j+1/2}, \sigma \Delta_{j+3/2} \right\} \right\}$$

where  $\Delta_{j+1/2} = \rho_{j+1}^{n+1} - \rho_j^{n+1}$  and  $\sigma = \text{sgn} \Delta_{j+1/2}$ .

The final mass density at grid  $j$  and time step  $n+1$  after corrected anti-diffusion stage is

$$\bar{\rho}_j^{n+1} = \rho_j^{(c)n+1} - f_{j+1/2}^{n+1} + f_{j-1/2}^{(c)n+1}$$



## Multi-dimensional algorithm

In this multi-dimensional algorithm the 1D FCT-SHASTA algorithm with time-splitting is used along one direction at a split-time step, while a  $x \rightarrow y \rightarrow \eta \rightarrow y \rightarrow x$  rotation is used to extend the FCT-SHASTA algorithm to multi-dimensions and to suppress the numerical eccentricity produced in transverse direction during the hydrodynamic evolution.

## Evolution

At first, we will change conservation equations to the form as

$$\tilde{T}_{,\tau}^{\tau\tau} + (v_x \tilde{T}^{\tau\tau})_{,x} + (v_y \tilde{T}^{\tau\tau})_{,y} + (v'_\eta \tilde{T}^{\tau\eta})_{,\eta} = S^\tau$$

$$\tilde{T}_{,\tau}^{\tau x} + (v_x \tilde{T}^{\tau x})_{,x} + (v_y \tilde{T}^{\tau x})_{,y} + (v'_\eta \tilde{T}^{\tau x})_{,\eta} = S^x$$

$$\tilde{T}_{,\tau}^{\tau y} + (v_x \tilde{T}^{\tau y})_{,x} + (v_y \tilde{T}^{\tau y})_{,y} + (v'_\eta \tilde{T}^{\tau y})_{,\eta} = S^y$$

$$\tilde{T}_{,\tau}^{\tau\eta} + (v_x \tilde{T}^{\tau\eta})_{,x} + (v_y \tilde{T}^{\tau\eta})_{,y} + (v'_\eta \tilde{T}^{\tau\eta})_{,\eta} = S^\eta$$

$$\tilde{J}_{,\tau}^\tau + (v_x \tilde{J}^\tau)_{,x} + (v_y \tilde{J}^\tau)_{,y} + (v'_\eta \tilde{J}^\tau)_{,\eta} = 0$$

where the tilde term  $\tilde{X} = \tau X$ ,  $v'_\eta = v_\eta/\tau$ , and the source terms are

$$\begin{pmatrix} S^\tau \\ S^x \\ S^y \\ S^\eta \end{pmatrix} = \begin{pmatrix} -\nabla \cdot (\mathbf{v}\tilde{P}) - \tau v_\eta'^2 (\tilde{T}^{\tau\tau} + \tilde{P}) - \tilde{P}/\tau \\ -\tilde{P}_{,x} \\ -\tilde{P}_{,y} \\ -\left(\frac{\tilde{P}}{\tau^2}\right)_{,\eta} - \frac{2}{\tau} \tilde{T}^{\tau\eta} \end{pmatrix}$$

# Evolution

Then the numerical method and procedures of a combined FCT-SHASTA and the 2nd order Runge-Kutta algorithm in solving hydrodynamic equations with a simplified conservation as below

$$\partial_\tau \mathcal{I} + \partial_i (v_i \mathcal{I}) = S$$

where  $\mathcal{I} := \tau T^{\tau\nu}$  denotes one component of the energy-momentum tensor.

# Evolution

- 1 Calculate source term at time step  $n$ :  $S = S(\tau^n, \varepsilon^n, v_i^n, \mathcal{I}^n)$ .
- 2 Get  $\mathcal{I}'^{n+1/2}$  by using SHASTA algorithm through  $\partial_\tau \mathcal{I} + \partial_i (v_i \mathcal{I}) = 0$  within time step  $n + 1/2$ .
- 3 Get  $\mathcal{I}^{n+1/2} = \mathcal{I}'^{n+1/2} + \frac{1}{2} \Delta \tau S(\tau^n, \varepsilon^n, v_i^n, \mathcal{I}^n)$  and use the root-finding method to calculate the energy density and velocity  $\varepsilon^{n+1/2}, v_i^{n+1/2}$ .
- 4 Calculate source term at half-time step  $n + 1/2$ :  $S = S(\tau^{n+1/2}, \varepsilon^{n+1/2}, v_i^{n+1/2}, \mathcal{I}^{n+1/2})$ .
- 5 Get  $\mathcal{I}'^{n+1}$  by using SHASTA algorithm through  $\partial_\tau \mathcal{I} + \partial_i (v_i \mathcal{I}) = 0$  with  $v_i^{n+1/2}$
- 6 Get  $\mathcal{I}^{n+1} = \mathcal{I}'^{n+1} + \frac{1}{2} \Delta \tau S(\tau^{n+1/2}, \varepsilon^{n+1/2}, v_i^{n+1/2}, \mathcal{I}^{n+1/2})$  and use the root-finding method to calculate the energy density and velocity  $\varepsilon^{n+1}, v_i^{n+1}$ .

## Root-finding

The energy density is determined from  $T^{\tau\nu}$  through a root finding method by iterating the equation

$$\varepsilon = T^{\tau\tau} - \frac{M^2}{T^{\tau\tau} + P(\varepsilon)}$$

with the iteration value of  $\varepsilon$  for the iteration is approximated by  $\varepsilon = T^{\tau\tau}$ . Where  $M^2 = (T^{\tau\perp})^2 + (\tau T^{\tau\eta})^2$ . And the flow velocity is given by

$$\begin{aligned}\vec{v}_{\perp} &= \vec{T}^{\tau\perp} / [T^{\tau\tau} + P(\varepsilon)] \\ v_{\eta} &= \tau T^{\tau\eta} / [T^{\tau\tau} + P(\varepsilon)]\end{aligned}$$

תודה  
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Tack